

# Modular Coil Design Improvements

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- Look at variations on present 0907, 1017 modular coils
- Impact of background 1/R field in modular optimization
- Goal is to improve  $I_{mod}/\Delta_{cc,min}$  ( $\sim J_{mod,max}$ ), for comparable field error

# Model

- Specify a set of  $I_{TF}$  values for fixed  $I_{pol}$ 
  - maintain  $I_{TF} + ?I_{mod} = 3I_{pol}$
- Vary winding surface, modular coils and currents  $I_{mod}$
- Include penalty functions for  $?_{cc} = ?_{cc,min}/I_{mod}$ , and  $?_{min}$ , e.g.,

$$p(?_{cc}) = w e^{-?_{cc}}$$

# Reference modular coils

- Reference 1017 is a continuation of modular solution 0907 with coils 3 and 4 extended in R on the outboard side for NBI access
- For  $I_{TF} = 0$ , try varying modular coil currents in optimization

ID #	N?	Nws	I <sub>mod</sub> (kA)	?B <sub>avg</sub> (%)	?B <sub>max</sub> (%)	? <sub>cc,min</sub> (cm)	? <sub>min</sub> (cm)	? <sub>cp,min</sub> (cm)
1017	10	30	-488	0.61	2.61	14.8	12.3	23.3
0105	10	40	$I_1 = -469.7,$ $I_2 = -485.2,$ $I_3 = -494.5,$ $I_4 = -517.8$	0.55	2.85	14.3	11.1	23.0

# Include fixed 1/R field in modular optimization

- Consider  $I_{TF}/I_{mod} < 0$
- Continue 0907 with modified penalty functions, variable modular currents
- Try to improve  $J = ?_{cc,min}/I_{mod,max}$

ID #	$I_{TF}$ (kA)	$I_{mod}$ (kA)	?B <sub>avg</sub> (%)	?B <sub>max</sub> (%)	? <sub>cc,min</sub> (cm) J(kA/cm)	? <sub>min</sub> (cm)	? <sub>cp,min</sub> (cm)
0907	0	-488	0.57	2.55	13.4 (36.4)	11.0	23.2
0122a3	2400*	-600.3, -605.6, -602.8, -599.3	0.63	2.86	19.5 (31.1)	12.4	23.4
0122a2	1500**	-559.3, -563.4, -559.2, -552.8	0.54	2.28	19.4 (29.0)	12.7	22.8

\*  $I_{TF}/3I_{pol} = 0.23$ ,    \*\*  $I_{TF}/3I_{pol} = 0.15$

# Include fixed 1/R field in modular optimization

- Consider  $I_{TF}/I_{mod} > 0$

ID #	$I_{TF}$ (kA)	$I_{mod}$ (kA)	?B <sub>avg</sub> (%)	?B <sub>max</sub> (%)	? <sub>cc,min</sub> (cm) J(kA/cm)	? <sub>min</sub> (cm)	? <sub>cp,min</sub> (cm)
0907	0	-488	0.57	2.55	13.4 (36.4)	11.0	23.2
0118b2	-2400	-383.1, -376.4, -379.2, -339.4	0.60	2.77	15.1 (25.3)	10.7	19.9
0124a1	-1500	-420.6, -421.7, -417.1, -397.8	0.51	2.33	15.9 (26.5)	10.2	21.4
0126a1	-1350	-425.3, -428.8, -425.9, -406.8	0.50	2.30	16.2 (26.5)	10.2	21.5
0126a2	-1650	-412.5, -414.3, -411.9, -389.5	0.51	2.30	15.5 (26.7)	9.8	21.3

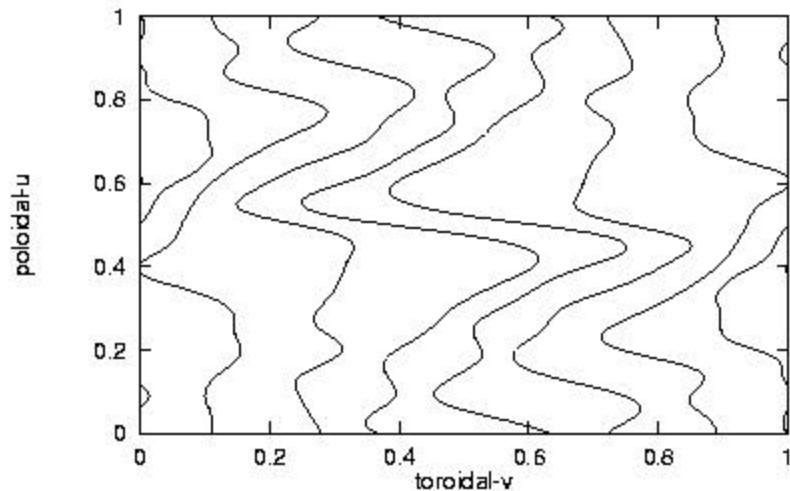
## Extend modular coils 3 and 4 for NBI access

- Continue cases 0122a2 ( $I_{TF}/I_{mod} < 0$ ) and 0124a1 ( $I_{TF}/I_{mod} > 0$ )

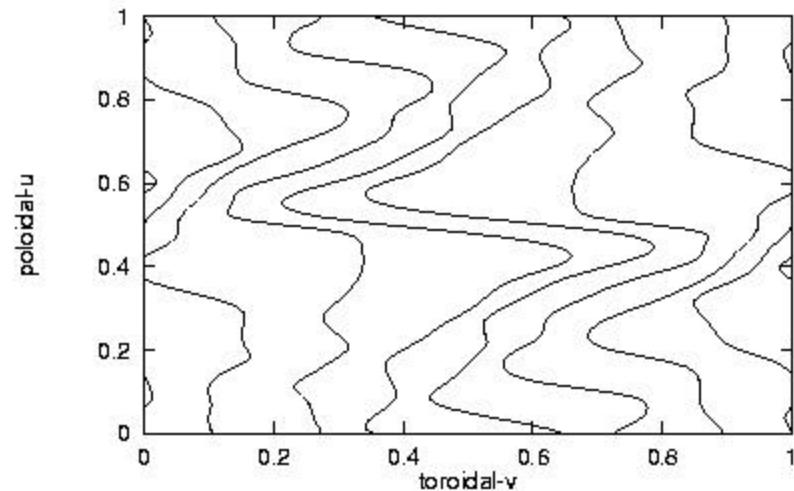
ID #	$I_{TF}$ (kA)	$I_{mod}$ (kA)	? $B_{avg}$ (%)	? $B_{max}$ (%)	? <sub>cc,min</sub> (cm) J(kA/cm)	$L_1,$ $L_{avg}$ (m)	? <sub>min</sub> (cm)	? <sub>cp,min</sub> (cm)
0105	0	-469.7, -485.2, -494.5, -517.8	0.55	2.85	14.3 (36.2)	7.38, 8.01	11.1	23.0
0123a1	1500	-546.1, -552.5, -567.6, -584.3	0.60	2.24	19.8 (29.5)	7.39, 8.03	12.4	22.5
0125a1	-1500	-407.0, -412.7, -432.3, -412.6	0.53	2.68	15.7 (27.5)	7.59, 8.10	9.3	21.4

## Effect of background 1/R field on toroidal variation of modularity for cases with coils 3 and 4 extended in radius

0123a1 ( $I_{TF}/I_{mod} < 0$ )



0125a1 ( $I_{TF}/I_{mod} > 0$ )



# Summary

- Improvements in modular coil current density and field errors are possible by prescribing a  $1/R$  background field in modular optimization.
- Next – find the optimal  $1/R$  field.