

NCSX Half Period Assembly Dimensional Control Assessment

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Presentation Overview



- NCSX HPA Dimensional Control Overview
- Status of HPA Dimensional Control Performance
- Measurement Techniques and Uncertainties
- Possible Improvements
- Note: much thought and insight, from a number of individuals and sources, has gone into this process over the last year. There is easily enough information to warrant a ~4 hour discussion; we have less than one hour here. If necessary or desired, I am willing to go into much more detail, with those interested, at another time. At this meeting I will need to skim over some details in order to give the overview.

The Current Center of a Modular Coil Winding is to be Positioned within 1.5mm [.06in] of its Theoretical Position

National Compact Stellarator Experiment

- This goal results from a limitation on toroidal flux in island regions.
- This tolerance applies at the end of machine assembly.
- To understand this goal, consider that the actual coil current center is a filament in space.
- Now, consider that this filament is 3mm [.12in] thick.
- Consider that the theoretical coil current center is an infinitely thin filament in space.
- When NCSX is assembled within tolerance, the filament representing the theoretical current center will lie within the 3mm thick filament representing the actual winding.
- The tolerance budget is divided between major assembly steps.
- 0.5mm [.02in] is allocated to half period assembly.

After Coil Fabrication, the Windings Cannot be Measured Directly



- The coil winding is a bundle of conductors that is wound into a "box" defined by the winding form and clamps.
- Clamps are adjusted, based on winding measurements, to position the current center accurately.
- A set of monuments ("conical seats") relate points on the MCWF to the HPA global coordinate system.
 - These monuments are used to relate the measurement equipment (Romer Arm) to the HPA global coordinate system.
- After coil winding and VPI is complete, the conductor/insulation surface is no longer accessible.
 - Measure the coil windings indirectly by measuring monuments.
 - "If the monuments are in their theoritical positions in the HPA coordinate system, then the coil current centers also occupy their theoretical positions." (within acceptable tolerance.

The Validity of Indirect Measurements of Coil Current Centers Depends on Several Assumptions and Parameters



- Measurement accuracy during winding.
- Deviations during winding.
- No movement of windings after lacing.
- No distortion during VPI and curing.

For This Discussion, "Perfect Modular Coils" are Assumed



- A "Perfect Modular Coil" is one for which, if all of the monuments are in their theoretical positions in the HPA global coordinate system, the coil current centers are on their theoretical path.
- We are making this assumption for two primary reasons:
 - It is felt that "tolerance recovery" by means of coil realignment will make this assumption valid.
 - GHN direction to use this assumption as a starting point, and focus exclusively on half period assembly issues.
- Applying our philosophy of indirect measurement, our dimensional control goal for half period assembly is that the position of every monument on the half period shall be within 0.5mm [.020"] of its theoretical position.

HPA Dimensional Control Covers the Following Major Assembly Steps



- Preparation of coils for Half Period Assembly.
- Positioning and installing the "A" coil in the HPA global coordinate system.
- Positioning and installing the "B" coil in the HPA global coordinate system.
 - We are here with B1.
- Positioning and installing the "C" coil in the HPA global coordinate system.

Preparing the Coils for HPA Requires Alignment, Measurement, and "Realignment"



- The external coil monuments ("tooling balls") must be related to the winding monuments ("conical seats")
 - Not achieved satisfactorily prior to winding.
 - Conical seats become inaccessible during assembly.
 - Must manage coil deformation.
 - Align to conical seats to establish coordinate system, then measure tooling balls.
- Pre-measurement of tooling balls and flanges.
 - Establish tooling ball coordinates for all future assembly steps.
 - Measure flanges for pre-calculation of shims.
- Coil "realignment"
 - Rigid body transformation of measured points (tooling balls and flanges) to recover winding tolerances.
 - A mathematical process.

Align the Laser Tracker to the Conical Seats, Measure Tooling Balls and Flanges



- The quality of the alignment is critical to the success of this step.
 - What is an alignment?
 - What does it mean?
- The modular coils can deform significantly as a function of their supports.
 - Winding fixture (vertical, bolted)
 - HPA assembly position (horizontal)
- Before pre-measurement, a modular coil must be twisted, or "racked", into its as-wound shape to the extent possible.
 - Adjustments normal to flange
 - Gravity load of one coil
 - .005" RMS deviation on alignment to conical seats. (ALARA)

What is an Alignment?



- Align laser tracker / software coordinate system to the coordinate system of interest.
- Align to a set of monuments and their known coordinates.
 - "Best fit"
- Alignment deviations are ulletdue to measurement error and actual deviations of monuments.

Verisurf Alignment Report

	030907 A1 O
Part Name:	WEDGE-AA
Alignment Name:	Auto Align
Coord System:	WORLD
Date:	

Fit Results

3/9/2007

Name	DX	DY	DZ	3D
OD Datast 4	0.000	0.014	0.044	0.000
3D Point 1	0.009	-0.014	0.011	0.020
3D Point 2	0	-0.003	0.012	0.013
3D Point 3	-0.002	-0.004	-0.004	0.006
3D Point 4	-0.004	-0.003	-0.011	0.012
3D Point 5	-0.005	-0.003	-0.008	0.010
3D Point 6	-0.005	0.008	0.015	0.017
3D Point 7	-0.005	0.007	0.012	0.014
3D Point 8	0.007	0.007	-0.016	0.019
3D Point 9	0.005	0.005	-0.01	0.012
				0.0143

Fit Summary

Total Points: 9	DX	DY	DZ	3D	
Maximum Deviation:	0.009	0.008	0.015	0.020	
Minimum Deviation:	-0.005	-0.014	-0.016	0.006	
Deviation Range:	0.014	0.022	0.03	0.014	
Average Deviation:	0	0	0	0.014	
RMS Deviation:	0.005	0.007	0.012	0.014	0.014
Standard Deviation:	0.006	0.007	0.012	0.004	

Transformation

	Х	Y	Z
Translation:	-43.521	100.198	89.243
Matrix I:	-0.205	0.976	0.076
Matrix J:	-0.916	-0.218	0.335
Matrix K:	0.344	-0.001	0.939

RMS Deviation is a Good Indicator of the Quality of an Alignment



- Usually gives a conservative estimate of deviations.
- Exceptional measurements can yield deceptively good results.
 - Not likely to happen.
- An alignment to a coil should be representative of the coil.
 - Operator judgment is required.
- To zero order, the RMS deviation indicates the positional accuracy of a point on the MCWF.

point	dx	dy	dz	3D
1	0.012	0.000	0.000	0.012
2	-0.003	0.000	0.000	0.003
3	-0.003	0.000	0.000	0.003
4	-0.003	0.000	0.000	0.003
5	-0.003	0.000	0.000	0.003
Average	0.000	0.000	0.000	0.005
RMS	0.006	0	0	0.006
Standard	0.007	0.000	0.000	0.004



- When taken from the winding fixture and placed horizontally, the modular coils can distort several times the magnitude of our tolerance goal.
- We have developed a procedure to adjust the deformations normal to the flanges so that the positioning of the conical seats in this direction matches the positioning as measured relative to a flange datum during winding.
 - Deformations in plane parallel to flanges cannot, practically, be changed.
 - Mathematical logic of racking procedure is presented in HPA DCP.
 - Proven in practice.
 - RMS deviation of alignment, and analysis of z-deviations in alignment report, indicates quality of racking.
- "A" coils are racked to begin HPA; proper shims maintain shape of "B" and "C" coils.

Some Self-Checking is Inherently Part of the Racking Procedure



- Laser measurements are used to determine adjustments.
- Adjustments are measured using dial indicators.
- Process converges to within ~.001"-.002"
 - Accuracy of convergence is limited by stiffness of the coil as well as measurement uncertainty.

Pre-Measurement of Flanges and Monuments Follows Alignment



- Establish a network of global monuments attached to building.
 - Use for relocating laser tracker.
 - Use for resuming work after equipment is powered down overnight or inadvertently bumped.
- Alignment criterion for global monuments is .002" RMS deviation.
- Measure all monuments.
 - Multiple laser positions.
- Scan the appropriate flange.

Half Period Assembly Begins with Positioning the "A" Coil into the HPA Global Coordinate System



- First rack coil to assure correct shape.
- Now racking to tooling balls → tighter alignment criterion of .003"RMS
- Why did we rack and pre-measure the "A" coil once when we will need to rack it again?
 - To bank progress already made.
 - To take that pressure off of critical path HPA assembly.
- Second align to the "A" coil tooling balls to establish the HPA global coordinate system.
- Why are we aligning to the "A" coil when we have spoken of positioning the coil into the HPA global coordinate system?
 - Kinematic inversion it is easier, and equivalent, to mathematically position the coordinate system onto the coil than to physically move the coil into the coordinate system.
 - We do not have this luxury on "B" and "C" coils.

Next, the "B" Coil is Added [We are here]



- Shims establish shape of coil and positioning in direction normal to A-B interface.
- Measure monuments on coil to verify opportunity to correct shim thicknesses.
- Alignment calculator used for positioning "B" coil in plane of A-B interface.
- Initial shim weld → position "B" coil, torque bolts, measure, final shim weld, measure.
- Accuracy goal is .012" deviation of monuments from theoretical position.
- How did we do?
 - 78 monuments measured, 2 outliers [.014", .015"]

number of nominals = 100

HP1_postfill_dxyza.txt number measured = 78

locations in half no	riod coordinato system	
xmeas ymeas zm	eas xnsrt vnsrt znsrt	-
13 721 10 652 -8	191 13 724 10 650 -8 180)
22733 -9454 -0	954 22 738 _9 456 _0 951	ĺ
15 381 -16 724 -11	801 15 389 -16 728 -11 790	5
18 7/9 _36 737 _0	964 18 751 _36 742 _0 954	í
20745 50000	954 10.751 -50.742 -0.754	r N
29.743 -30.929 -0.	770 29 745 44 028 5 767	,
20.740 - 44.930 - 5.	<i>110</i> 20.745 -44.950 -5.707 <i>162</i> 28 7 <i>1</i> 8 <i>-16 1</i> 00 <i>-</i> 9 <i>16</i> 1	
25,747 = 40.373 = 7.	306 25 768 $_{12}$ 521 $_{-10}$ 303	2
<i>A</i> 5 809 -53 <i>A</i> 28 -17	608 45 812 -53 432 -17 606	,
$31 \ 0.09 \ -35 \ 416 \ -24$	903 31 014 _35 418 _24 894	, ,
40 500 -43 366 -24	811 40 504 -43 374 -24 811	ĺ
50 978 -40 682 -36	111 50 982 -40 685 -36 109)
59.449 -50.769 -12.	912 59.453 -50.774 -12.910)
65.316 -49.370 -22.	759 65.320 -49.377 -22.757	7
64.538 -49.077 -24.	428 64.544 -49.080 -24.429)
102.096 -14.817 -18.	710 102.096 -14.821 -18.711	
88.655 0.088 -41.	505 88.659 0.087 -41.508	3
83.987 -12.140 -48.	194 83.990 -12.143 -48.197	7
72,723 -14,731 -59.	883 72.725 -14.733 -59.886	5
102.748 -2.368 -20.	105 102.749 -2.372 -20.105	5
95.207 18.810 -25.	065 95.206 18.810 -25.066	5
97.389 32.156 -0.	936 97.386 32.152 -0.932	2
88.249 36.073 -9.	196 88.250 36.073 -9.197	7
84.527 36.978 -16.	645 84.530 36.985 -16.648	3
83.912 34.527 -22.	612 83.913 34.525 -22.613	3
89.297 26.526 -33.	425 89.297 26.527 -33.428	3
88.247 29.432 -31.	096 88.248 29.431 -31.097	
80.567 38.301 -28.	303 80.565 38.297 -28.304	ŀ
79.693 38.134 -29.	935 /9.69/ 38.133 -29.936)
//.44/ 12./01 -48.	003 //.450 IZ./00 -48.064 222 47 100 22 071 EE 225	ŀ
62 555 29 466 46	233 07.100 22.971 -33.233)
66 161 33 780 -40	$186 \ 66 \ 161 \ 33 \ 778 \ -40. \ 411 \ 186$)
57 878 35 904 -47	<i>447</i> 57 877 35 901 -47 448	, }
59 745 40 234 -30	881 59 751 40 233 -30 878	, ,
56 435 50 719 -5	495 56 437 50 719 -5 499	ý
44,970 51,891 -0.	990 44.970 51.891 -0.994	L
57.382 51.358 -12.	046 57.383 51.360 -12.051	
56.732 52.829 -19.	634 56.732 52.824 -19.638	3
55.973 52.599 -21.	309 55.975 52.600 -21.313	3
42.735 47.706 -25.	736 42.735 47.708 -25.737	7
42.934 46.644 -34.	926 42.934 46.639 -34.926	5
57.383 51.359 -12.	045 57.383 51.360 -12.051	
42.735 47.707 -25.	736 42.735 47.708 -25.737	
42.934 46.645 -34.	925 42.934 46.639 -34.926)
24.458 44.355 -4.	497 24.461 44.357 -4.493	Ś
29.741 50.927 -0.	953 29.745 50.931 -0.945 097 27 044 E0 47E 11 001	/
27.843 50.074 -11.	087 27.844 30.873 -11.091 442 39 394 47 011 33 443)
20.202 47.010 -22.	043 20.204 47.011 -22.042	2
24.994 40.009 -0. 25 776 $1111 - 15$	560 25 778 11 112 -15 558	2
20 659 41 053 -0	960 20 667 41 053 -0 952	5
21, 482 45, 669 -8	777 21.484 45.670 -8 778	3
16. 172 34. 636 -12.	486 16.175 34.634 -12.480)
13.721 10.652 -8.	191 13.724 10.650 -8.180)
22.734 -9.453 -0.	956 22. 738 -9. 456 -0. 951	
15.381 -16.724 -11.	800 15.389 -16.728 -11.790)
18.749 -36.739 -0.	963 18. 751 - 36. 742 - 0. 954	ŀ
40.502 -43.366 -24.	811 40. 504 -43. 374 -24. 811	

45.810 -5 46.555 -5 44.969 -5 59.450 -5 54.757 -4 45 -217 -4	3. 428 - 17. 6 3. 754 - 15. 9 1. 880 - 0. 9 0. 770 - 12. 9 8. 907 - 16. 2 0. 271 - 22	H 07 45.812 34 46.555 43 44.970 11 59.453 56 54.759 58 45 220	P1_postfi -53.432 -53.762 -51.884 -50.774 -48.910	II_dxyza.txt -17.606 -15.933 -0.943 -12.910 -16.254 22.757	
03.317 - 4	9.3/1 - 22.7	38 03.320 37 (4 544	-49.377	-22.757	
64.539 - 4	9.0/8 -24.4.	27 04.544	-49.080	-24.429	
60.219 -4	1.800 -34.4	68 60.222	-41.870	-34.407	
50.978 -40	0.682 -36.1	10 50.982	-40.685	-36.109	
56.875 -40	0.275 -46.6	00 56.878	-40.278	-46.599	
83.109 -3	1.424 -31.0	72 83.114	-31.428	-31.072	
67.631 -2	7.411 -49.0	01 67.633	-27.413	-49.002	
97.242 -3	2.404 -0.9	37 97.247	-32.411	-0.937	
93.076 -2	7.628 - 32.8	48 93.078	-27.633	-32.848	
90.763 -29	9.660 -33.9	57 90.770	-29,663	-33, 958	
72 721 -14	4 731 -59 8	83 72 725	-14 733	-59 886	
83 986 -1	2 140 -48 1	95 83 990	-12 143	-48 197	
102 095 -1	4 817 -18 7	10 102 096	_14 821	-18 711	
102.070 = 1002.070 = 1000000000000000000000000000000000	2 260 20 10	05 102 070	2 272	20 105	
102.747 -	2.300 -20.1	05 102.749	-2.312	-20.100	

locatio	ns in coo	ordi nate	system r	normal to	o interfa	ce			
xnomb	ynomb	znomb	xmeasb	ymeasb	zmeasb	del x	del y	del z	del s
15.694	10.650	-2.993	15.696	10.652	-3.004	0.001	0.002	-0.011	0.012
21.692	-9.456	6.884	21.688	-9.454	6.8/8	-0.004	0.002	-0.005	0.007
18.493	-10.728		18.490	-10.724	-5.829	-0.004	0.004	-0.014	0.015
17.940	-30.742	0.01/ 0.201	17.940	-30.737	5.507 0.277	0.002	0.004	-0.010	
20.277	-30. 930	9.201 1 112	20.270	-30. 929	9.277	0.001	0.008	-0.004	0.009
30 250	-46 400	0 942	30 249	-46 393	0 941	-0.004	0.007	-0.002	0.010
27.738	-42, 521	-0.868	27.734	-42, 519	-0.873	-0.004	0.002	-0.005	0.007
49.071	-53.432	-0.875	49.069	-53. 428	-0.878	-0.002	0.004	-0.003	0.005
37.659	-35.418	-12.787	37.656	-35.416	-12.795	-0.003	0.002	-0.008	0.009
46. 547	-43.374	-9.461	46. 544	-43.366	-9.463	-0.003	0.009	-0.002	0.009
60. 257	-40.685	-16. 495	60. 255	-40.682	-16. 498	-0.002	0.003	-0.004	0.005
60.283	-50.774	8.203	60.280	-50.769	8.200	-0.003	0.006	-0.003	0.007
69.164	-49.377	0.957	69.161	-49.370	0.953	-0.003	0.007	-0.004	0.009
69.007	-49.080	-0.881	69.001	-49.077	-0.882	-0.006	0.003	-0.001	0.007
102.338	-14.821	17.337	102.338	-14.817	17.337	0.000	0.003	0.000	0.003
97.509	-12 143	-0.002	97.304	-12 140	-0.000	-0.003	0.001	0.002	0.000
88 821	-14 733	-31 401	88 819	-14 731	-31 399	-0.003	0.002	0.002	0 003
103.428	-2.372	16.250	103. 428	-2.368	16.249	0.000	0.003	0.000	0.003
98.038	18.810	9.008	98.037	18.810	9.010	0.000	0.001	0. 001	0.001
91.832	32. 152	32.432	91.836	32. 156	32.430	0.004	0.004	-0.002	0.006
86.073	36.073	21.541	86.072	36.073	21.542	-0.001	0.001	0.001	0.002
85.126	36.985	13.267	85.123	36.978	13.269	-0.003	-0.007	0.002	0.008
86.586	34.525	7.451	86.586	34.527	7.452	0.000	0.002	0.001	0.002
95.345	26.527	-0.8/0	95.343	26.526	-0.868	-0.002	0.000	0.002	0.003
95.001	29.431	0.901	93.000	29.432	0.901	-0.001	0.001	0.001	0.002
85 129	30.277	-0.873	85 126	38 134	-0.873	-0.001	0.004	0.002	0.003
89.218	12,700	-18, 676	89, 215	12,701	-18,676	-0.003	0.001	0.000	0.004
82.020	22.971	-28, 927	82.019	22.973	-28.925	-0.001	0.003	0.003	0.004
74.656	28.463	-22.217	74.656	28.466	-22.216	0.000	0.003	0.001	0.003
75.916	33. 778	-15.137	75. 916	33. 780	-15.134	-0.001	0.002	0.002	0.003
70.615	35.901	-24.791	70. 615	35.904	-24.790	0.000	0.003	0.001	0.003
66.708	40.233	-8.580	66.704	40.234	-8.585	-0.004	0.001	-0.005	0.006
54.914	50.719	14.135	54.911	50.719	14.139	-0.003	0.001	0.003	0.004
42.598	51.891	14.447	42.596	51.891	14.451	-0.002	0.001	0.004	0.004
58.044 60.027	51.300	0.302 0.050	58.042	51.308	0.300 0.052	-0.003	-0.002	0.004	
59 888	52.024	-0.883	59 885	52.029	-0.880	-0.002	-0.004	0.003	0.005
48.960	47.708	-9.568	48.959	47.706	-9.568	-0.001	-0.001	0.001	0.004

		HI	P1 postfi	II dxvza.	txt			
52.290 46. 58.044 51.	639 -18. 136 360 8. 302	52. 290 58. 042	46. 644 51. 359	-18. 135 8. 307	0.000	0. 005 -0. 001	0. 001 0. 006	0. 005 0. 006
48.960 47.	708 -9.568	48.960	47.707	-9.567	-0.001	0.000	0.001	0.001
24 522 40.0	357 4 144	24 521	40.043	4 140	-0.000	-0.008	-0.001	0.000
28.276 50.	931 9.282	28.273	50. 927	9.277	-0.003	-0.004	-0.005	0.007
29.958 50.	675 -0.899	29.956	50.674	-0.896	-0.002	0.000	0.003	0.004
34.322 47.0	011 -11.603	34.321	47.016	-11.604	-0.001	0.005	-0.001	0.005
20.238 48.0	008 U. 939 142 -5 803	20.200	48.009 11 11	-5 806	-0.002	0.001	-0.002	0.003
19.746 41.0	053 6.174	19.742	41.053	6. 163	-0.004	0.002	-0.011	0.003
23.190 45.	670 -0.901	23. 188	45.669	-0.900	-0.002	-0.001	0.001	0.003
19.468 34.	634 -6.195	19.467	34.636	-6.202	0.000	0.002	-0.007	0.007
15.694 10.	650 -2.993 456 6.884	15.695	10.652	-3.004	-0.001	0.003	-0.011	
18.493 -16.	728 -5.815	18.490	-16, 724	-5.828	-0.003	0.003	-0.013	0.014
17.946 -36.	742 5.517	17.948	-36.739	5.507	0.002	0.003	-0.009	0.010
46.547 -43.	374 -9.461	46.545	-43.366	-9.462	-0.002	0.008	-0.001	0.009
49.0/1 -53.4	432 -0.875	49.069	-53.428	-0.8//	-0.002	0.004	-0.002	0.004
42.581 -51.5	884 14,494	42.579	-51,880	14, 494	-0.001	0.007	0.000	0.005
60. 283 -50.	774 8.203	60.280	-50.770	8.201	-0.003	0.005	-0.002	0.006
57.016 -48.	910 3.455	57.014	-48.907	3.452	-0.001	0.003	-0.003	0.004
69.164 -49.	3/7 0.957	69.161	-49.371	0.955	-0.003	0.006	-0.002	0.007
68 379 -41	870 -11 792	68 376	-49.078	-0.000	-0.008	0.002	-0.001	0.000
60.257 -40.	685 -16.495	60.254	-40.682	-16.497	-0.003	0.003	-0.003	0.005
69.386 -40.1	278 - 24. 335	69.383	-40.275	-24.337	-0.003	0.003	-0.002	0.004
88.729 -31.4	428 -0.772	88.724	-31.424	-0.773	-0.005	0.004	-0.001	0.006
91 703 -32	413 - 22.915	91 698	-27.411	-22.915	-0.003	0.002	-0.002	0.004
98.700 -27.	633 0.967	98.698	-27.628	0.967	-0.002	0.005	0.000	0.006
96.910 -29.	663 -0.865	96.903	-29.660	-0.866	-0.007	0.003	-0.001	0.008
88.821 -14.	/33 -31.401	88.816	-14. /31	-31.400	-0.005	0.002	0.001	0.005
102 338 -14	821 17 337	102 337	-12.140	17 337	-0.004	0.002	0.000	0.005
103.428 -2.	372 16.250	103. 427	-2.368	16.249	-0.001	0.004	-0.001	0.004
xavg = -0.0	019 yavg	= 0.00	028 za	avg = -0.	0016	savg =	0.0058	
xstd = 0.0	020 ystd	= 0.00	028 ZS	std = 0.	0040	sstd =	0.0028	

Finally, the "C" coil is added [in process]



- The same general steps as the A-B assembly are followed.
- Intermediate measurements to date are encouraging.
- Accuracy goal is .020" maximum deviation of monuments from theoretical positions.

Coil Distortion and Measurement Uncertainty is Introduced Throughout the Process



- Our assembly process and dimensional control plan attempt to minimize both.
- Different measurement techniques have different levels of uncertainty, and different degrees of applicability to specific tasks.

Blunders, Systemic Errors and Random Errors are the Sources of Measurement Error



- "Blunders" are mistakes in either making, or recording, measurements, and are usually obvious.
 - Correct blunders, where possible, before processing data.
- Systemic errors are errors inherent to equipment, and can in theory be compensated for during data analysis.
 - Examples thermal expansion of a scale bar, thermal expansion of components to be measured.
 - In our case, these are smaller than our random errors.
- Random errors result from random variations in a process or measurement technique.
 - Define confidence intervals on measurements that are subject to random variation.

Laser Measuring Tools



- Corner cube
 - 1.5" or .5" diameter.
 - Sits in magnetic nest.
 - .5" diameter, with special nest, mimics short shank tooling ball.
 - Negligible positioning accuracy relative to nest.
 - Global monuments are 1.5"dia corner cube, in nest that is secured to building or HPA fixture.
 - When nest is placed in tooling ball hole, the accuracy issues are the same as for a tooling ball – tightness of the hole.
 - Possible blunders using the .5"diameter corner cube and special nest does it remain seated in hole after grip is released? [air pressure in hole may act as spring] ~.001" - .002" effect; difficult to recognize
 - Limited viewing angles

Laser Measuring Tools



- Leica Surface Reflector
 - Allows the laser to measure to the center of a tooling ball by creating a virtual center.
 - Avoids the problem of a tooling ball or nest "releasing" during measurement.
 - Limited view angles.
 - Highly accurate.



- Measure a sphere around a tooling ball (or 15mm ball bearing in a conical seat) using a corner cube, in a nest, on a wand.
- Best view, least accurate.
- Was necessary for measuring conical seats.
- Qualification tests performed to assess accuracy of this technique.
- In-field checking of sphericity of measurement helps to eliminate blunders.

Some Thoughts on Confidence Intervals



- For a process with a normal distribution, we can define confidence intervals as ratios of the standard deviation
 - Some [two-sided] ratios:
 - 50% -> .67; 75% -> 1.15; 90% -> 1.65; 95% -> 1.96; 99% -> 2.58
 - For a standard deviation of .0006in for any component of a measurement, the confidence intervals become:
 - 50% -> .0004"; 75% -> .0007"; 90% -> .001"; 95% -> .0012"; 99% -> .0015"
- If we have a normally distributed population N(μ,σ) of measurements , and we take samples of n measurements, then the means of the samples will also be normally distributed.

$$\overline{x} = N\left(\mu, \sigma / \sqrt{n}\right)$$

 The effective standard deviation is reduced. For our superpoints(n=100), by one order of magnitude. For "Dan-O" points (n=50) by ~7. Some Thoughts on Confidence Intervals



- How do the confidence intervals on the components affect the 3-d deviation?
- Let α , β , γ represent the magnitude of expected error, or half the confidence interval, in the x, y, and z measurements respectively.
- The radius of the "error sphere" representing the 3-d deviation is then $\varepsilon = \sqrt{3}\sigma$
- For a 99% confidence interval and σ =.0006in, we have
 - Single point -> .0013"
 - "Dan-O" point -> .00019
 - Super point ->.00013
 - Scepter Sphere -> .0044

Standard Deviation of Measurements is Obtained from Qualification Tests



- Use the square root of variance as an unbiased estimator for the standard deviation.
- Place a confidence interval on the estimate of the variance, then use the upper end of that interval.

$$\chi_{.005}^{2} \le \frac{(n-1)s^{2}}{\sigma^{2}} \le \chi_{.995}^{2}$$



Where are we now, assuming 99% confidence intervals?



- Alignment to a modular coil same as RMS deviation
 - .005" when we achieve our goal.
- Pre-measurement uncertainty .0059"
 - .0044 measurement uncertainty from sphere + .0015 for global alignment.
- Our measurement uncertainty after A1B1 .0034"
 - .0015 for global alignment + .0019" "Dan-O" uncertainty.
- .0143" total.
- This is not expected to change after C1 is added to A1B1, because the uncertainties are not directly additive.

Is our performance really at the "top of error bar" level?



- Convergence of racking process indicates that measurements with scepter are better than the extreme end of error bar.
- The use of pre-calculated shims, and adjustment of shims based on laser measurements, has worked to a greater accuracy than that indicated by the extremes of a 99% confidence interval.
- Horizontal position adjustments using the alignment calculator perform better than what we would obtain if our measurements were at the extremes of a 99% confidence interval.

Some caveats and thoughts for future discussion...



- On the early modular coils (the ones we are presently assembling) we did not preserve the conical seats prior to pre-measurement. We therefore had to rack, and align, to measurements of the tooling balls taken during initial conical seat installation, when the deformed shape of the coil was not precisely defined. The racking and alignments to these monuments did not meet our .005" criterion, and we may well have lost ~.020" of accuracy here.
- Can we make use of our large number of monuments to draw some statistical inferences, with higher accuracy/confidence, than we have now?