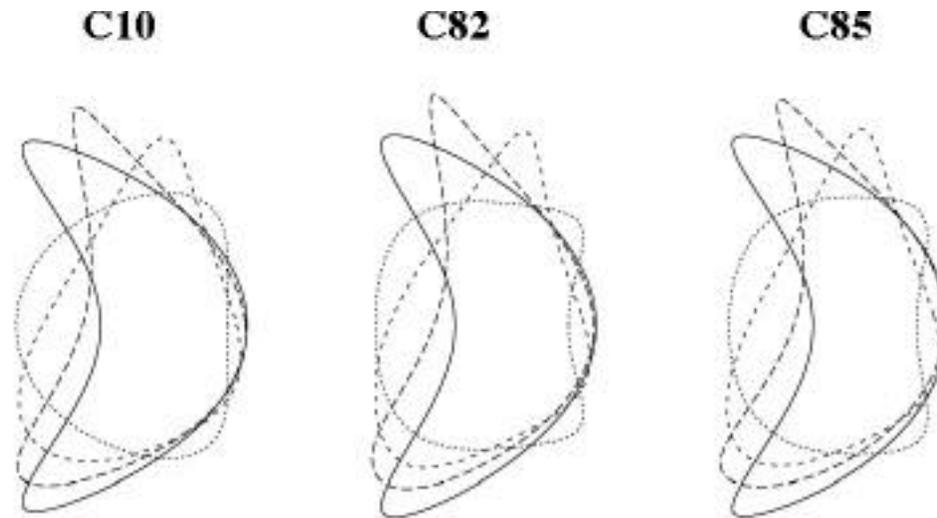


Progress in Configuration Development

- We discussed, last week, methods by which the required boundary shaping may be reduced for the kink stability.
 - current profile,
 - magnitude of current.
- We also examined various configurations, showing that QAS3_C82 was a good starting point for using the above methods to ease the problem associated with the high coil current density.
- We now have a new configuration, QAS3_C85, which
 - is kink stable at ~4% beta, $I_p \sim 180$ kA, with the C10/C82 reference profiles.
 - has comparable, perhaps somewhat better, QAness as in C10/C82, particularly in the outer region.

- has comparable J_{\max} as that in C10.
- This is achieved, starting from C82, by
 - relaxing constraint on the kink growth rate at $I_p=200$ kA,
 - further optimizing the quasi-axisymmetry in regions $s>0.5$,
 - imposing an additional constraint on the maximum coil current density.

Comparison of Boundary Shapes of Three Recent Configurations

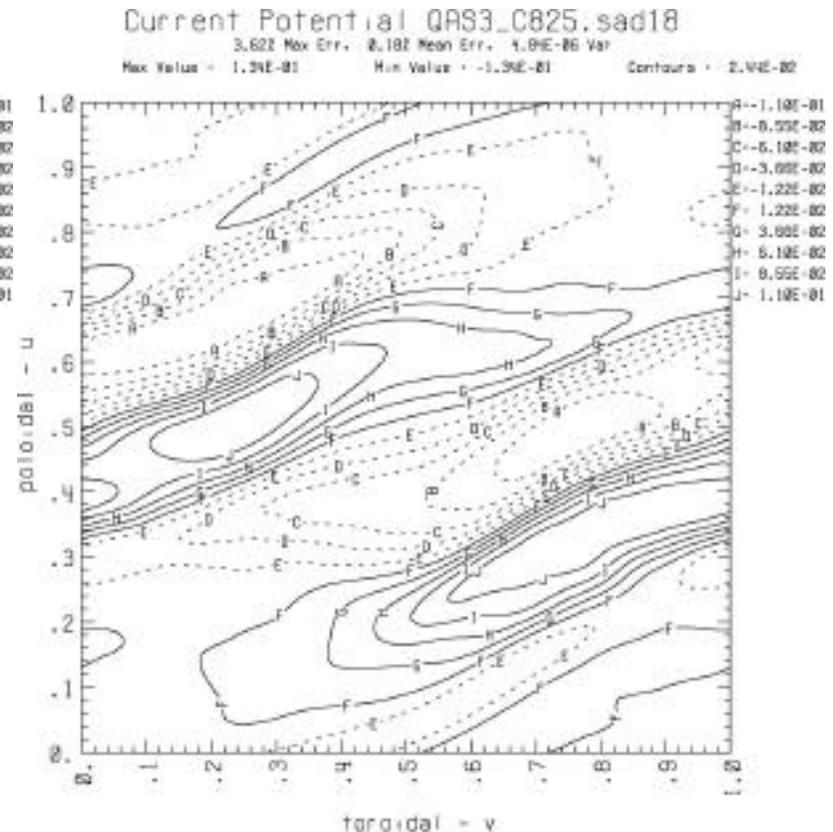
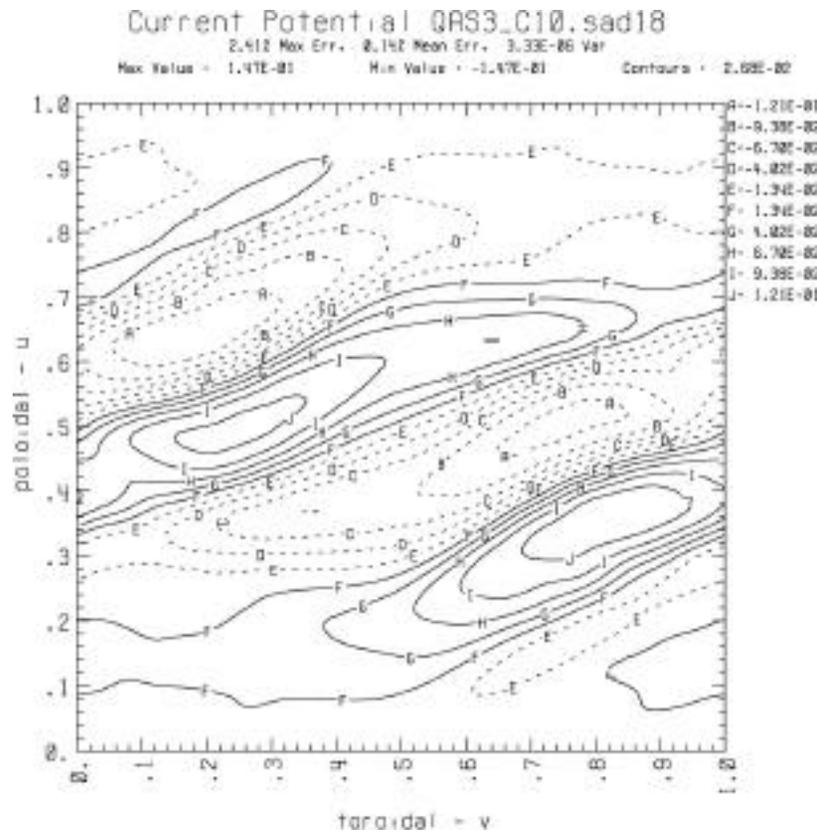


A	3.43	3.43	3.48
κ	1.81	1.90	1.98
δ	0.48	0.45	0.53
Jmax	0.84	1.02	0.82

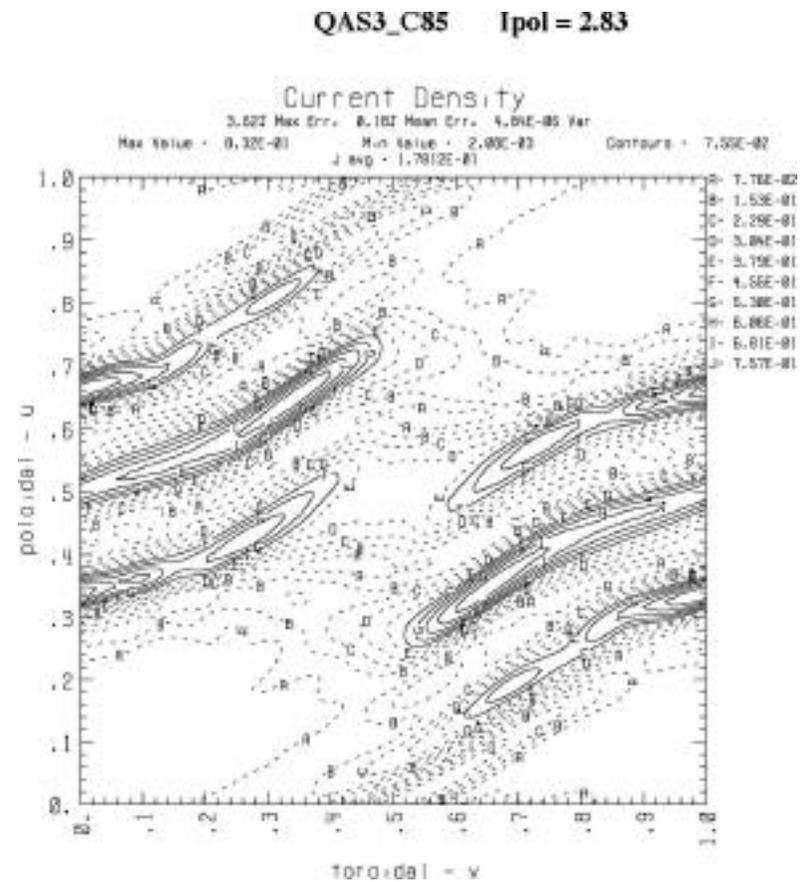
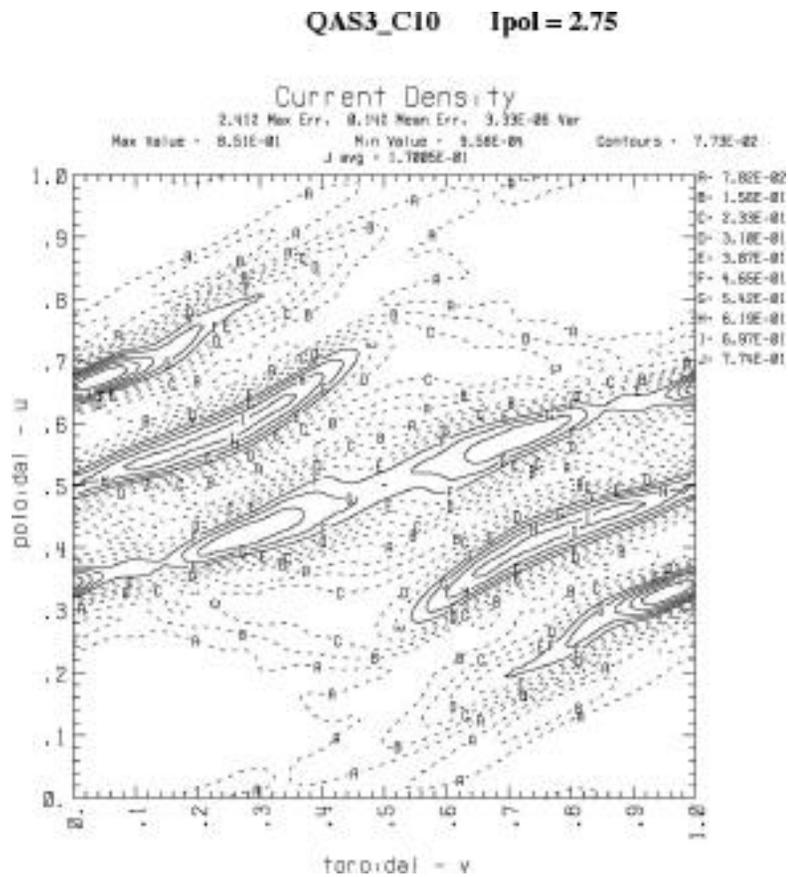
Comparison of Potential Contours from Coil Current Sheet Solutions (18 cm uniform offset)

$\langle M \rangle = 2.91$

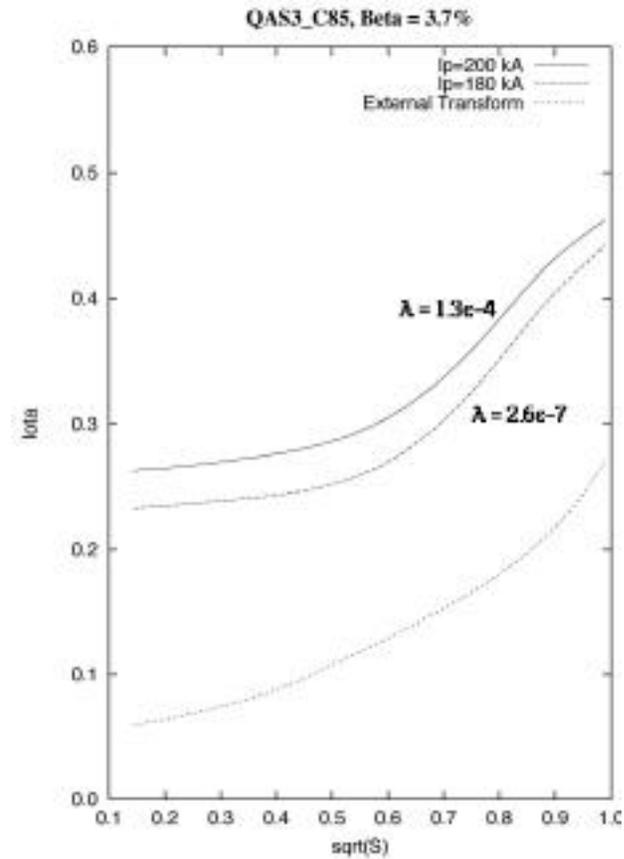
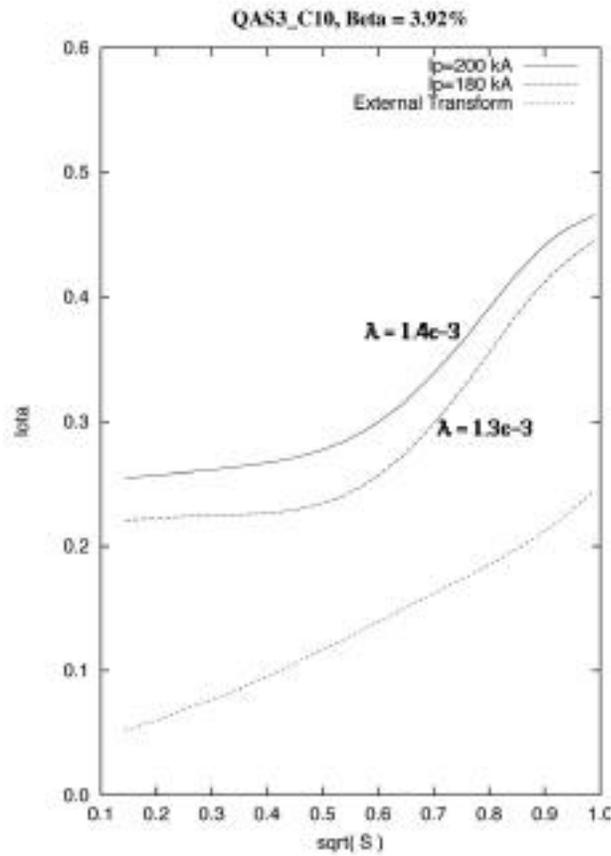
$\langle M \rangle = 3.01$



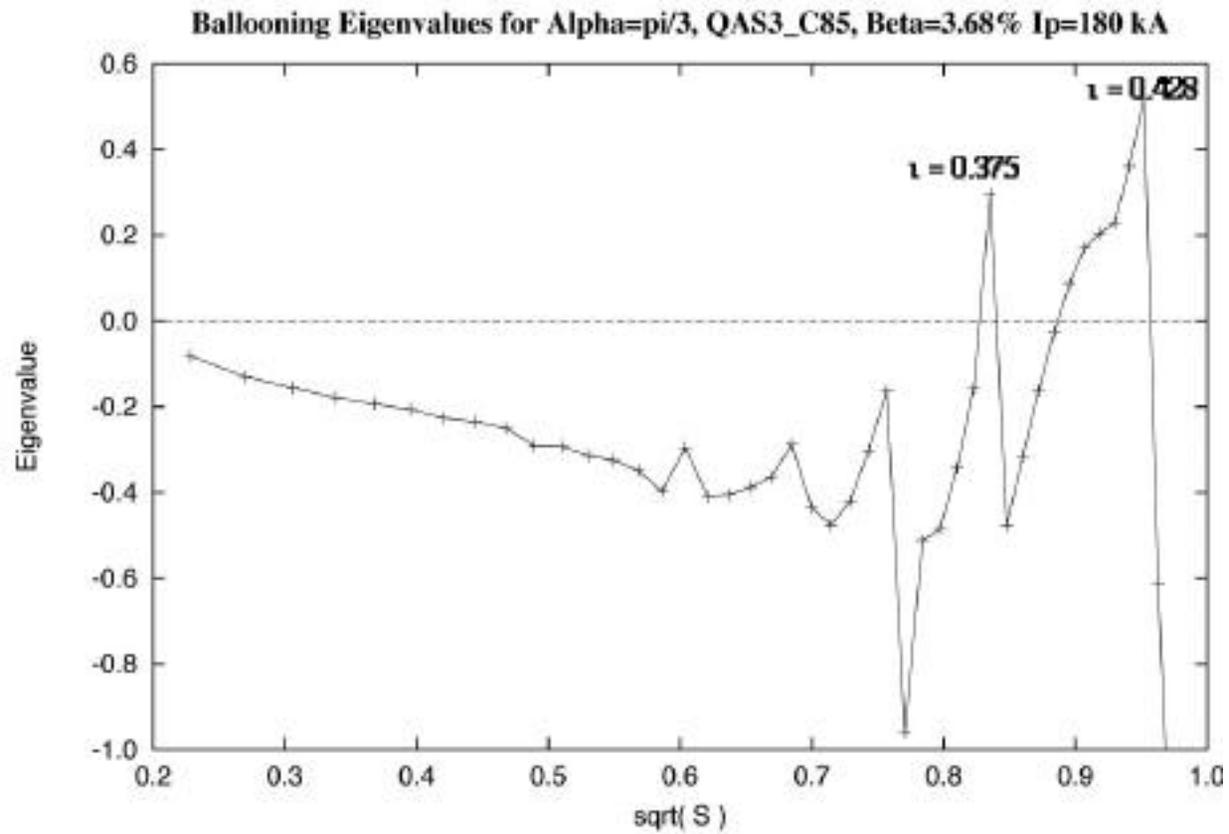
Comparison of Current Densities from Current Sheet Solutions



Comparison of Rotational Transform and the Kink Eigenvalues

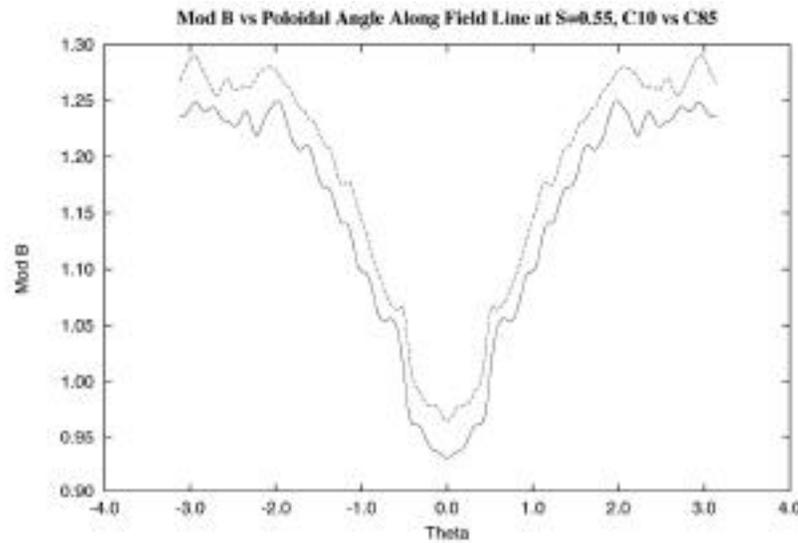


Preliminary Calculations of the Ballooning Stability for C85



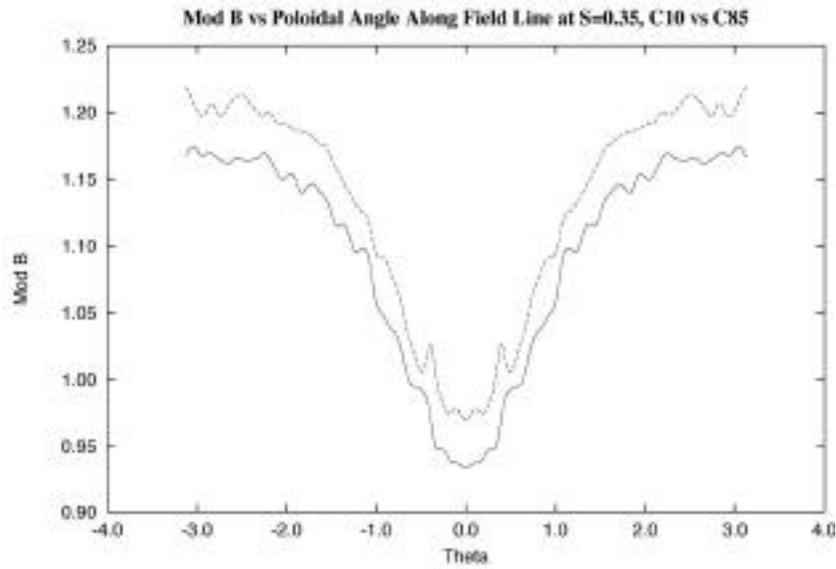
Comparisons of Transport Measures for Particle Confinement

$S = 0.55$



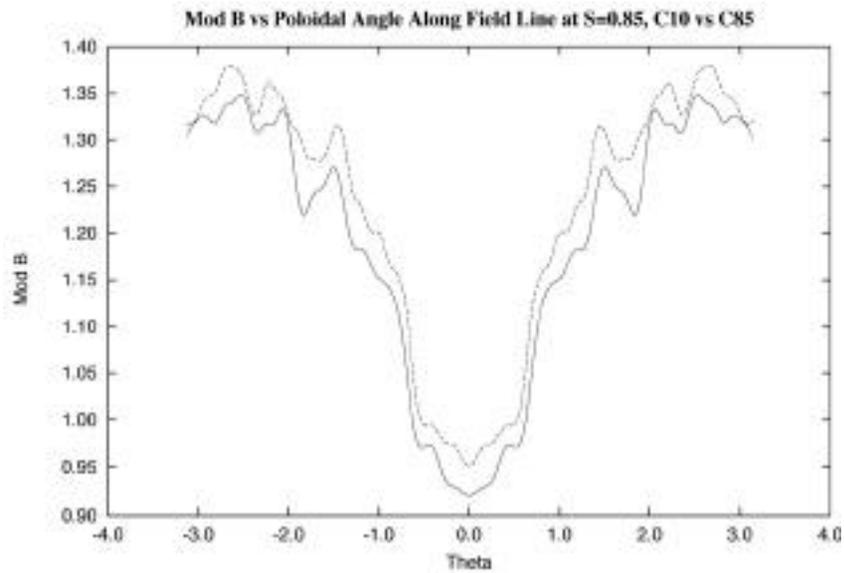
	<u>C10</u>	<u>C82</u>	<u>C85</u>
$(B_{mn})^2$	2.1e-4	2.5e-4	1.9e-4
$\{(m-n)*B_{mn}\}^2$	5.0e-3	6.2e-3	4.3e-3
w_d	1.8e-2	2.2e-2	1.2e-2
$w \sin d$	1.0e-2	1.2e-2	6.3e-3
Poloidal flux	0.22	0.22	0.22
$B(s=0)$	1.01	1.02	1.05
$B(s=1)$	1.20	1.21	1.23

$$S = 0.35$$



	<u>C10</u>	<u>C82</u>	<u>C85</u>
$(B_{mn})^2$	5.5e-5	5.6e-5	7.6e-5
$\{(m-n)*B_{mn}\}^2$	1.7e-3	1.7e-3	2.2e-3
wd	5.3e-3	6.3e-3	7.9e-3
w sin d	3.1e-3	2.6e-3	2.9e-3

$$S = 0.85$$



	<u>C10</u>	<u>C82</u>	<u>C85</u>
$(B_{mn})^2$	1.4e-3	2.1e-3	1.2e-3
$\{(m-n) \cdot B_{mn}\}^2$	2.3e-2	4.0e-2	1.7e-2
wd	3.2e-2	5.4e-2	3.2e-2
wsin d	2.1e-2	3.5e-2	1.7e-2