

The ARIES Compact Stellarator Study: Introduction & Overview

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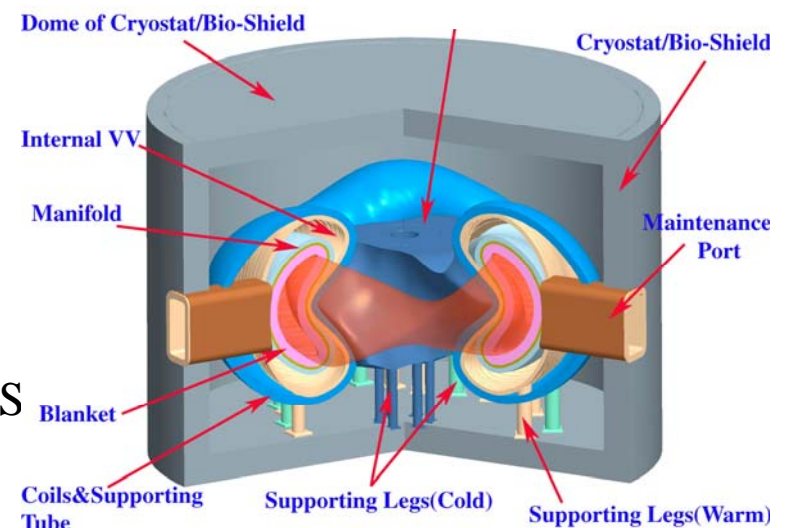
ARIES-CS Review Meeting

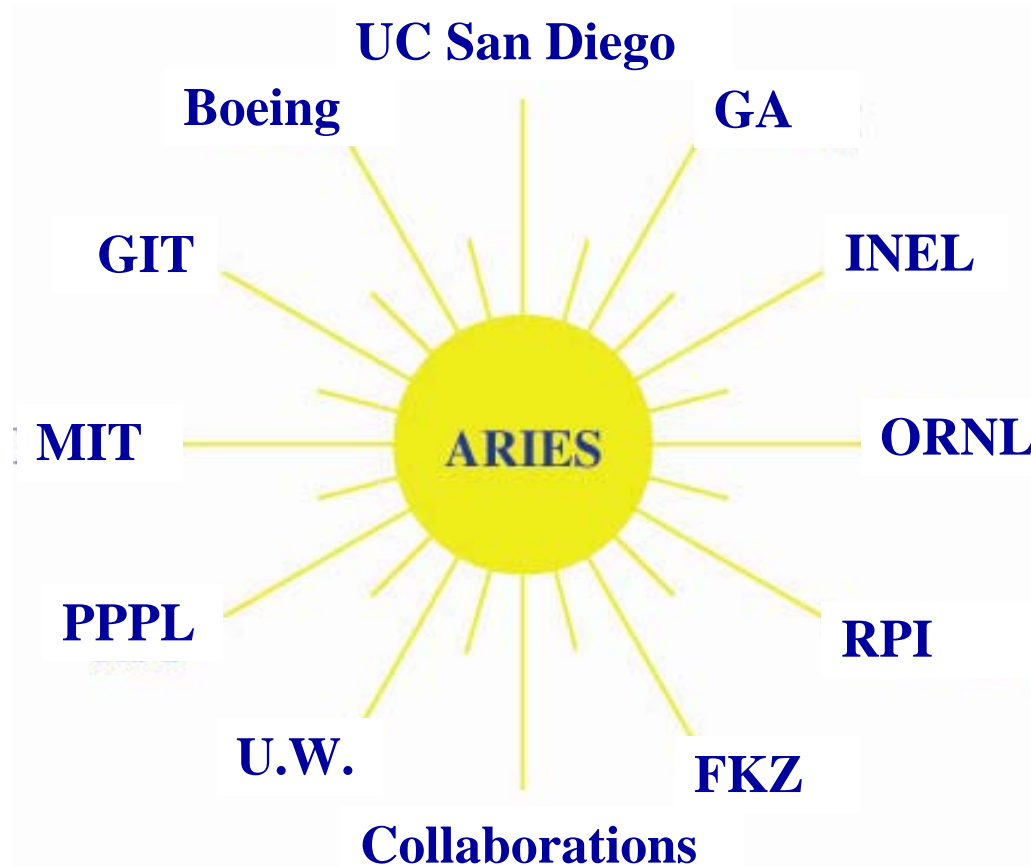
October 5, 2006

PPPL, Princeton, NJ

Electronic copy: <http://aries.ucsd.edu/najmabadi/TALKS>

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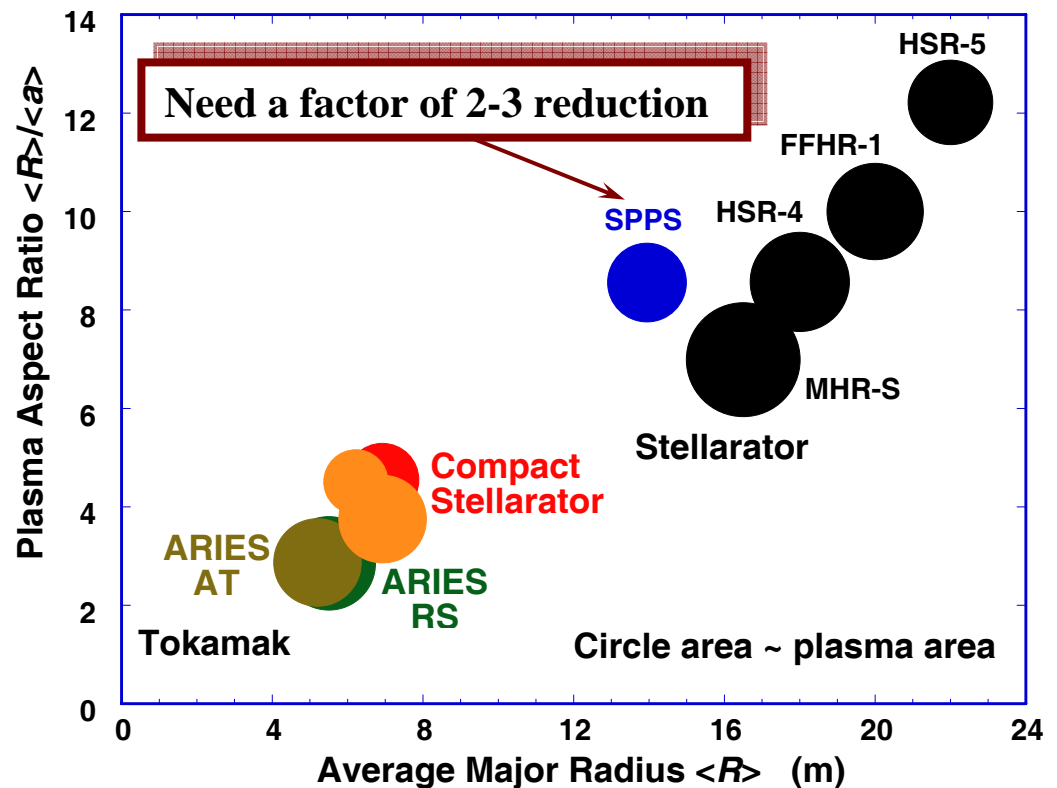
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Goals of the ARIES-CS Study

- Can compact stellarator power plants be similar in size to advanced tokamak power plants?
 - ✓ Reduce aspect ratio while maintaining “good” stellarator properties.
 - ✓ Include relevant power plants issues (α particle loss, Divertor, Practical coils).
 - ✓ Identify key areas for R&D (what areas make a big difference)
- Impact of complex shape and geometry
 - ✓ Configuration, assembly, and maintenance drives the design
 - ✓ Complexity-driven constraints (e.g., superconducting magnets)
 - ✓ Complex 3-D analysis (e.g., CAD/MCNP interface for 3-D neutronics)
 - ✓ Manufacturability (feasibility and Cost)
- First design of a compact stellarator power plant
 - ✓ Design is pushed in many areas to uncover difficulties

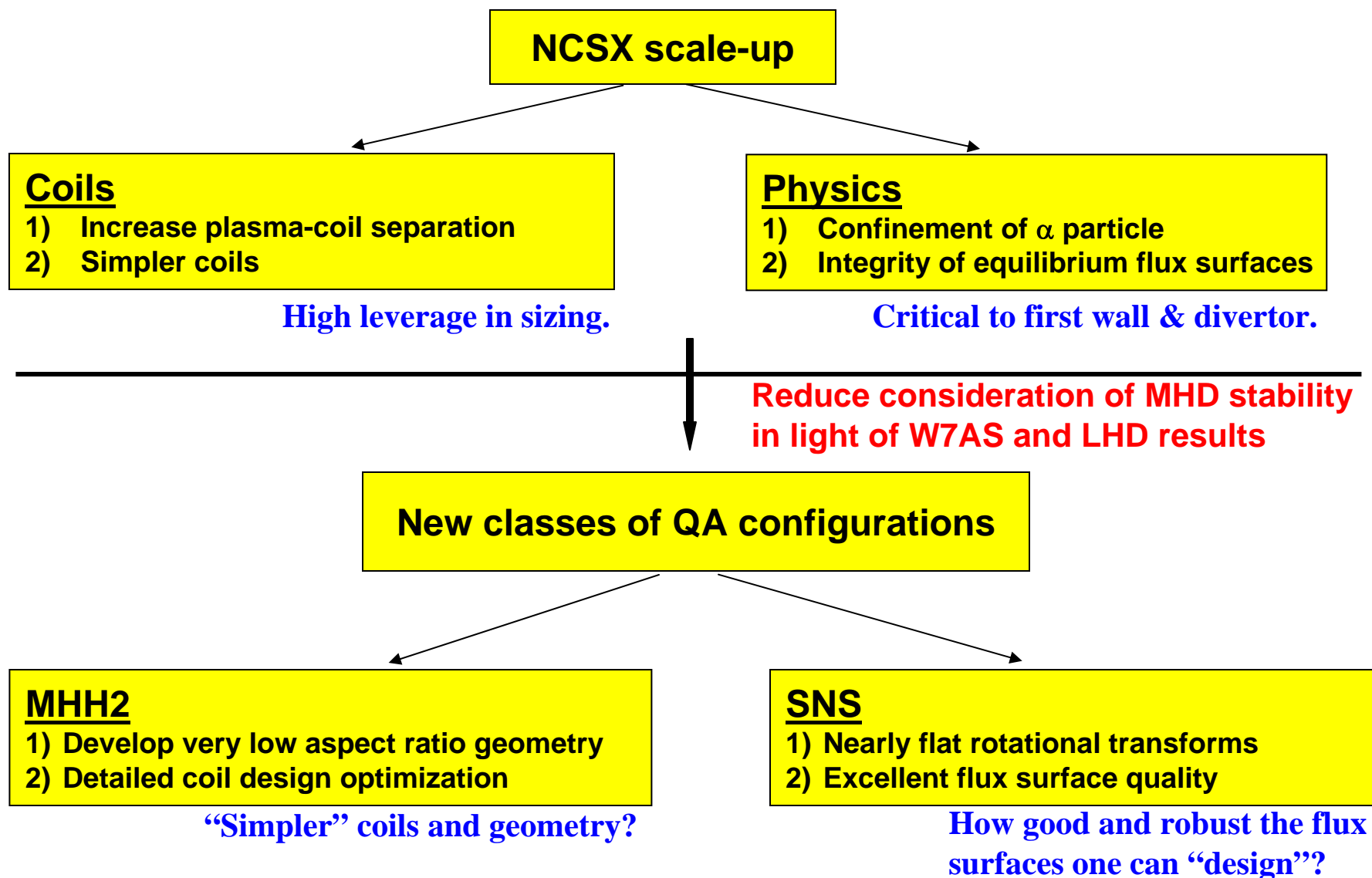
Goal: Stellarator Power Plants Similar in Size to Tokamak Power Plants

- Multipolar external field -> coils close to the plasma
- First wall/blanket/shield set a minimum plasma/coil distance (~2m)
↓
- A minimum minor radius
- Large aspect ratio leads to large size.

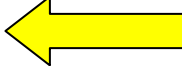


- Approach:
 - ✓ **Physics:** Reduce aspect ratio while maintaining “good” stellarator properties.
 - ✓ **Engineering:** Reduce the required minimum coil-plasma distance.

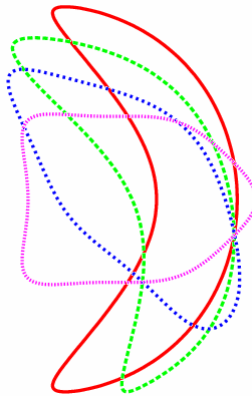
Physics Optimization Approach



Optimization of NCSX-Like Configurations: Increasing Plasma-Coil Separation

- ✓ A series of coil design with $A_c = \langle R \rangle / \Delta_{\min}$ ranging 6.8 to 5.7 produced.
- ✓ Large increases in B_{\max} only for $A_c < 6$.
- ✓ α energy loss is large $\sim 18\%$. 

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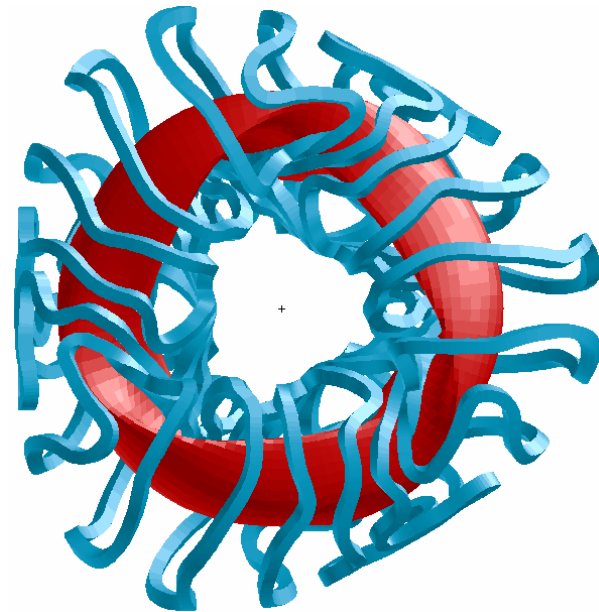
$$A_c = 5.9$$

For $\langle R \rangle = 8.25\text{m}$:

$$\Delta_{\min}(\text{c-p}) = 1.4\text{ m}$$

$$\Delta_{\min}(\text{c-c}) = 0.83\text{ m}$$

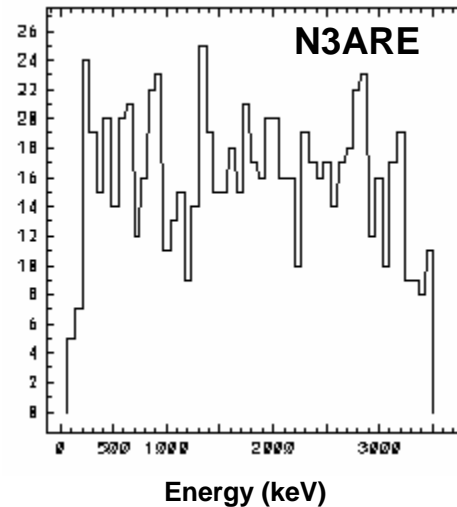
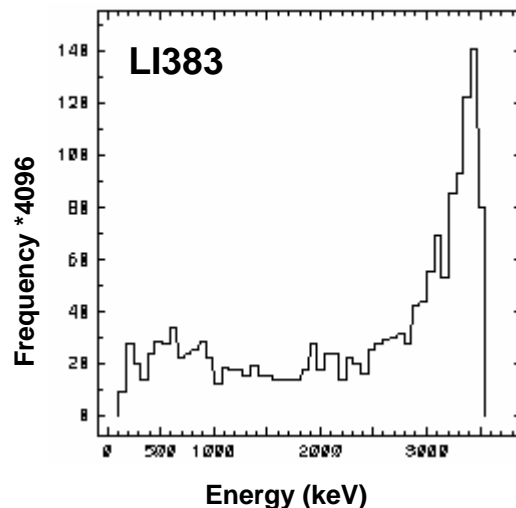
$$I_{\max} = 16.4\text{ MA @ } 6.5\text{T}$$



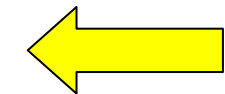
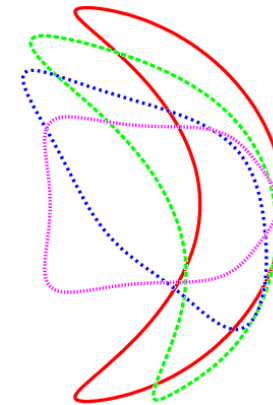
Optimization of NCSX-Like Configurations: Improving α Confinement & Flux Surface Quality

A bias is introduced in the magnetic spectrum in favor of B(0,1) and B(1,1)

- ✓ A substantial reduction in α loss (to $\sim 3.4\%$) is achieved.



N3ARE



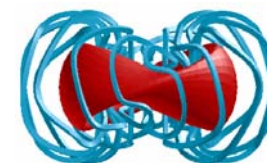
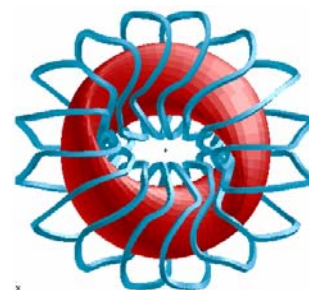
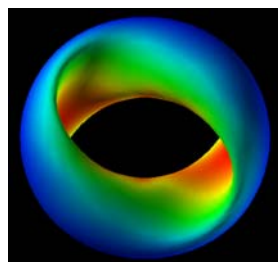
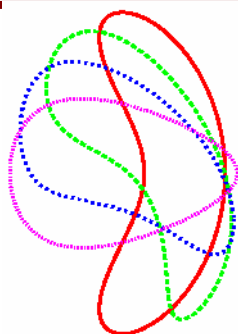
**Baseline
Configuration**

- ✓ The external kinks and infinite-n ballooning modes are marginally stable at 4% β with no nearby conducting wall.
- ✓ Rotational transform is similar to NCSX, so the same quality of equilibrium flux surface is expected.

Two New Classes of QA Configurations

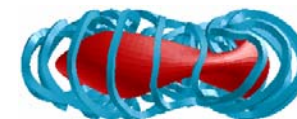
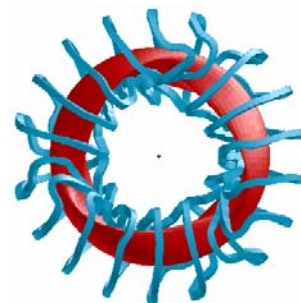
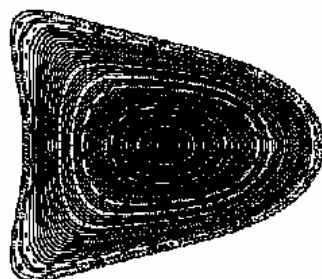
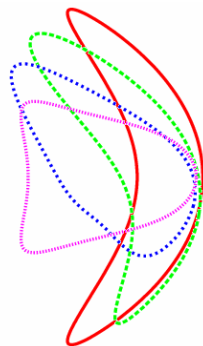
II. MHH2

- ✓ Low plasma aspect ratio ($A_p \sim 2.5$) in 2 field period.
- ✓ Excellent QA, low effective ripple ($< 0.8\%$), low α energy loss ($\leq 5\%$).

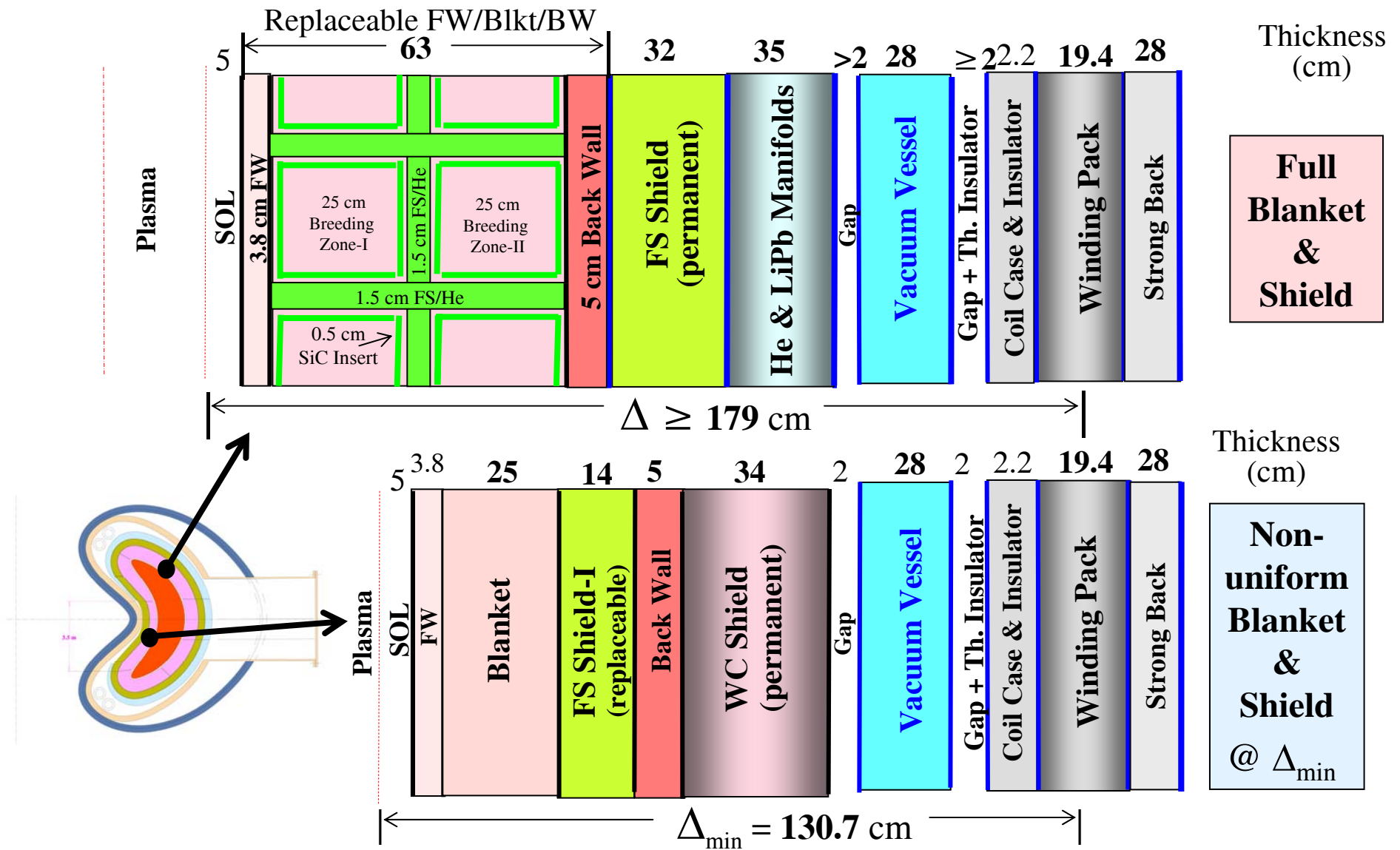


III. SNS

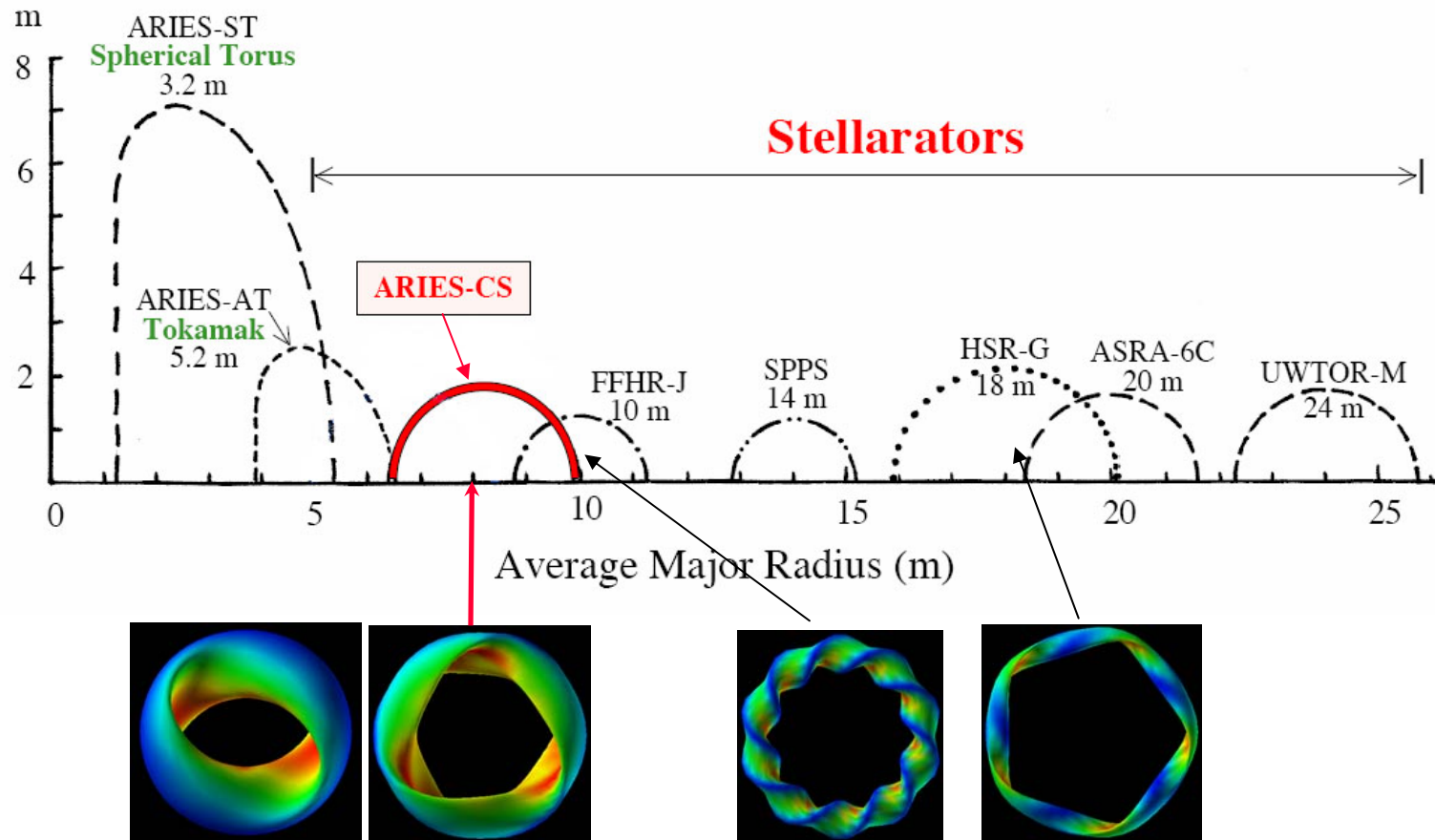
- ✓ $A_p \sim 6.0$ in 3 field period. Good QA, low ϵ -eff ($< 0.4\%$), α loss $\leq 8\%$.
- ✓ Low shear rotational transform at high β , avoiding low order resonances.



Minimum Coil-plasma Stand-off Can Be Reduced By Using Tapered-Blanket Zones



Resulting power plants have similar size as Advanced Tokamak designs

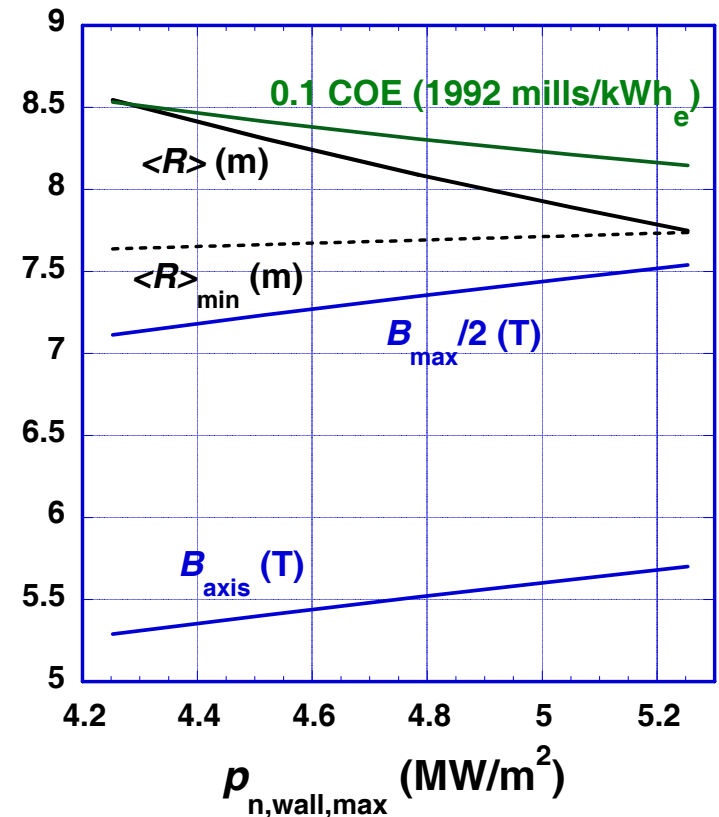


- Trade-off between good stellarator properties (steady-state, no disruption, no feedback stabilization) and complexity of components.
- Complex interaction of Physics/Engineering constraints.

Resulting power plants have similar size as Advanced Tokamak designs

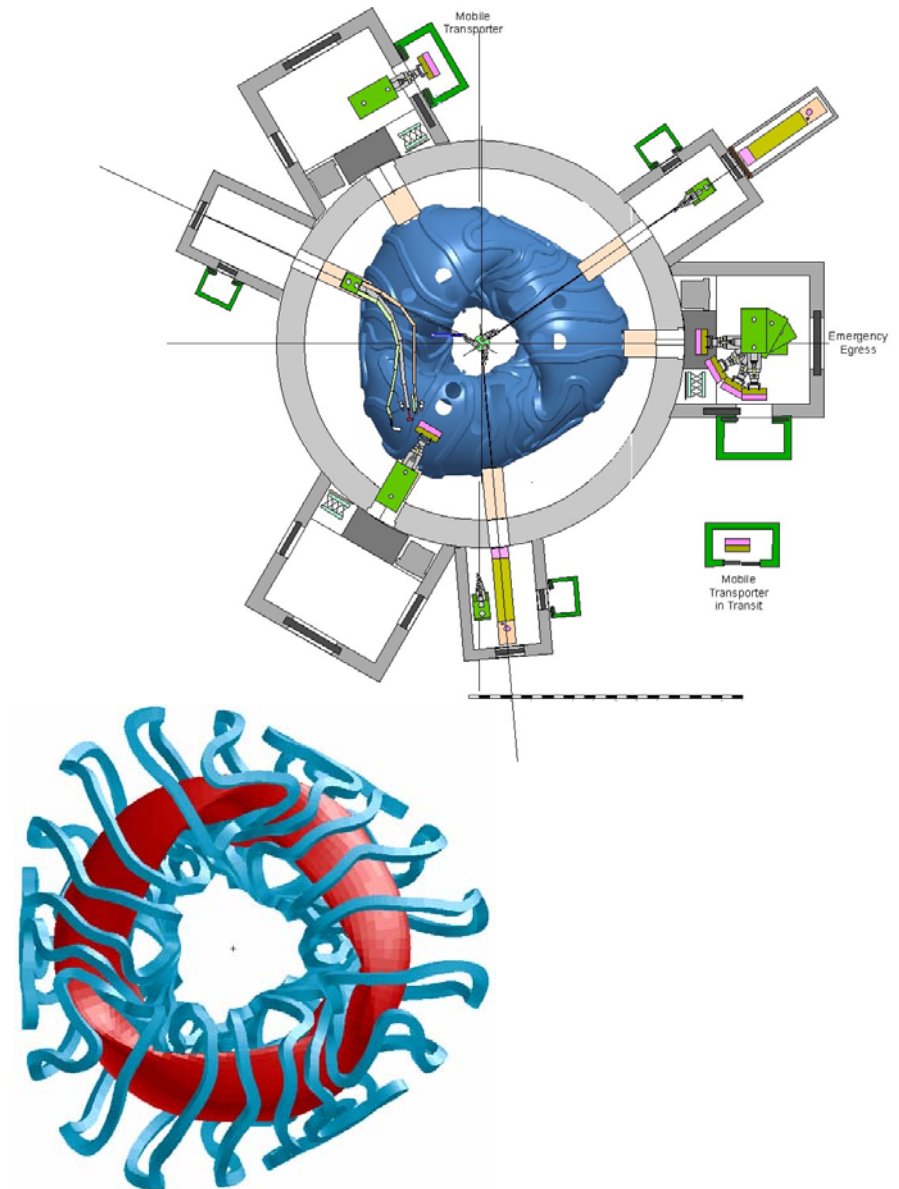
	SPPS	ARIES-CS	ARIES-AT	ARIES-RS
$\langle R \rangle$, m	14.0	7.75	5.2	5.5
$\langle B_0 \rangle$, T	5.0	5.7	5.9	8.0
$\langle \beta \rangle$	5.0%	5.0%	9.2%	5.0%
FPC Mass, tonnes	21,430	10,962	5,226	12,679
Reactor Plant Equip. (M\$)		1,642	900	1,386
Total Direct Cost (M\$)		2,633	1,757	2,189

- Major radius can be increased to ease engineering difficulties with a small cost penalty.



Basic Parameters of ARIES-CS

Major radius	7.75 m
Minor radius	1.7 m
Aspect ratio	4.5
Average plasma density	$3.6 \times 10^{20}/\text{m}^3$
Average Temperature	5.7 keV
β	5.0 %
B_o	5.7 T
B_{max}	15.1 T
Fusion power	2.4 GW
Avg./max. wall load	2.6/5.3 MW/m ²
Alpha loss	5 %
TBR	1.1

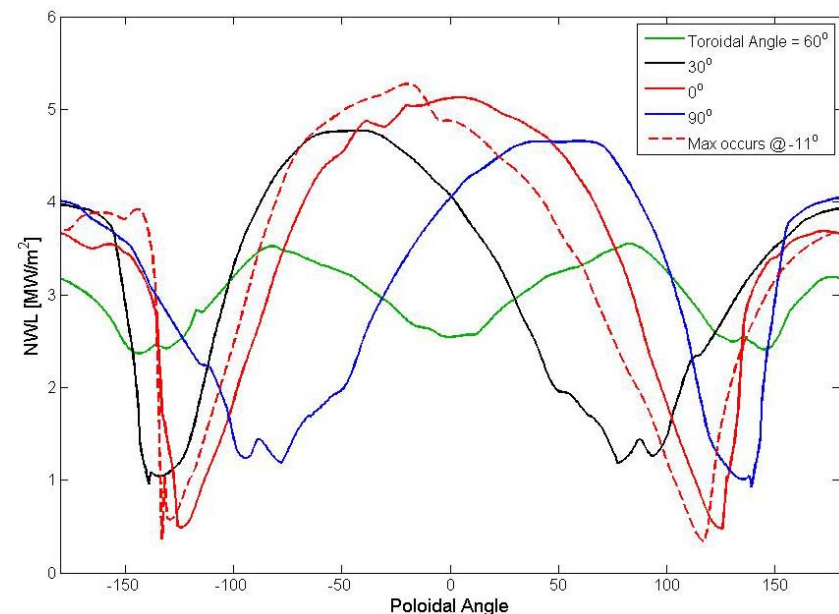
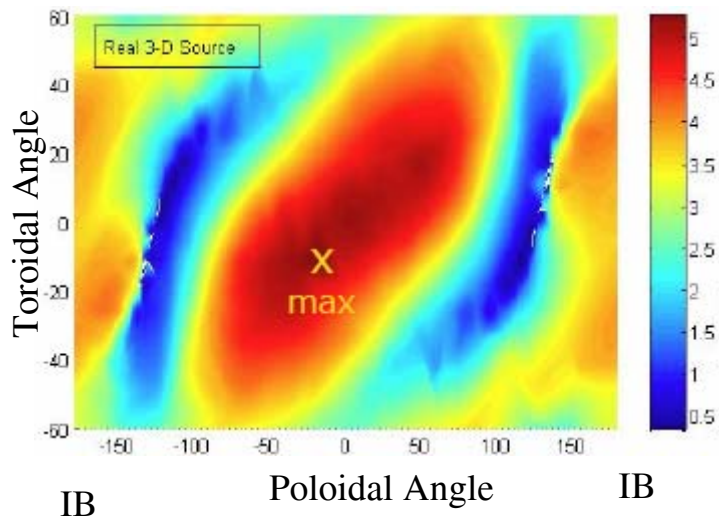


**Complex plasma shape and plasma-coil
relative position drives many engineering
systems**

First ever 3-D modeling of complex stellarator geometry for nuclear assessment using CAD/MCNP coupling

- Detailed and complex 3-D analysis is required for the design
 - ✓ Example: Complex plasma shape leads to a large non-uniformity in the loads (e.g., peak to average neutron wall load of 2).

Distribution of Neutron wall load



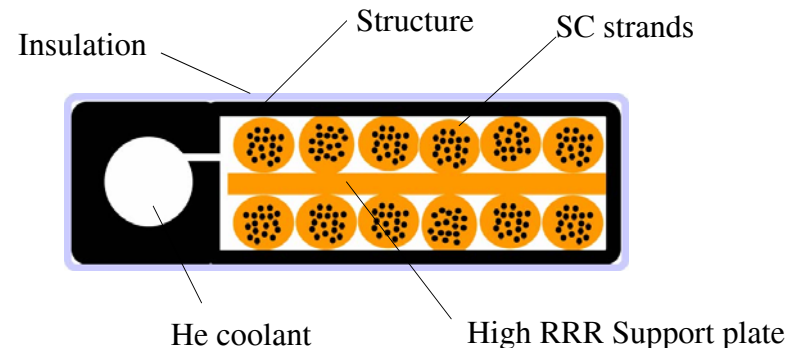
Coil Complexity Impacts the Choice of Superconducting Material

- Strains required during winding process is too large.
 - ✓ NbTi-like (at 4K) $\Rightarrow B < \sim 7\text{-}8\text{ T}$
 - ✓ NbTi-like (at 2K) $\Rightarrow B < 9\text{ T}$, problem with temperature margin
 - ✓ Nb₃Sn $\Rightarrow B < 16\text{ T}$, Conventional technique does not work because of inorganic insulators

Option 1: Inorganic insulation, assembled with magnet prior to winding and capable to withstand the heat treatment process.



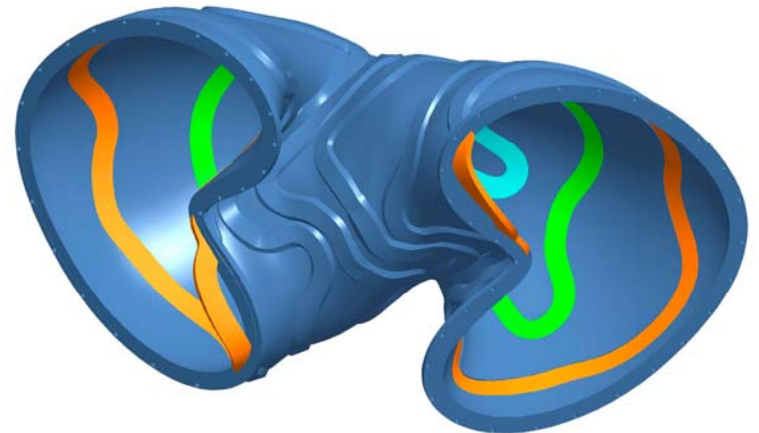
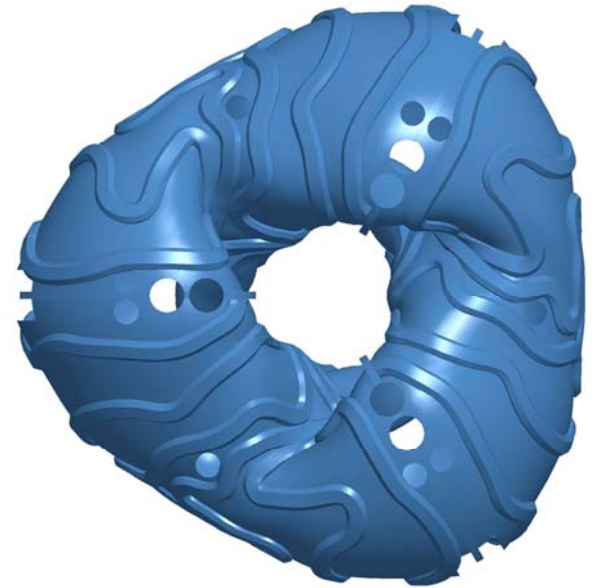
Option 2: conductor with thin cross section to get low strain during winding. (Low conductor current, internal dump).



Option 3: HTS (YBCO), Superconductor directly deposited on structure.

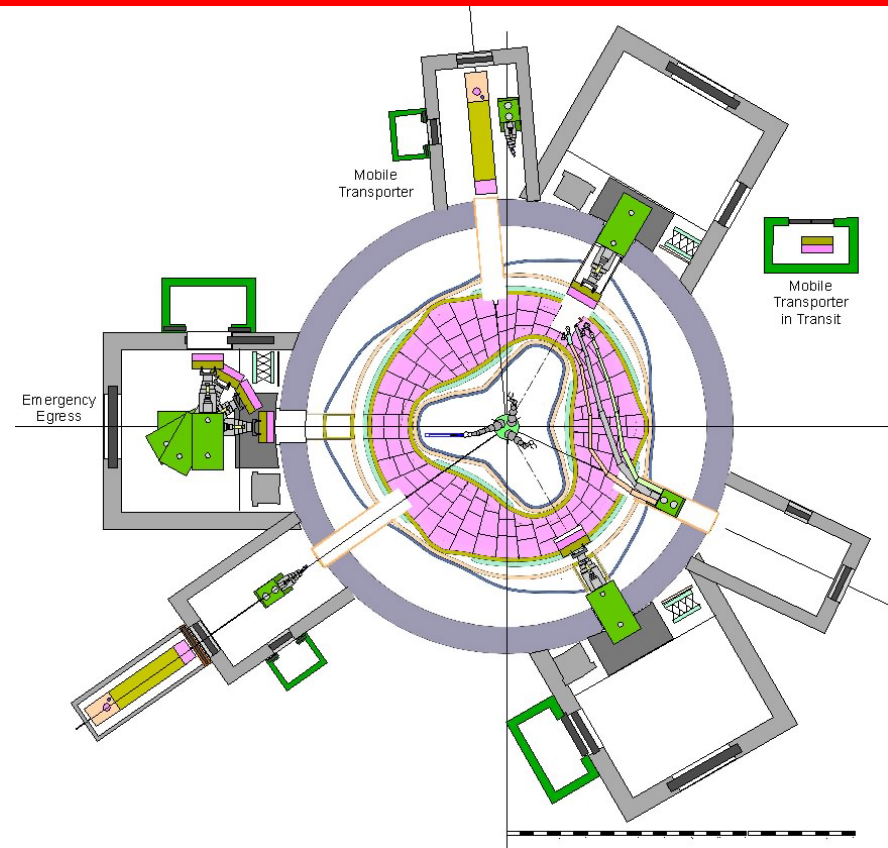
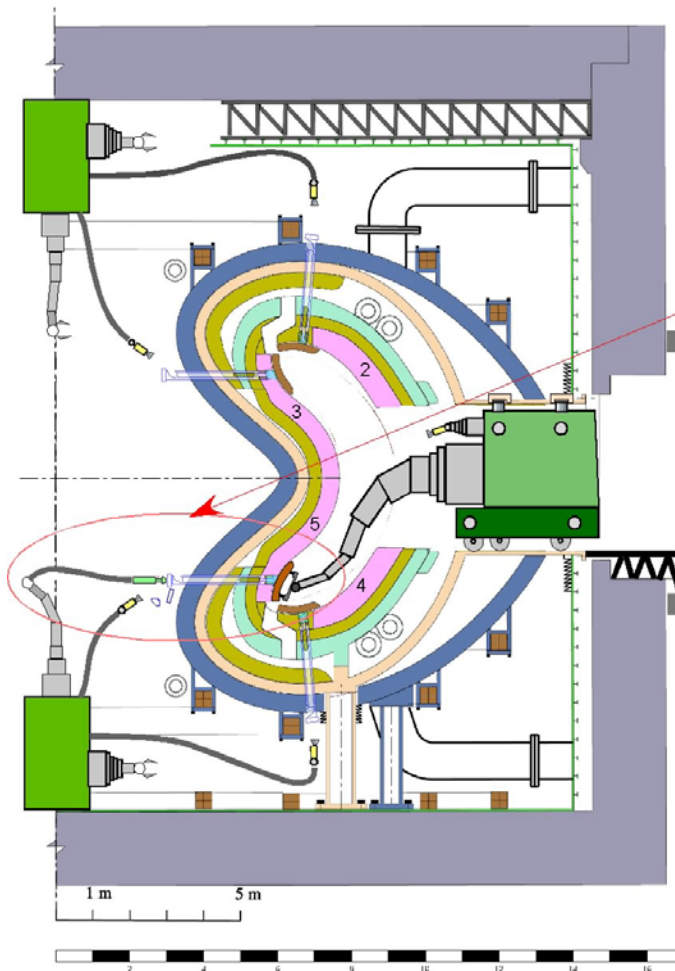
Coil Complexity Dictates Choice of Magnet Support Structure

- It appears that a continuous structure is best option for supporting magnetic forces.
- Superconductor coils wound into grooves inside the structure.
- Net force balance between field periods.
- Absence of disruptions reduces demand on coil structure.



Port Assembly: Components are replaced Through Ports

- Modules removed through three ports using an articulated boom.

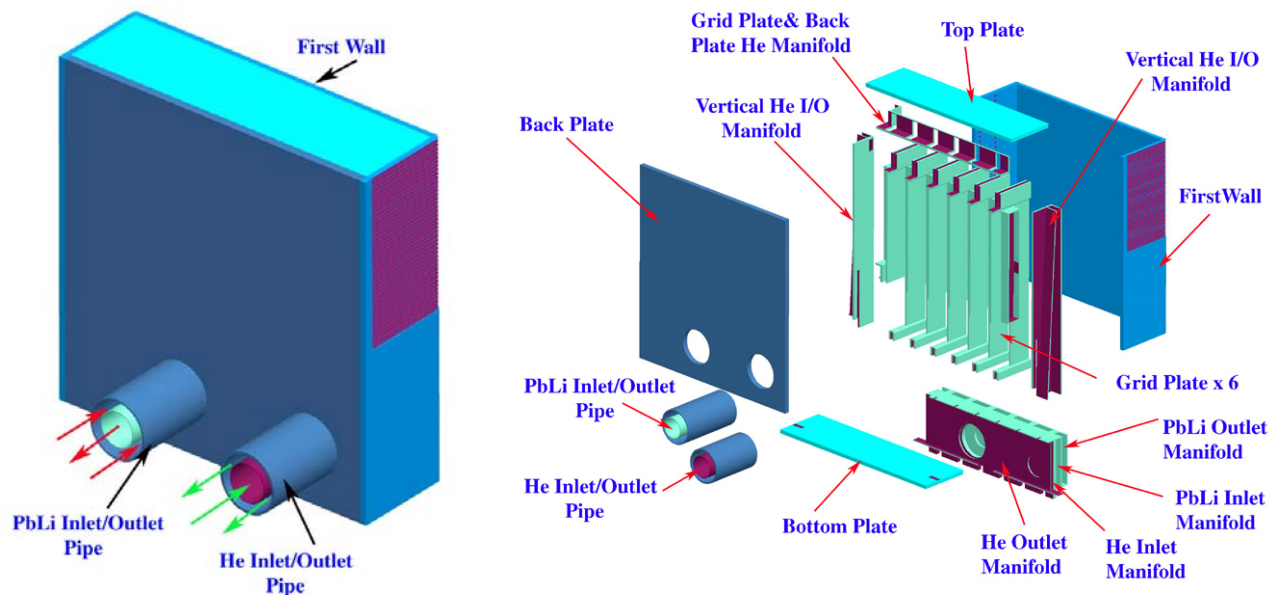


Drawbacks:

- ✓ Coolant manifolds increases plasma-coil distance.
- ✓ Very complex manifolds and joints
- ✓ Large number of connect/disconnects

Blanket Concepts are Optimized for Stellarator Geometry

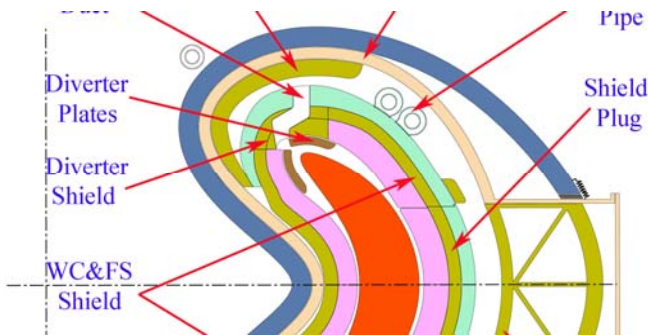
- Dual coolant with a self-cooled PbLi zone and He-cooled RAFS structure
 - ✓ Originally developed for ARIES-ST, further developed by EU (FZK), now is considered as ITER test module
 - ✓ SiC insulator lining PbLi channel for thermal and electrical insulation allows a LiPb outlet temperature higher than RAFS maximum temperature



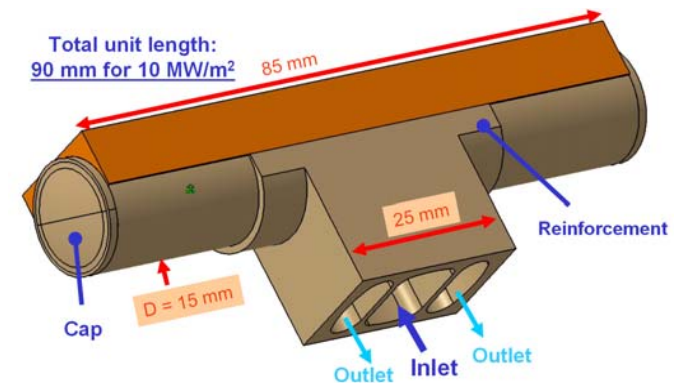
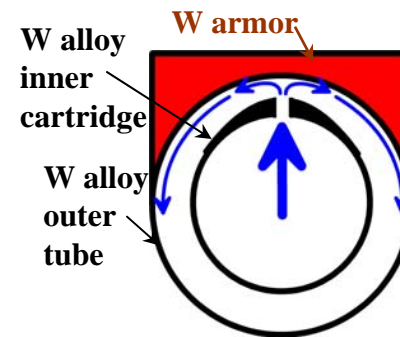
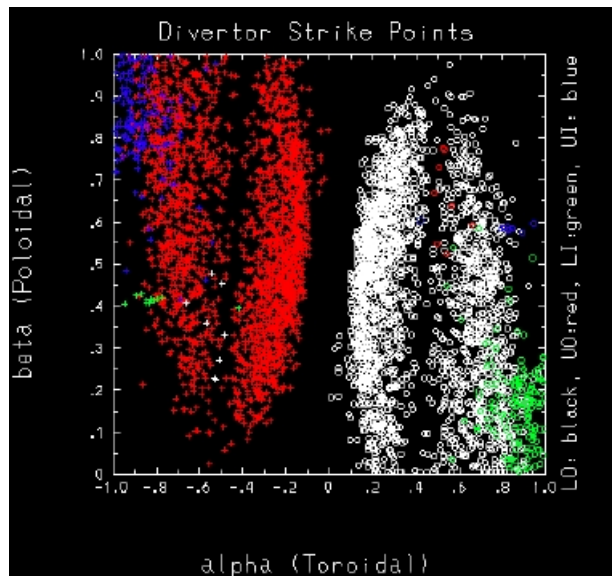
- Self-cooled PbLi with SiC composite structure (as in ARIES-AT)
 - ✓ Higher-risk high-payoff option

A highly radiative core is needed for divertor operation

- Heat/particle flux on divertor was computed by following field lines outside LCMS.
 - ✓ Because of 3-D nature of magnetic topology, location & shaping of divertor plates require considerable iterative analysis.



Top and bottom plate location with toroidal coverage from -25° to 25° .



- Divertor module is based on W Cap design (FZK) extended to mid-size (~ 10 cm) with a capability of 10 MW/m^2

Summary of the ARIES-CS Study

Goal 1: Can compact stellarator power plants similar in size to advanced tokamak power plants?

- Reduce aspect ratio while maintaining “good” stellarator properties.
- Include relevant power plants issues (α particle loss, divertor, practical coils).
- Identify key areas for R&D (what areas make a big difference)

Results:

- ✓ Compact stellarator power plants can be similar in size to advanced tokamaks (The best “size” parameter is the mass not the major radius).
- ✓ α particle loss can be reduced substantially (how low is low enough?)
- ✓ A large number of QA configurations, more desirable configurations are possible. In particular, mechanism for β limit is not known. Relaxing criteria for linear MHD stability may lead to configurations with a less complex geometry or coils.

Summary of the ARIES-CS Study

Goal 2: Understand the impact of complex shape and geometry

A. Configuration, assembly, and maintenance drives the design

- ✓ A high degree of integration is required
- ✓ Component replacement through ports appears to be the only viable method.
- ✓ Leads to modules that can be fitted through the port and supported by articulated booms.
- ✓ Large coolant manifold (increase radial build), large number of connects and disconnects, complicated component design for assembly disassembly.

B. Complexity-driven constraints (e.g., superconducting magnets)

- ✓ Options were identified. Base case requires development of inorganic insulators.

Summary of the ARIES-CS Study

Goal 2: Understand the impact of complex shape and geometry

C. Complex 3-D analysis

- ✓ 3-D analysis is required for almost all cases (not performed in each case).
- ✓ CAD/MCNP interface for 3-D neutronics, 3-D solid model for magnet support, ...

D. Manufacturability (feasibility and Cost)

- ✓ Feasibility of manufacturing of component has been included in the design as much as possible.
- ✓ In a large number of cases, manufacturing is challenging and/or very expensive.

Exploration and Optimization of Compact Stellarators as Power Plants -- Motivations

Timeliness:

- Initiation of NCSX and QPS experiments in US; PE experiments in Japan (LHD) and Germany (W7X under construction).
- Progress in our theoretical understanding, new experimental results, and development of a host of sophisticated physics tools.

Benefits:

- Such a study will advance physics and technology of compact stellarator concept and addresses concept attractiveness issues that are best addressed in the context of power plant studies, *e.g.*,
 - ✓ α particle loss
 - ✓ Divertor (location, particle and energy distribution and management)
 - ✓ Practical coil configurations.
- NCSX and QPS plasma/coil configurations are optimized for most flexibility for scientific investigations at PoP scale. Optimum plasma/coil configuration for a power plant (or even a PE experiment) will be different. Identification of such optimum configuration will help define key R&D for compact stellarator research program.