

# Physics Issues of Compact Drift-Optimized Stellarators

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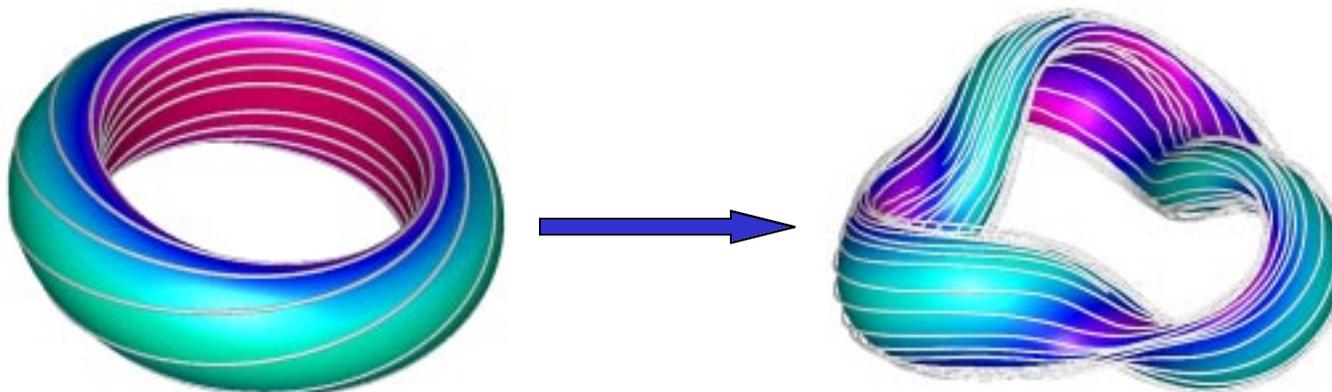
- Introduction/Motivation
- Optimization Method and Physics Analysis Tools
- Physics evaluations for recent configurations
  - Electron and ion neoclassical losses
  - Energetic orbit losses
  - Ballooning/kink/vertical stability
  - Bootstrap current
- Conclusions

# Introduction

# Compact stellarators (low $A = R/\langle a \rangle$ ) offer:

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- Combination of the desirable features of TOKAMAKS (low  $A$ , high  $\beta$ , good confinement)
- with those of the STELLARATOR (low recirculating power, disruption avoidance)
- Focus is on COMPACTNESS (while preserving confinement/stability)



# Features of low $A = R/\langle a \rangle$ stellarators

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- Lower cost near-term experiments while maintaining a similar plasma radius as large aspect ratio devices
- Longer term potential of a more economically-sized, higher-power-density reactor
- Opens up a new regime of stellarator parameter space with new physics expected in:
  - transport
  - equilibrium fragility
  - plasma flow dynamics
  - enhanced confinement regimes
  - RF heating strategies
  - microturbulence

# Strategies for QOS Optimization

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- Optimize an ultra low aspect ratio ( $A = 2.5 - 3$ ), low  $\beta$  configuration for a Concept Exploration experiment
  - most of the rotational transform supplied externally
- Optimize compact ( $A = 3 - 3.5$ ), high  $\beta$  configurations as part of the longer-term QOS program
  - a larger fraction of the transform provided by plasma currents

# Methods

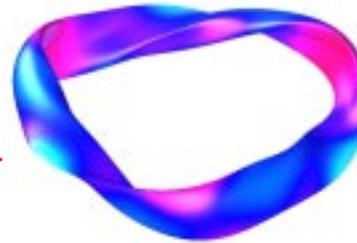
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- Stellarator optimization
- Transport evaluation
- Ballooning
- Bootstrap Currents

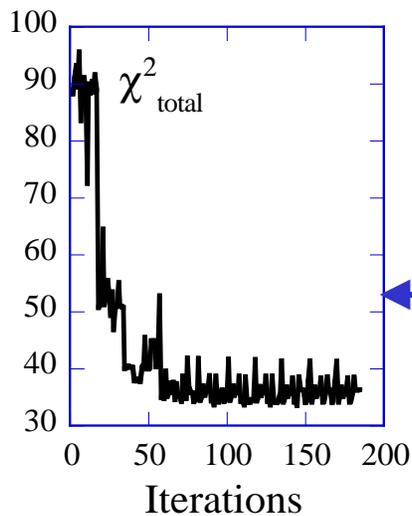
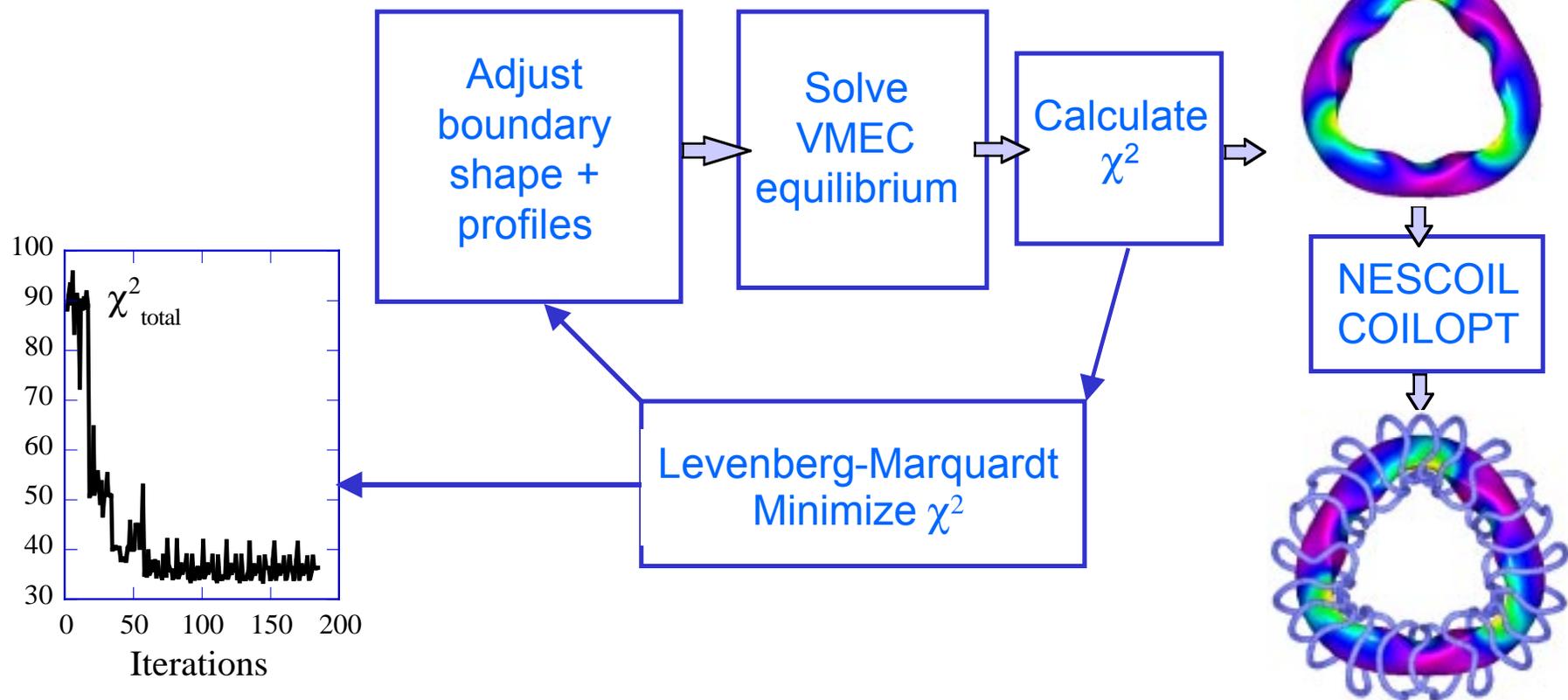
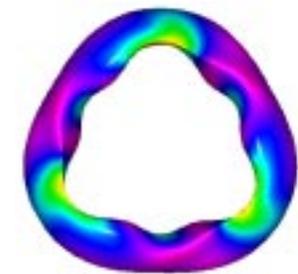
# Stellarator optimization loop determines outer flux surface shape. Coils to produce this shape are then “reverse-engineered”:

Stellarator optimization

Initial configuration



Final optimized configuration



# Optimization Process Successfully Integrates a complex, interacting set of Physics Criteria:

Stellarator optimization

<u>Targets</u> (Physics/Engineering)	<u>Example</u>
Bounce-average omnigenicity (drift surfaces and flux surfaces aligned)	$B_{\min} = B_{\min}(\psi)$ $B_{\max} = B_{\max}(\psi)$ $J = J(\psi)$
Target nearby quasi-symmetries	Minimize $B_{mn}$ if $m \neq 0$ (QP), or if $m/n \neq 1$ (QH)
Local diffusive transport	$D, \chi$ from DKES
Current profile	self-consistent $I_{BS}$ , $I(\psi)$ goes to 0 at edge
Limit maximum plasma current	e.g., $I_{\max} < 40$ kAmps
Iota profile	$i(\psi) = 0.5$ ( $\rho = 0$ ) to $0.8$ ( $\rho = a$ )
Magnetic Well, Mercier	$V'' < 0, D_M > 0$ over cross section
Ballooning stability	$\langle \beta \rangle \sim 2-4\%$
Aspect ratio	$R_o/a \approx 2.5$ to $3.5$
Limit outer surface curvature	avoid strong elongation/cusps

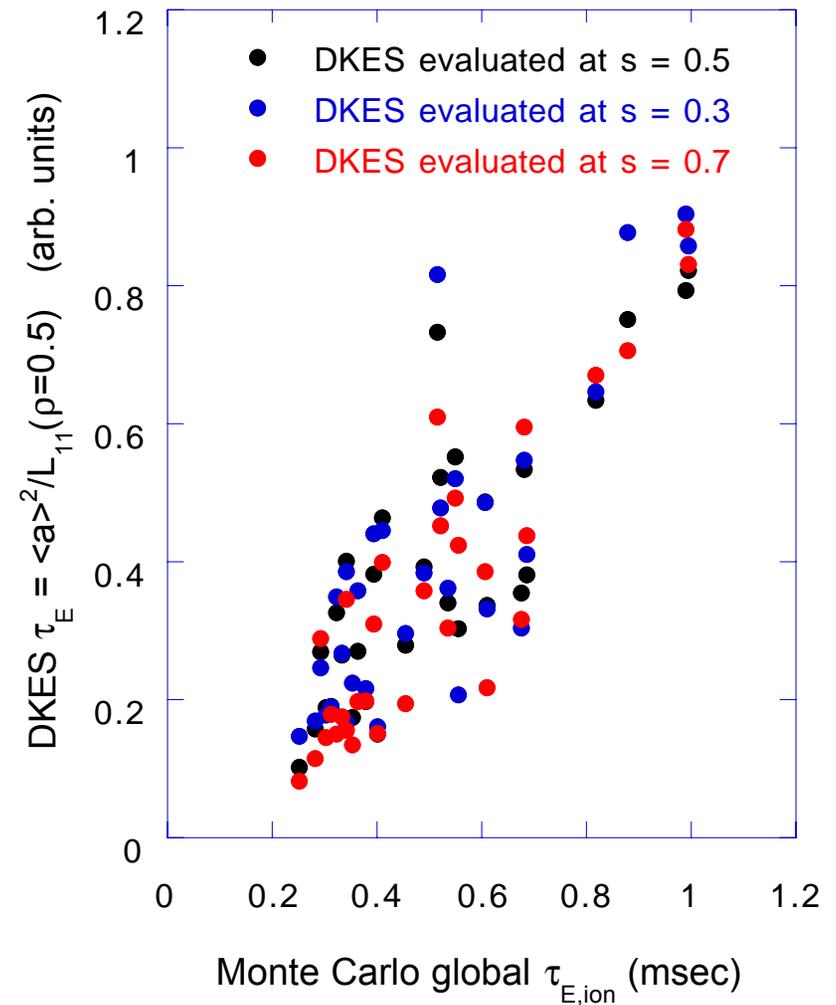
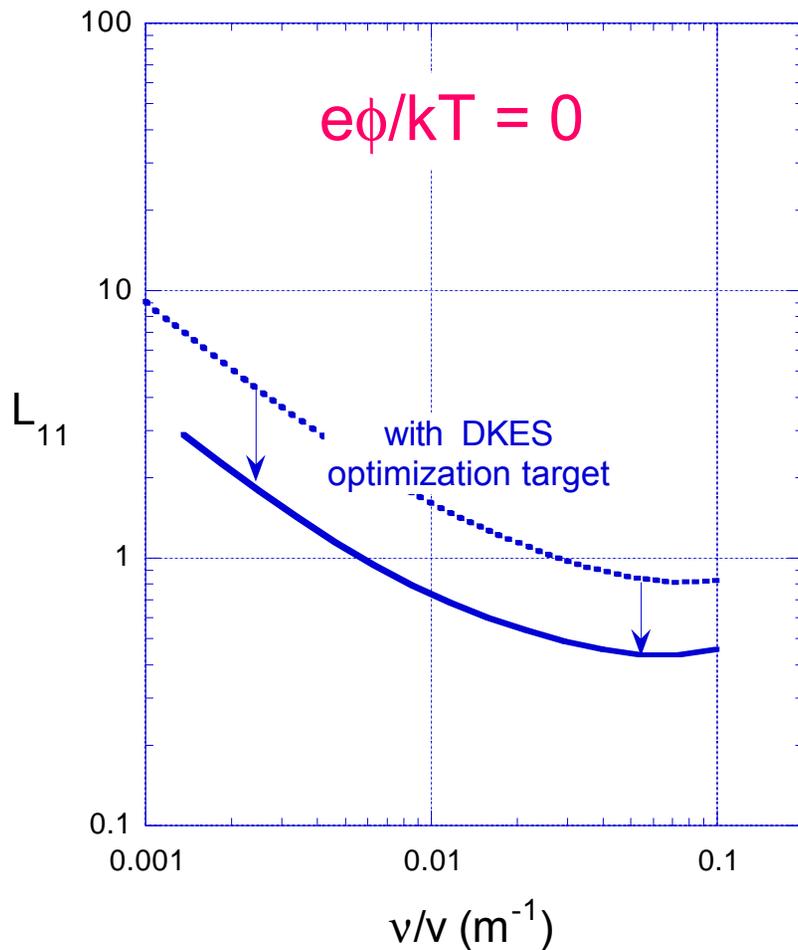
## Control variables:

shape (30-40 Fourier harmonics  $R_{mn}, Z_{mn}$ )  
for LCFS + profile parameters

# Transport optimizations using the DKES transport target have resulted in confinement improvement.

Stellarator optimization

3 field periods ( $A = 3.4$ )



# Bootstrap and Ballooning Analysis

Stellarator optimization

- The **COBRA** code used for rapid ballooning optimization and configuration evaluation
  - Initially estimates growth rate with finite difference solution, then refines with variational principle and Richardson extrapolation
  - R. Sanchez, S.P. Hirshman, et al., Journal of Computational Physics **161**(2000) 576.
- Optimization targets **collisionless bootstrap current** for bootstrap consistency
  - K.C. Shaing, E.C. Crume, Jr., J.S. Tolliver, S.P. Hirshman, W.I. van Rij "Bootstrap current and parallel viscosity in the low collisionality regime in toroidal plasmas", Phys. Fluids B1, 148 (1989).
  - K.C. Shaing, S.P. Hirshman, J.S. Tolliver "Parallel viscosity-driven neoclassical fluxes in the banana regime in nonsymmetric toroidal plasmas", Phys. Fluids 29, 2548 (1986)

# Transport tools

- General purpose stellarator particle simulation code (DELTA5D)
  - thermal electron/ion transport, bootstrap current
  - alpha particles
  - neutral beams, ICRH tails
  - uses MPI to achieve near linear speedup with number of processors
- Drift Kinetic Equation Solver (DKES)
  - variation of bootstrap current with collisionality and electric field
  - local diffusion coefficients  ambipolarity condition
  - integrate over profiles to obtain global lifetimes
  - uses shared memory OpenMP parallelism to achieve ~ x 3 speedup (with Ed D'Azevedo, ORNL CCS Division)
- Other qualitative measures:  $J$ ,  $B_{\min}$ ,  $B_{\max}$ ,  $|B|$  contours

# Applications of DKES to QO transport:

Stellarator optimization

- Used in the optimizer
- Collisional bootstrap current
- Ambipolarity studies
  - Initially, use DKES for both electron and ion fluxes
  - Then hybrid model: DKES electron flux with ion particle flux from particle-based calculation

# The DKES (Drift Kinetic Equation Solver) provides the full neoclassical transport coefficient matrix (multi-helicity)

Transport analysis

$$I_i = \begin{bmatrix} \bar{\Gamma} \cdot \bar{\nabla}_s \\ \frac{1}{T} \bar{Q} \cdot \bar{\nabla}_s \\ n \langle (\bar{u} - \bar{u}_s) \cdot \bar{B} \rangle \end{bmatrix} = -\sum_{j=1}^3 L_{ij} A_j \quad A_j = \begin{bmatrix} \frac{n'}{n} - \frac{3 T'}{2 T} - \frac{e E_r}{T} \\ \frac{T'}{T} \\ -\left(\frac{e}{T}\right) \left( \frac{\langle \bar{E} \cdot \bar{B} \rangle}{\langle B^2 \rangle} \right) \end{bmatrix}$$

$$L_{ij} = n \frac{2}{\sqrt{\pi}} \int_0^\infty dK \sqrt{K} e^{-K} g_i g_j D_{ij}$$

$$\text{where } g_1 = g_3 = 1, g_2 = K, K = \left( \frac{v}{v_{th}} \right)^2$$

$$D_{11} = D_{12} = D_{21} = D_{22} = -\frac{v_{th}}{2} \left[ \frac{B v_{th}}{\Omega} \left( \frac{d\rho}{dr} \right)^{-1} \right]^2 K \sqrt{K} \Gamma_{11}$$

$$D_{31} = D_{32} = -D_{13} = -D_{23} = -\frac{v_{th}}{2} \left[ \frac{B v_{th}}{\Omega} \left( \frac{d\rho}{dr} \right)^{-1} \right] K \Gamma_{31}$$

$$D_{33} = -\frac{v_{th}}{2} \sqrt{K} \Gamma_{33}$$

$$\Gamma_{ij} = \Gamma_{ij} \left( \frac{v}{v}, \frac{E_r}{v} \right)$$

- W. I. Van Rij, S. P. Hirshman, Phys. Fluids **B 1**, 563 (1989)

- Variational: provides upper and lower bounds on dS/dt

- Expands f in Fourier-Legendre series

(i.e., to carry out the above integrals, one will need to generate a 2-D matrix of  $\Gamma$ 's vs. these parameters for each flux surface)

# DELTA5D Monte Carlo code is used for both thermal plasma and fast ion confinement studies

Transport analysis

- Thermal plasma
  - Global and local diffusive limits
- Various fast ion populations
  - ICRF tails (quasilinear diffusion operator)
  - Neutral beam ions (pencil beam approximation)
  - Alphas
  - Alfvén turbulence (to be added)
- Options for  $f$  and  $\delta f$  particle weightings
- Diagnostics: particle and energy losses, loss patterns, energy slowing down, escaping pitch angle/energy/lifetime distributions
- Longer term goal: Multi-species (thermal, fast ion, impurity), coupled transport and electric field evolution model
- Computational characteristics
  - parallelization over particles rather than domains
  - uses collective MPI communications, runs on T3E and IBM-SP

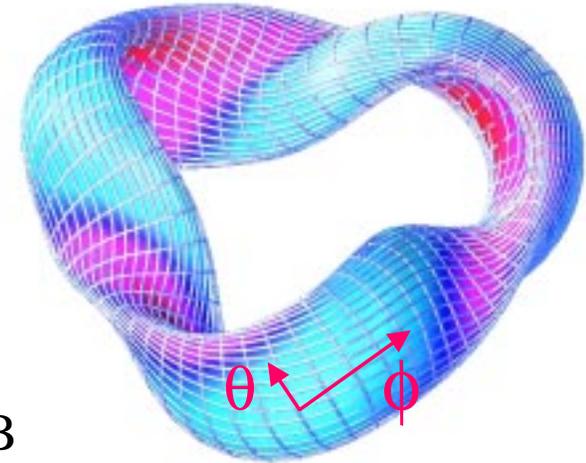
# Hamiltonian Guiding Center Orbit Equations:

Transport analysis

$$\dot{\psi} = (g\dot{P}_\theta - I\dot{P}_\phi) / D, \quad \dot{\rho}_\parallel = \frac{1}{D} [-(\rho_\parallel g' - \iota)\dot{P}_\theta + (1 + \rho_\parallel I')\dot{P}_\phi]$$

$$\dot{\theta} = \left\{ \left[ \frac{e^2 \rho_\parallel^2 B}{m} + \mu \right] \frac{\partial B}{\partial \psi} + e \frac{\partial \Phi}{\partial \psi} \right\} \frac{\partial \psi}{\partial P_\theta} + \frac{e^2 B^2}{m} \rho_\parallel \frac{\partial \rho_\parallel}{\partial P_\theta}$$

$$\dot{\phi} = \left\{ \left[ \frac{e^2 \rho_\parallel^2 B}{m} + \mu \right] \frac{\partial B}{\partial \psi} + e \frac{\partial \Phi}{\partial \psi} \right\} \frac{\partial \psi}{\partial P_\phi} + \frac{e^2 B^2}{m} \rho_\parallel \frac{\partial \rho_\parallel}{\partial P_\phi}$$



where  $D = e[g + \iota + \rho_\parallel(gI' - Ig')]$ ,  $\rho_\parallel = mv_\parallel / eB$

$$\dot{P}_\theta = -\frac{\partial B}{\partial \theta} \left[ \frac{e^2 \rho_\parallel^2 B}{m} + \mu \right], \quad \frac{\partial \rho_\parallel}{\partial P_\theta} = -(\rho_\parallel g' - \iota) / D$$

$$\dot{P}_\phi = -\frac{\partial B}{\partial \phi} \left[ \frac{e^2 \rho_\parallel^2 B}{m} + \mu \right], \quad \frac{\partial \rho_\parallel}{\partial P_\phi} = (I' \rho_\parallel + 1) / D$$

$\Phi$  = electrostatic potential

$g$  = net poloidal current outside a flux surface

$I$  = net toroidal current inside a flux surface

$\iota$  = rotational transform

# Coulomb collision operator for collisions of test particles (a) with a background plasma (b):

Transport analysis

$$C_{ab} f_a = \frac{v_D^{ab}}{2} \frac{\partial}{\partial \lambda} (1 - \lambda^2) \frac{\partial f_a}{\partial \lambda} + \frac{1}{v^2} \frac{\partial}{\partial v} \left\{ v^2 \left[ 2v_\varepsilon \alpha_{ab} f_a + \frac{v_\varepsilon}{v} \alpha_{ab}^3 \frac{\partial f_a}{\partial v} \right] \right\}$$

where

$$v_D^{ab} = \frac{v_0^{ab}}{(v / \alpha_{ab})^3} \left[ \phi \left( \frac{v}{\alpha_b} \right) - G \left( \frac{v}{\alpha_b} \right) \right] \quad v_\varepsilon = v_0^{ab} G \left( \frac{v}{\alpha_b} \right)$$

$$\phi(x) = \frac{2}{\sqrt{\pi}} \int_0^x dt t^{1/2} e^{-t} \quad G(x) = \frac{1}{2x^2} [\phi(x) - x\phi'(x)]$$

$$\alpha_{ab} = \sqrt{\frac{2T_{b0}}{m_a}} \quad \alpha_b = \sqrt{\frac{2T_{b0}}{m_b}} \quad v_0^{ab} = \frac{4\pi n_b \ln \Lambda_{ab} (e_a e_b)^2}{(2T_b)^{3/2} m_a^{1/2}}$$

# Monte Carlo Equivalent of the Fokker-Planck Operator

[A. Boozer, G. Kuo-Petravic, Phys. Fl. **24** (1981)]

Transport analysis

$$\lambda_n = \lambda_{n-1}(1 - \nu_d \Delta t) \pm [(1 - \lambda_{n-1}^2) \nu_d \Delta t]^{1/2}$$

$$E_n = E_{n-1} - (2\nu_\varepsilon \Delta t) \left[ E_{n-1} - \left( \frac{3}{2} + \frac{E_{n-1}}{\nu_\varepsilon} \frac{d\nu_\varepsilon}{dE} \right) T_b \right] \pm 2[T_b E_{n-1} \nu_\varepsilon \Delta t]^{1/2}$$

# Local Monte-Carlo equivalent quasilinear ICRF operator (developed by J. Carlsson)

$$E^+ = E^- + \mu^E + \zeta \sqrt{\sigma^{EE}}$$

$$\lambda^+ = \lambda^- + \mu^\lambda + \zeta \sqrt{\sigma^{\lambda\lambda}}$$

Transport analysis

$\zeta$  = a zero-mean, unit-variance random number (i.e.,  $\mu^\zeta = 0$  and  $\sigma^\zeta = 1$ )

$$\sigma^{EE} = 2 m^2 v_\perp^2 \Delta v_0 \quad \sigma^{\lambda\lambda} = 2 \left( \frac{k_\parallel - \frac{v_\parallel}{v^2}}{\omega} \right)^2 \frac{v_\perp^3 \Delta v_0}{v^2}$$

$$\mu^E = 2 \left( 1 - \frac{k_\parallel v_\parallel}{\omega} \right) m v_\perp \Delta v_0 \quad \mu^\lambda = \left\{ 2 \left[ \left( 1 - \frac{k_\parallel v_\parallel}{\omega} \right) - \frac{v_\perp^2}{v^2} \right] \left( \frac{k_\parallel - \frac{v_\parallel}{v^2}}{\omega} \right) + \frac{v_\parallel}{v^2} \frac{v_\perp^2}{v^2} \right\} \frac{v_\perp \Delta v_0}{v}$$

where

$$\Delta v_0 = \frac{1}{v_\perp} \left( \frac{eZ}{2m} |E_+ J_{n-1}(k_\perp \rho) + E_- J_{n+1}(k_\perp \rho)| \right)^2 \frac{2\pi}{n |\dot{\Omega}|}$$

as  $\dot{\Omega} \rightarrow 0$

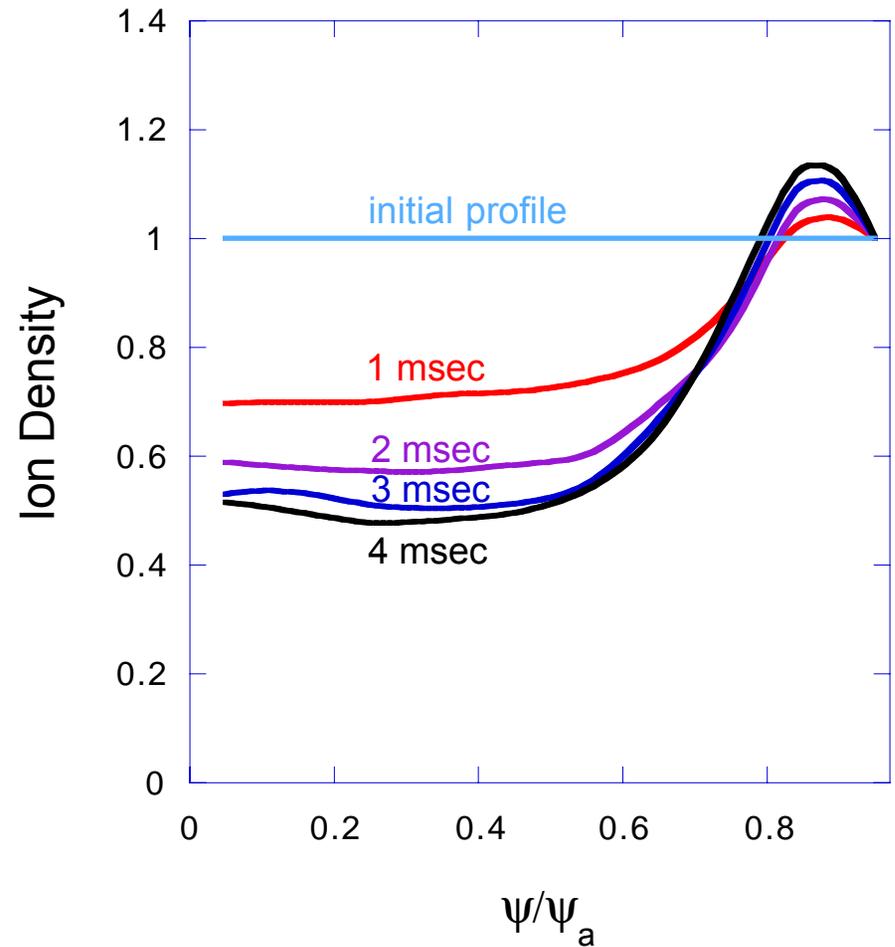
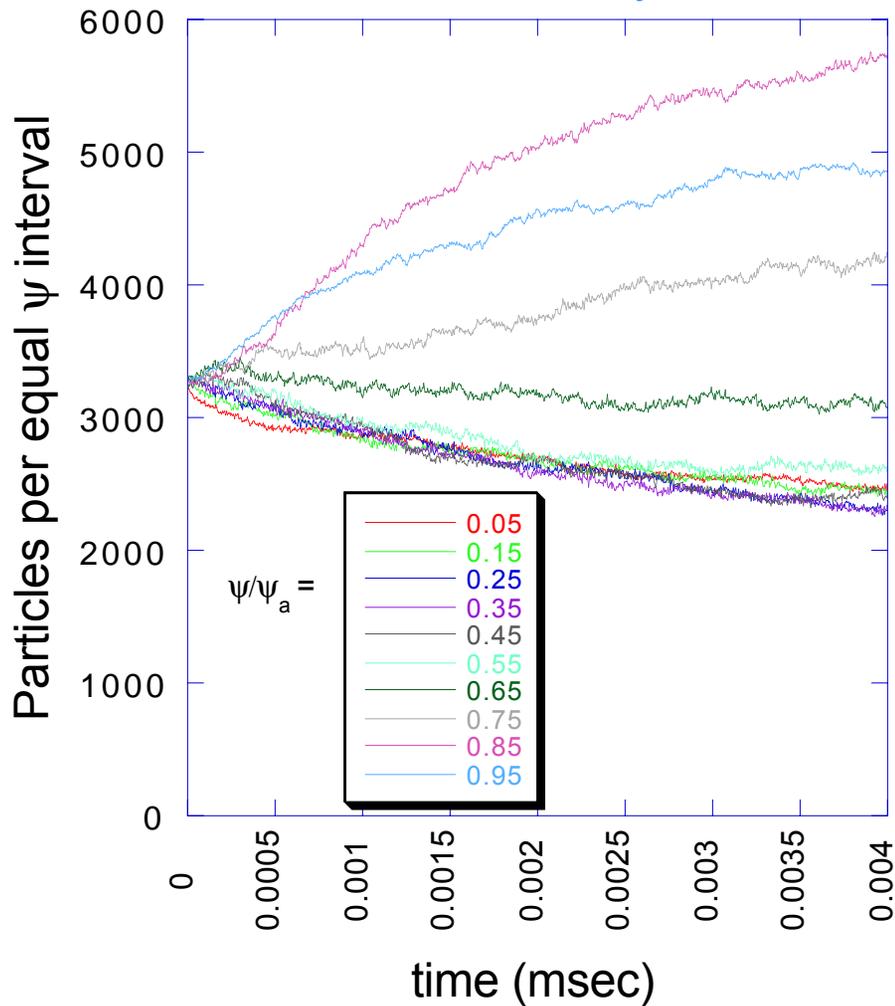
$$\frac{2\pi}{n |\dot{\Omega}|} \rightarrow 2\pi^2 \left| \frac{2}{n \ddot{\Omega}} \right|^{2/3} \times \text{Ai}^2 \left( -\frac{n^2 \dot{\Omega}^2}{4} \left| \frac{2}{n \ddot{\Omega}} \right|^{4/3} \right)$$

# For the low density, higher temperature case, the ion particle density evolves to a hollow profile shape.

Transport analysis

In future work will explore dependence on:

- Particle refueling and energy input model
- Self-consistency between collision operator and particle profiles

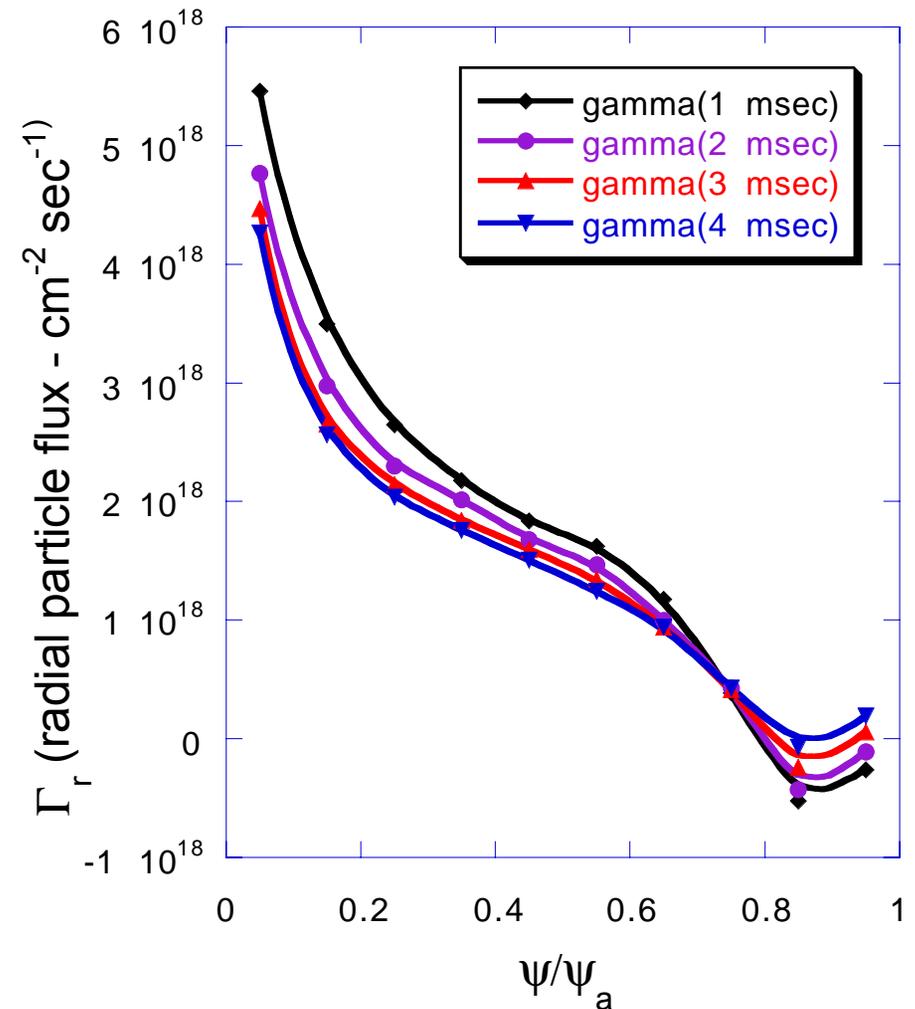
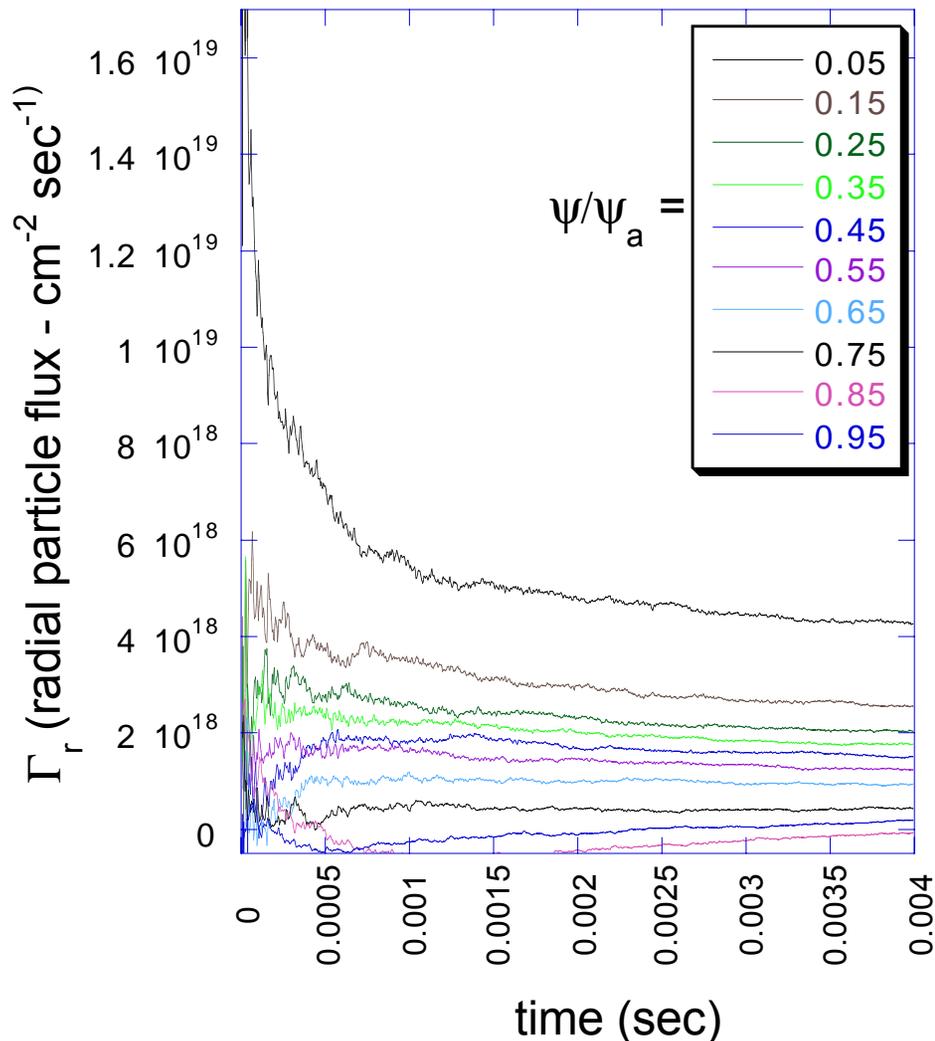


Particle fluxes are peaked near the center  
where the ion temperature is highest

$$n(0) = 3 \times 10^{13} \text{ cm}^{-3}, T(0) = 1.8 \text{ keV}$$

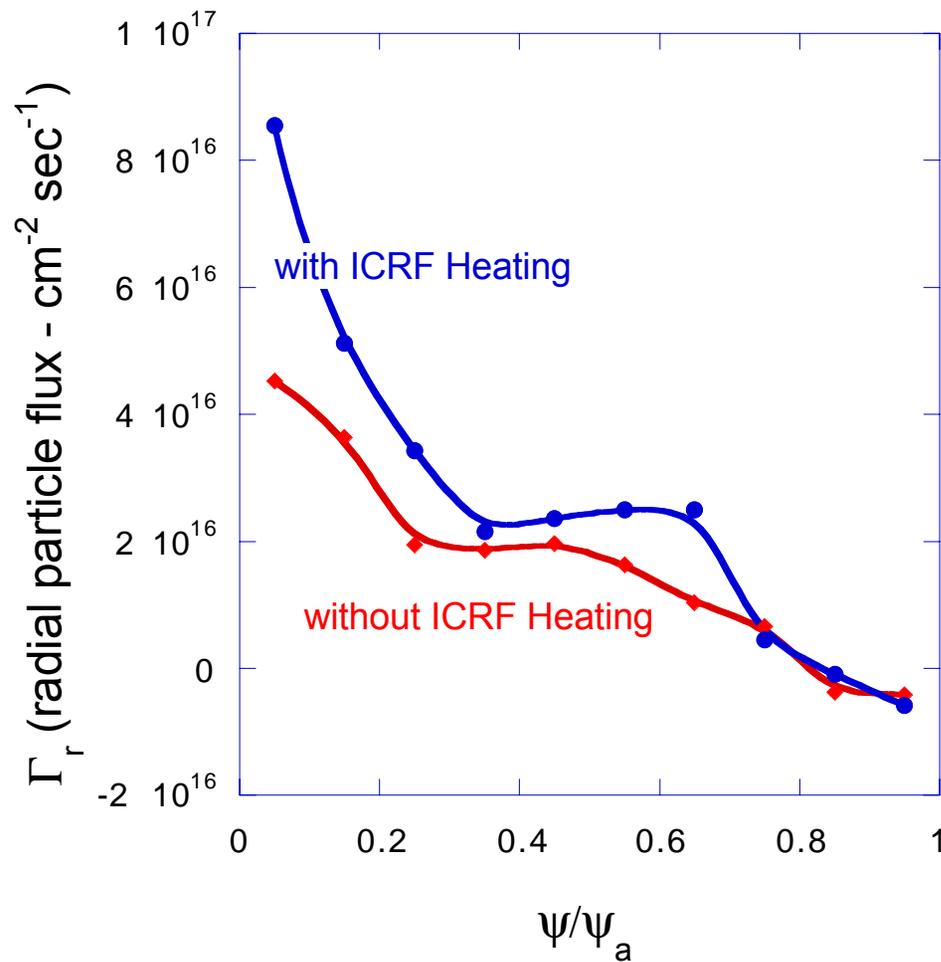
Transport analysis

time-averaged ion particle fluxes



Since ICRF heating does not preserve  $\mu$  or  $J$ , it can enhance radial particle fluxes. This can be an important issue and control knob for the generation of the ambipolar electric field

Transport analysis



# Configuration Development

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- Ultra low  $A$  (2.5 - 3), near-term devices
  - most of the transform supplied externally
  - quasi-poloidal symmetry built-in
- Compact ( $A = 3 - 3.5$ ) high  $\beta$  devices
  - large fraction of transform comes from current
  - quasi-poloidal symmetry enhanced by high  $\beta$

# Selection Criteria for Configurations

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- Guidelines for the selection of a configuration for a CE:
  - Compact:  $A < 3$ 
    - This ultra low aspect ratio range is lower than existing stellarators (1/2 to 2/3 that of NCSX)
  - Good confinement:  $\tau_{\text{neo}} > 2 * \tau_{\text{ISS95}}$ 
    - Drift-optimized so that neoclassical transport is not the dominant loss mechanism
    - Cases normalized to:  $R \cdot \langle a \rangle = 0.278$  and  $\langle |B| \rangle = 1.0$

# Selection Criteria for Configurations (cont.)

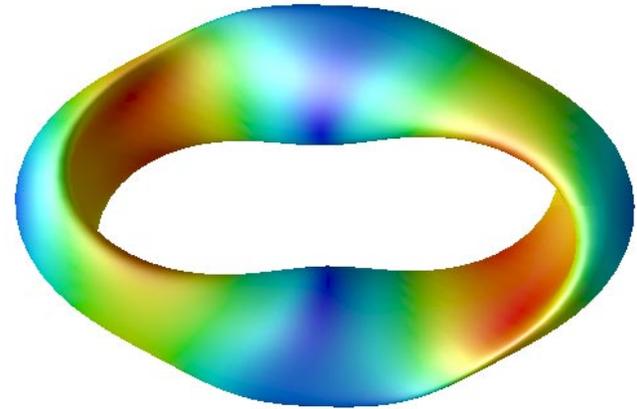
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- Stability: MHD stable at  $\beta \sim 2\%$ 
  - Ballooning and Mercier analysis included in optimization to ensure stability at  $\beta$  levels relevant to a CE
- Accessibility: not an issue for low  $I_{BS}$  QOS
- Flexibility: ability to vary the bootstrap current through the  $|B|$ -spectrum

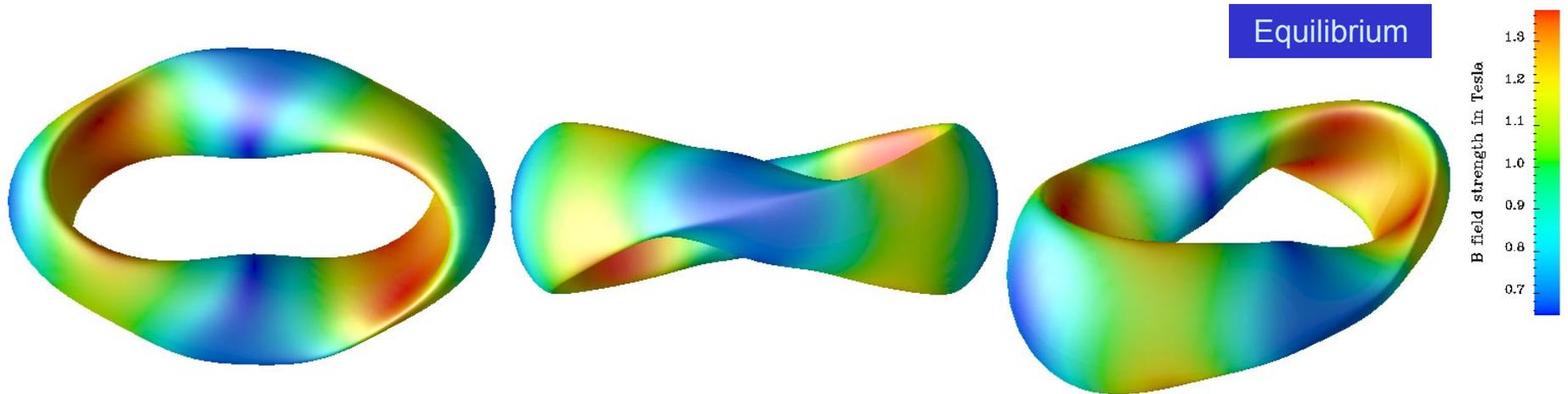
# Quasi-Poloidally Symmetric Cases

Equilibrium

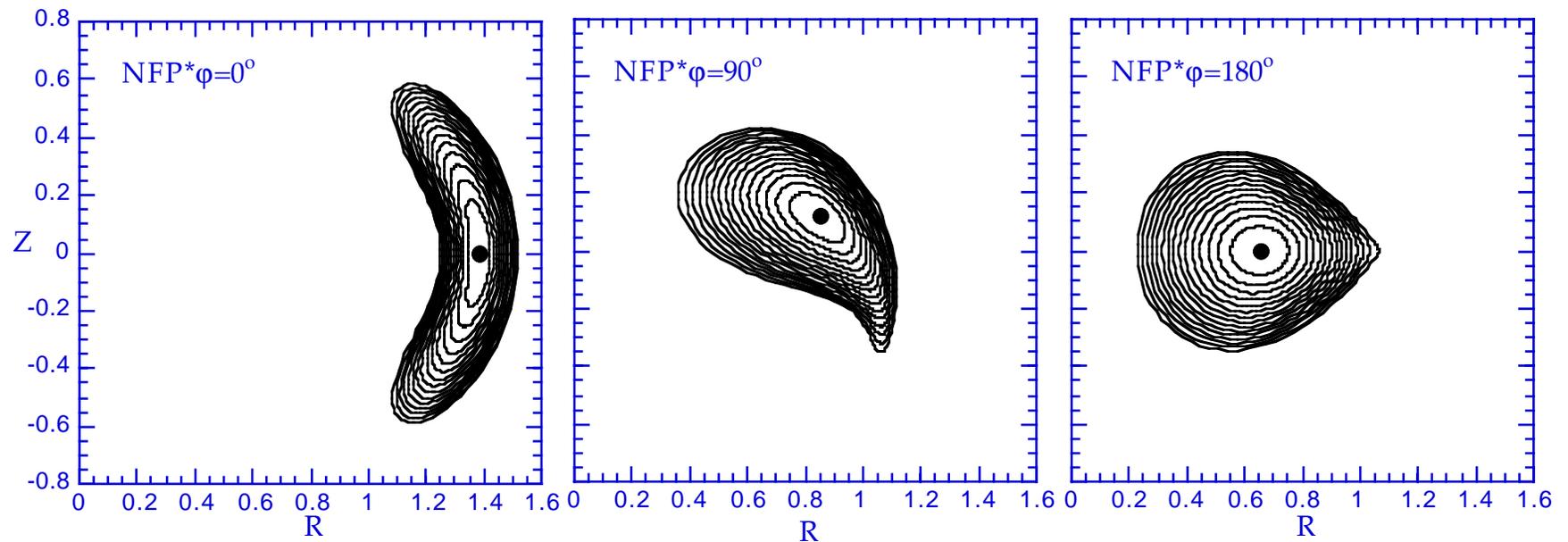
- Base case: A2.5\_M2\_B1.3
  - Max.Tor.Cur. = 25.7 kA
- Low aspect ratio:  $A < 2.5$ 
  - Have obtained configurations with aspect ratios in the range:  $A=2.1$  to  $A=3.0$
- Rotational transform below 0.5:  $\iota \sim 0.3 - 0.4$ 
  - Majority of the transform is from the coils, bootstrap current causes iota to increase
  - Stable to neoclassical tearing modes



# Outer Surface Views for A2.5\_M2\_B1.3



## Cross Sections for A2.5\_M2\_B1.3

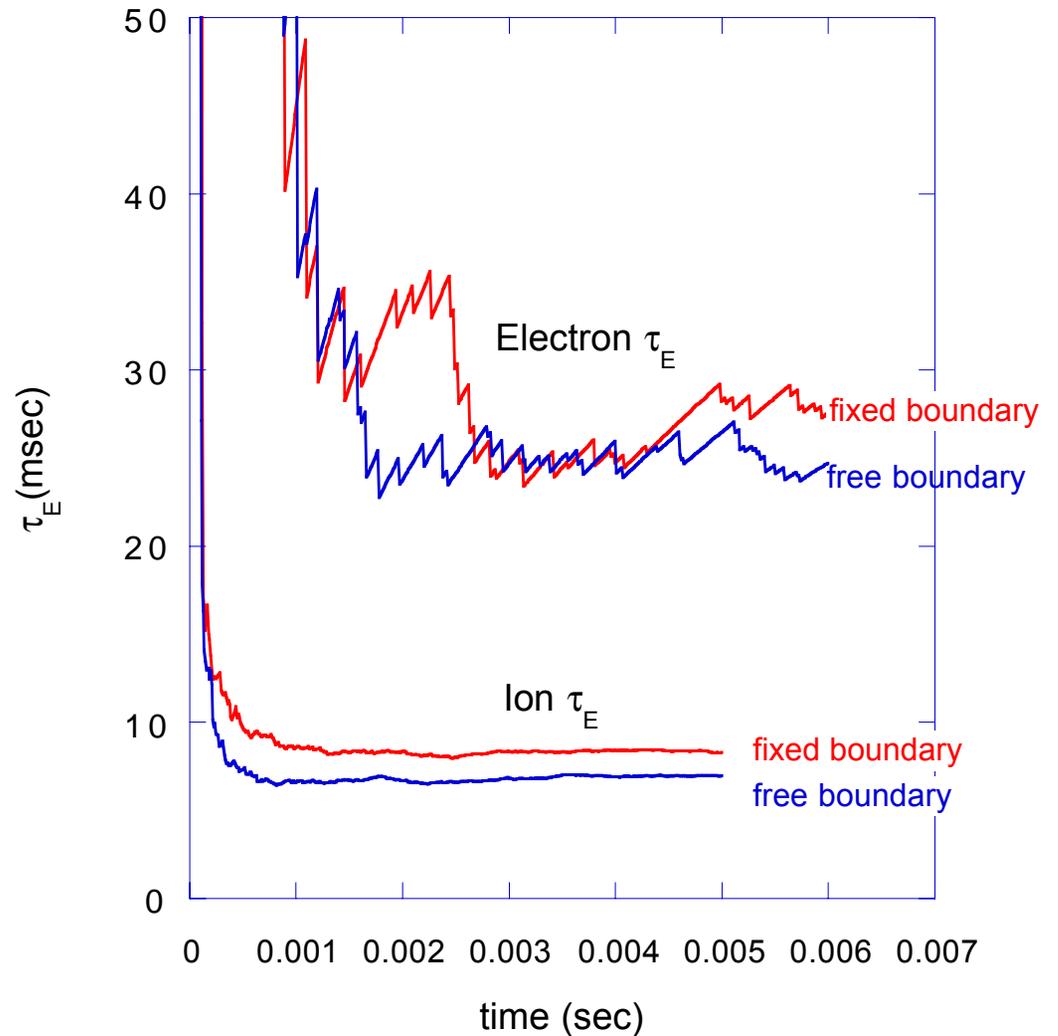
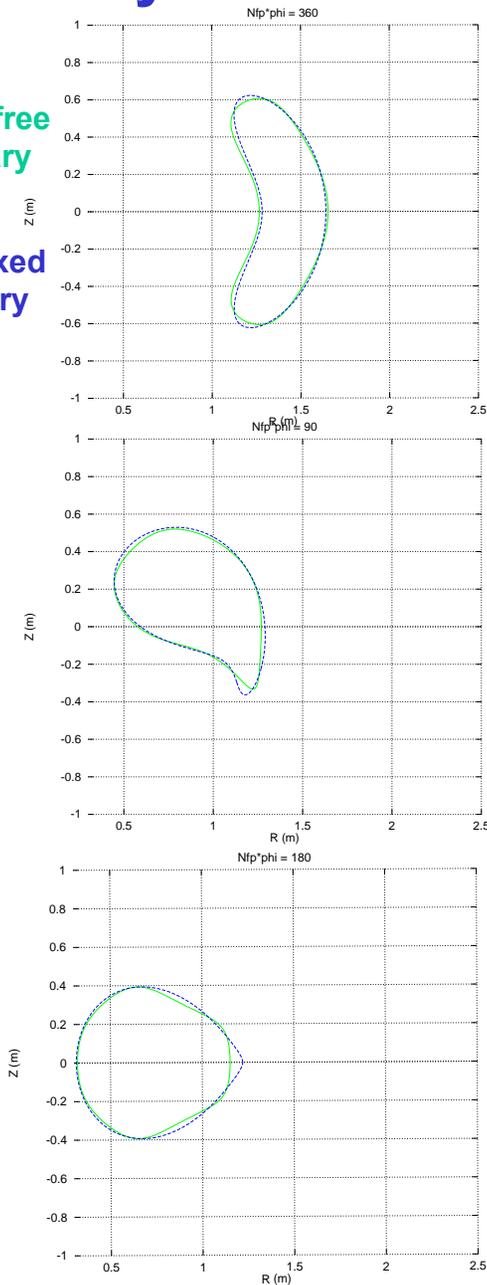


# Free boundary A2.5\_M2\_B1.3 configuration (from coils) yields very similar transport as original fixed boundary case:

Transport analysis

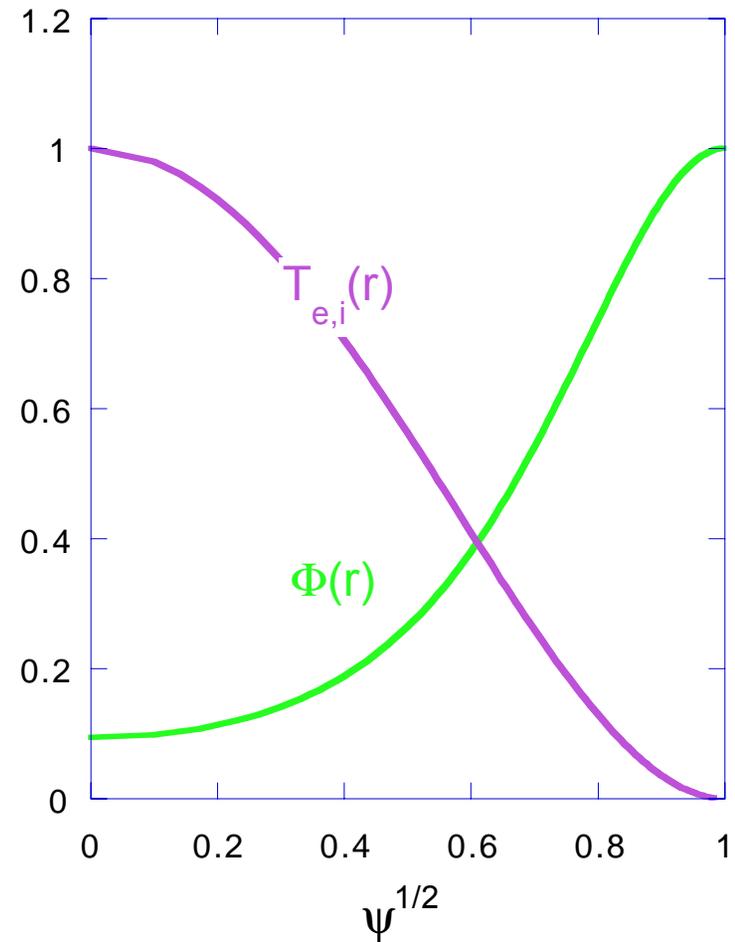
green = free  
boundary

blue = fixed  
boundary



# Profiles used in transport studies

- $n = \text{constant}$ ,  $Z_{\text{eff}} = 1$
- $(1 - r^2)^2 T_e, T_i$  profiles
- $e\phi(r)$  varies inversely with  $kT_e$
- ion root
- electron root to be investigated



# Projected QO/CE heating scenarios include both ECH and ICH regimes

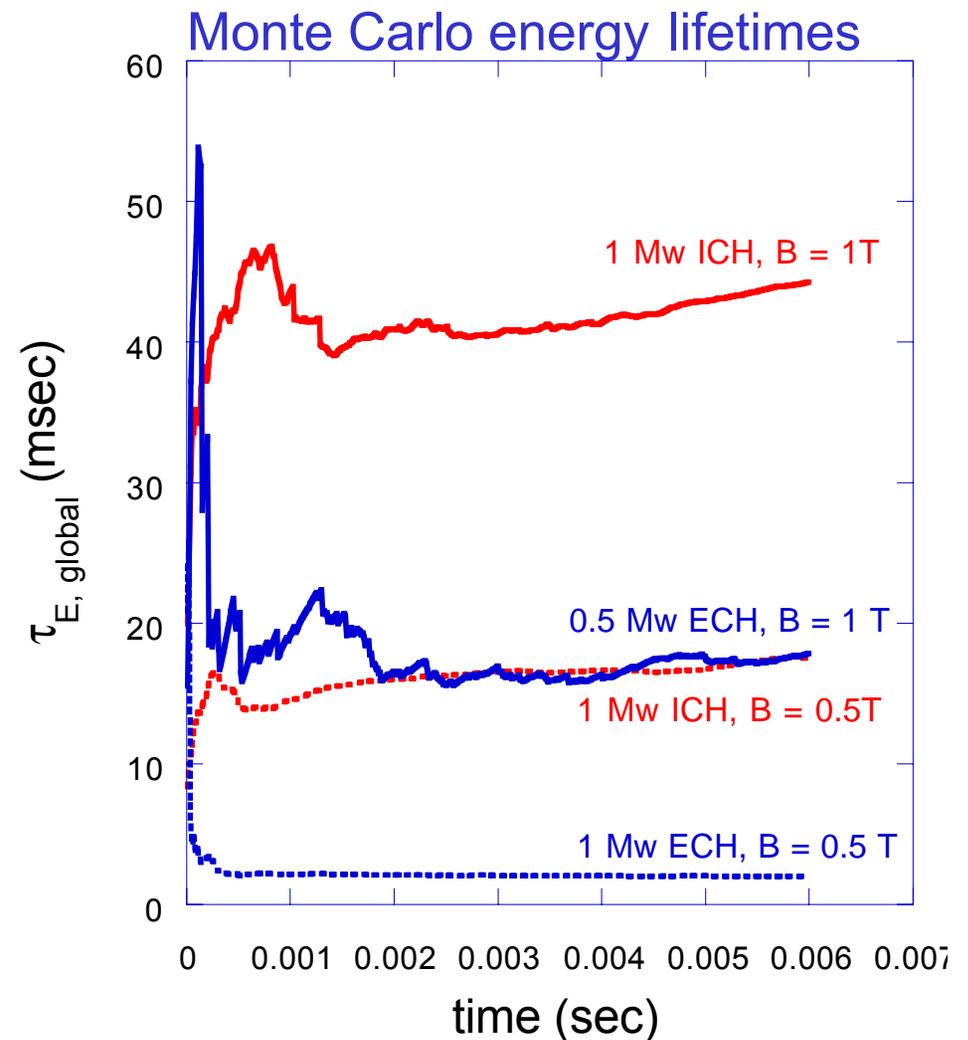
Transport analysis

RF	$P_{\text{heat}}$ (MW)	$\langle B \rangle$ (Tesla)	$n/10^{20}$ ( $\text{m}^{-3}$ )	$T_e$ (keV)	$T_i$ (keV)	$\tau_{\text{ISS95}}$ (msec)	$v_{*elec}$	$v_{*ion}$	$\langle \beta \rangle$
(1) ECH	0.5	1	0.18	1.4	0.15	8.1	0.019	1.6	0.7
(2) ECH	1	0.5	0.045	2.1	0.2	1.5	0.0021	0.22	1
(3) ICH	1	1	0.83	0.5	0.5	11.7	0.68	0.64	2
(4) ICH	1	0.5	0.59	0.4	0.25	5.5	0.75	1.8	3.7

# Confinement in the 2 field period, A = 2.5 configuration covers a range from $\tau_{E,global} = (1.4 \text{ to } 3.6) \tau_{E,ISS95}$ for different ECRF and ICRF heating scenarios

## Transport analysis

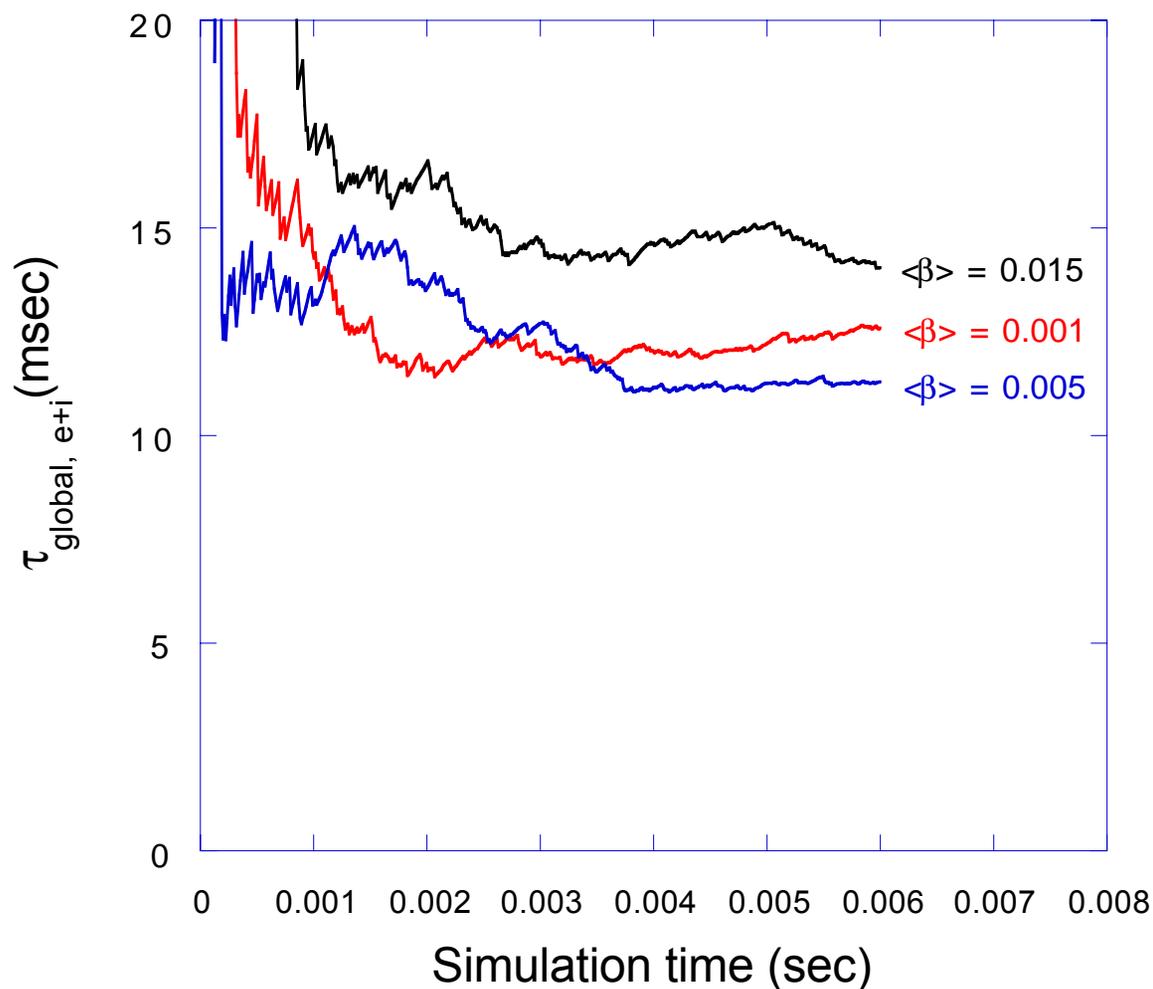
RF	B (Tesla)	$\tau_E^{ion}$ (msec)	$\tau_E^{elec}$ (msec)	$\tau_E^{global}$ (msec)	$\tau_E^{ISS95}$ (msec)
ECH	1	16.2	17.4	16.2	8.1
ECH	0.5	4.27	1.95	2.1	1.5
ICH	1	27	~100	41.7	11.7
ICH	0.5	7.7	~55	16.4	5.5



# Transport analysis in regimes with ( $T_e > T_i$ ) for the 2 field period A=2.5 device shows tendency to improve with increasing $\beta$ :

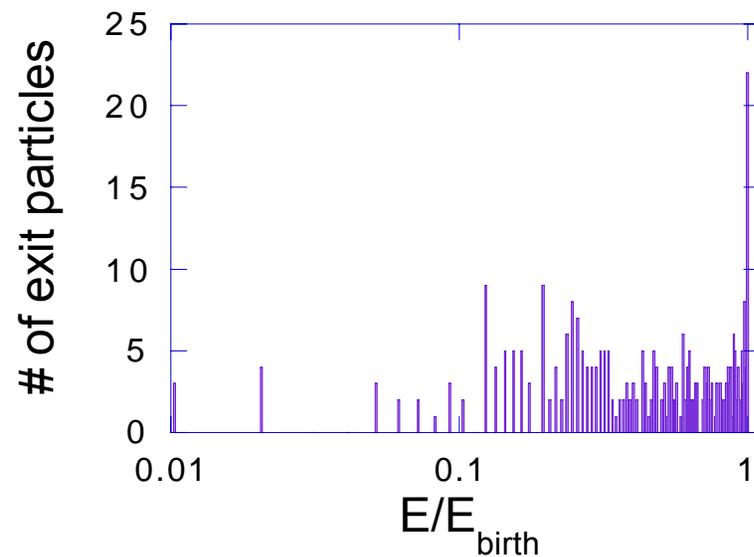
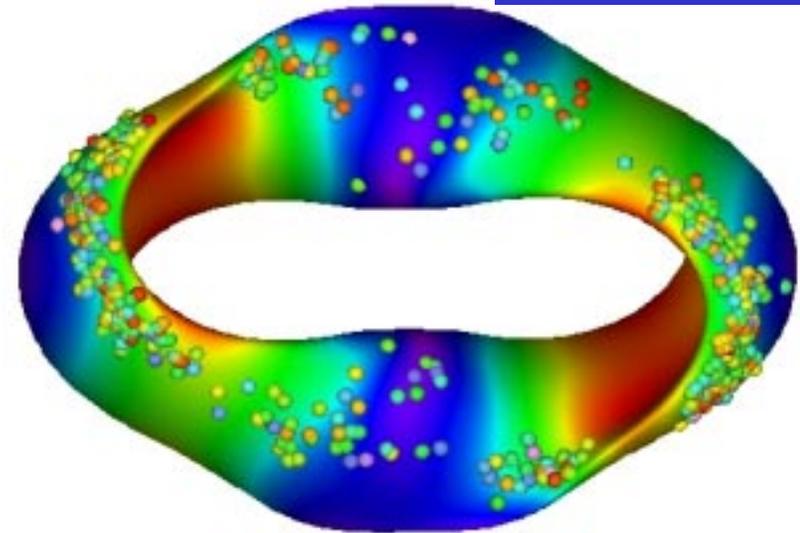
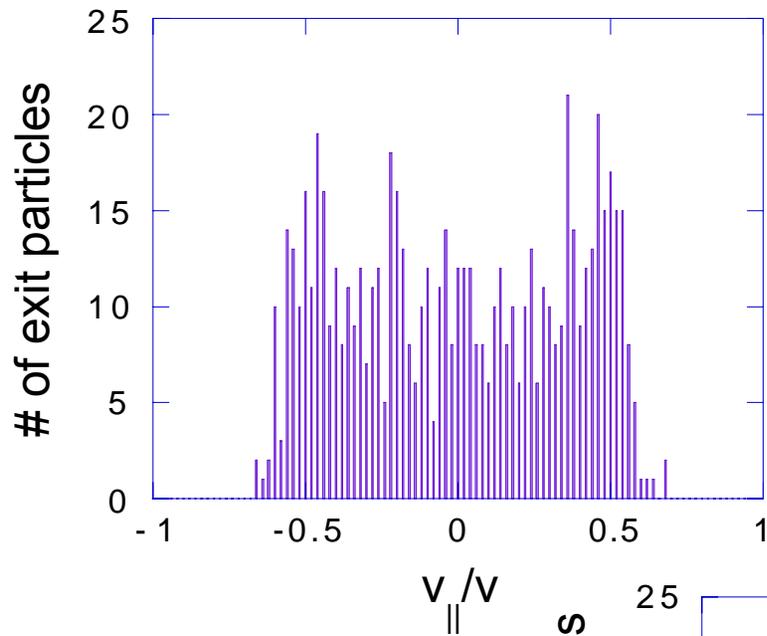
Transport analysis

$$T_e = 1.8 \text{ keV}, T_i = 0.5 \text{ keV}, n = 3 \times 10^{13} \text{ cm}^{-3}$$
$$v_{*e} = 0.019, v_{*i} = 0.233$$



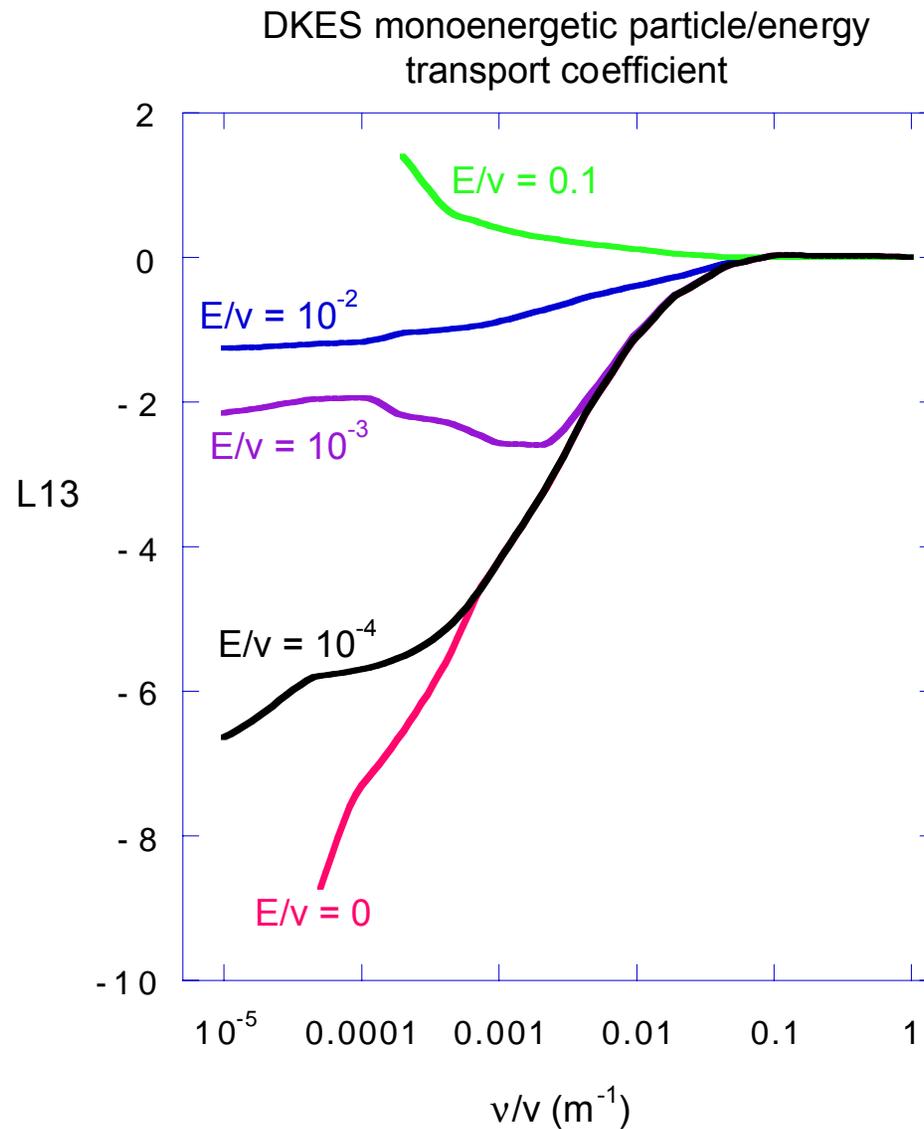
# Energetic particle loss simulations show exit pitch angle, energy and exit position of ions on outer flux surface

Transport analysis



# Collisionality and electric field dependence of bootstrap current coefficient (results shown are for $N_{fp} = 2$ , $A = 2.5$ device)

Transport analysis

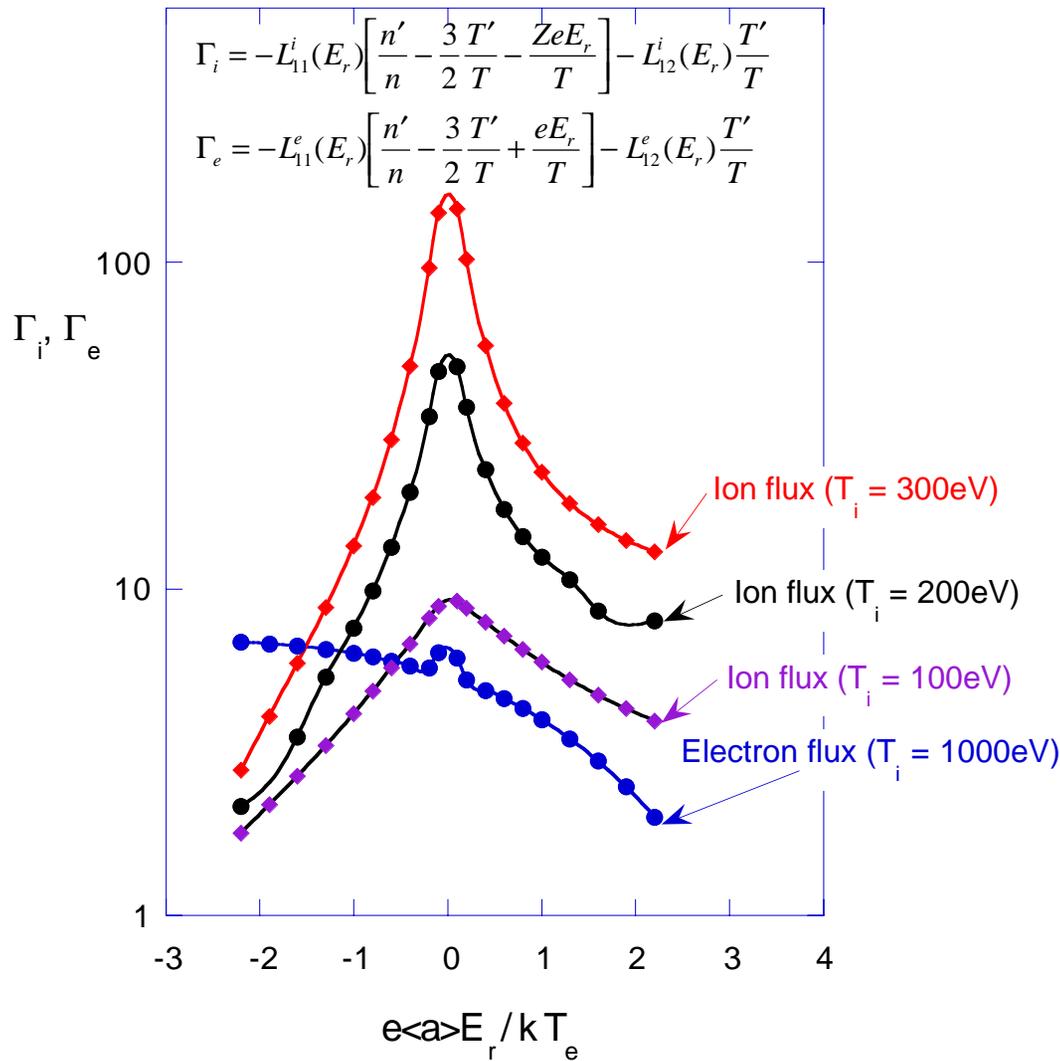


# Self-Consistent ambipolar electric field calculations

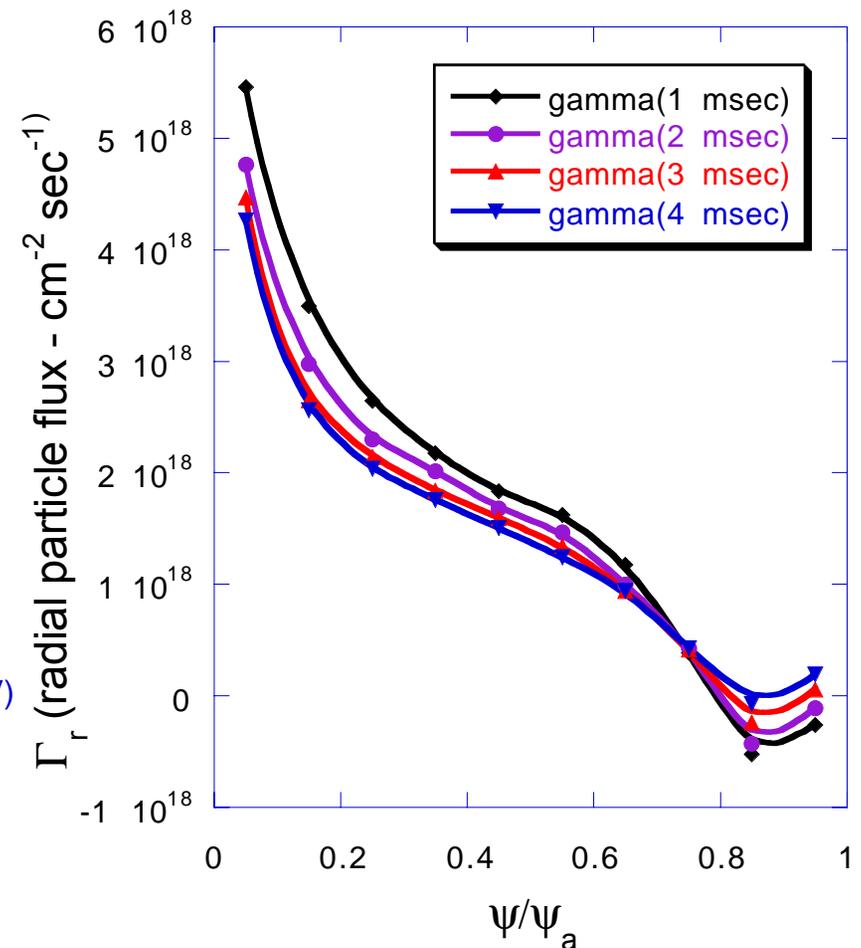
- initially DKES will be used offline for electrons and ion to obtain  $\phi(r)$  for DELTA5D
- next step is to use DKES for electron flux coupled with DELTA5D for ion flux

Transport analysis

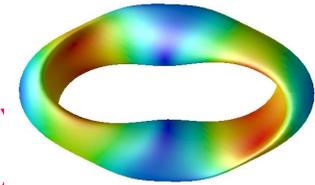
## Ion, electron fluxes from DKES



## Ion flux from DELTA5D

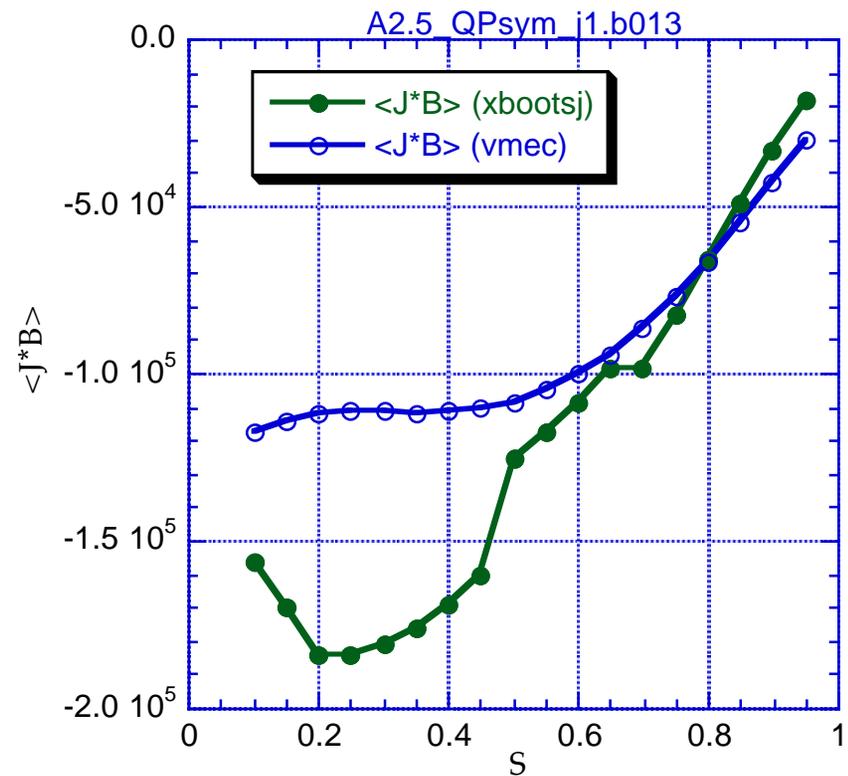
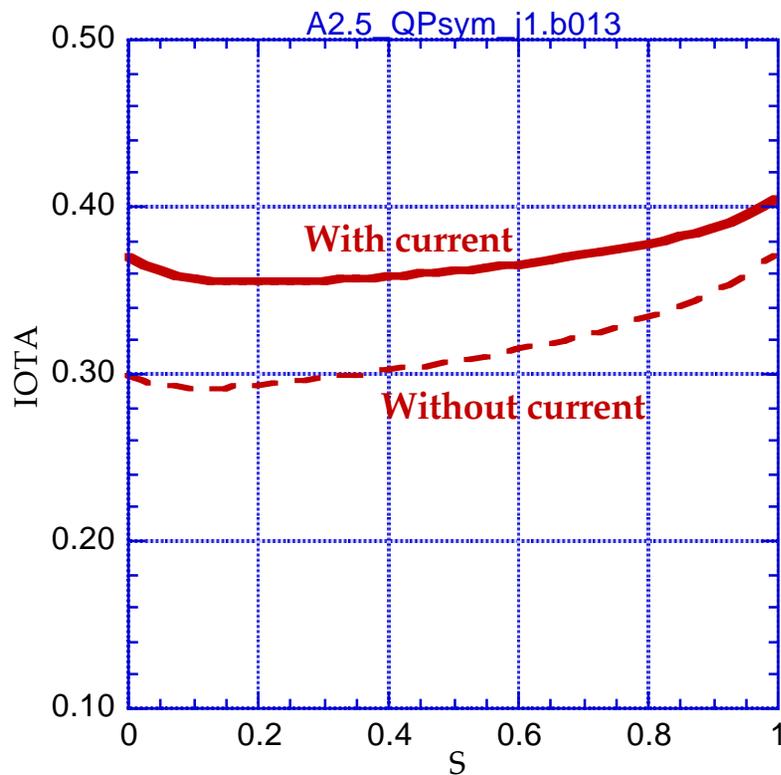


# QP Symmetry Cases (cont.)



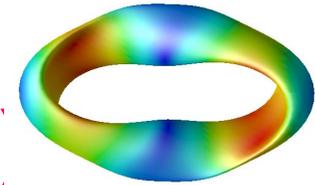
Bootstrap current

- Weak shear with iota mainly from coils

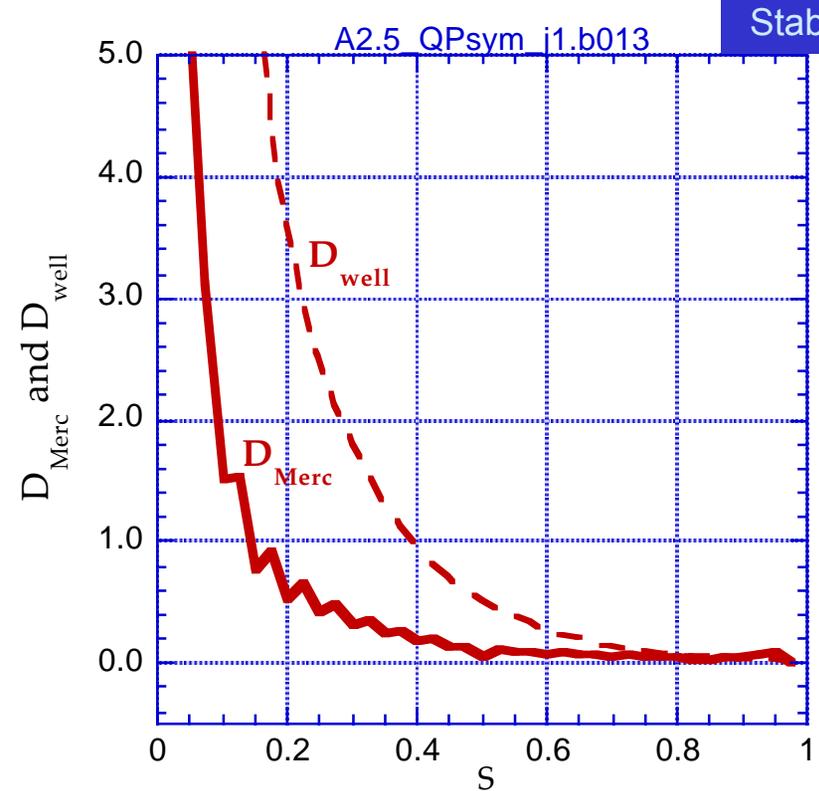
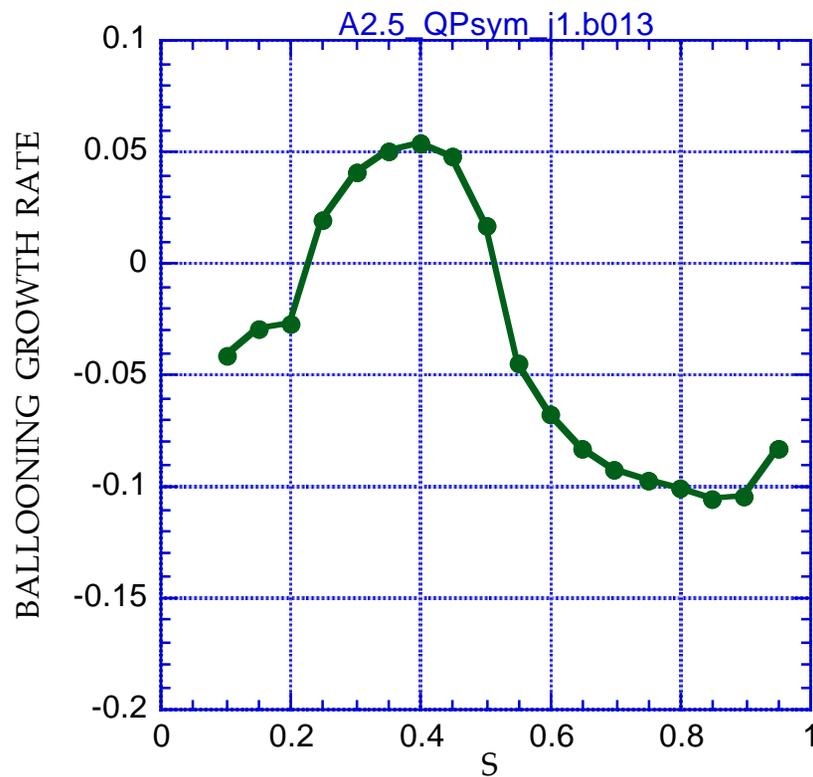


- Bootstrap consistency is fair

# QP Symmetry Cases (cont.)



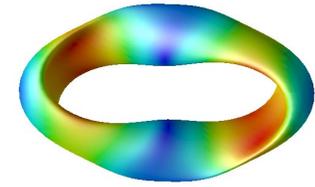
- Pressure profile for this case is ballooning unstable



Stability

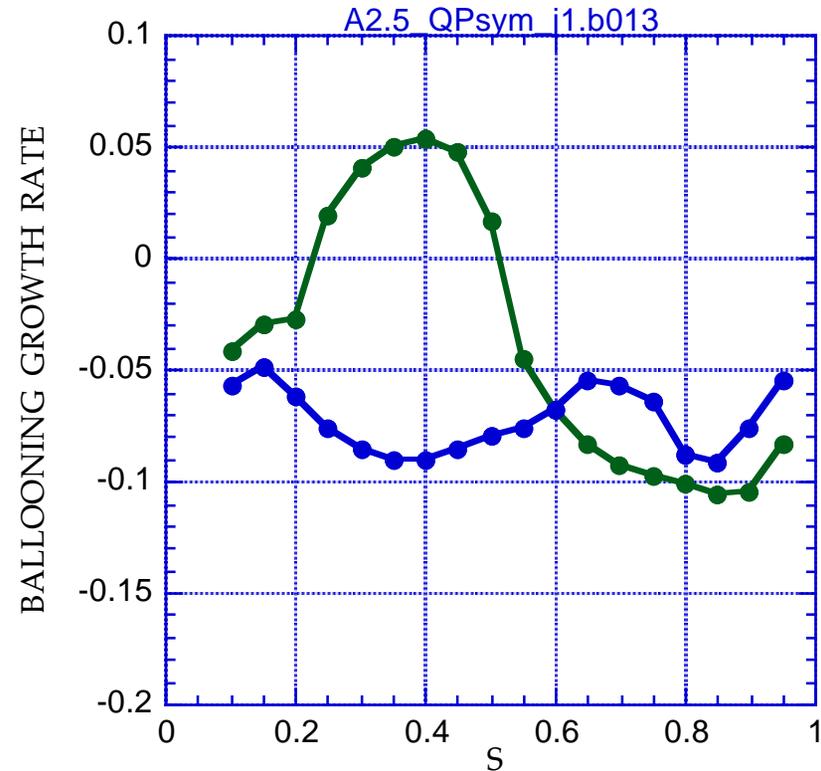
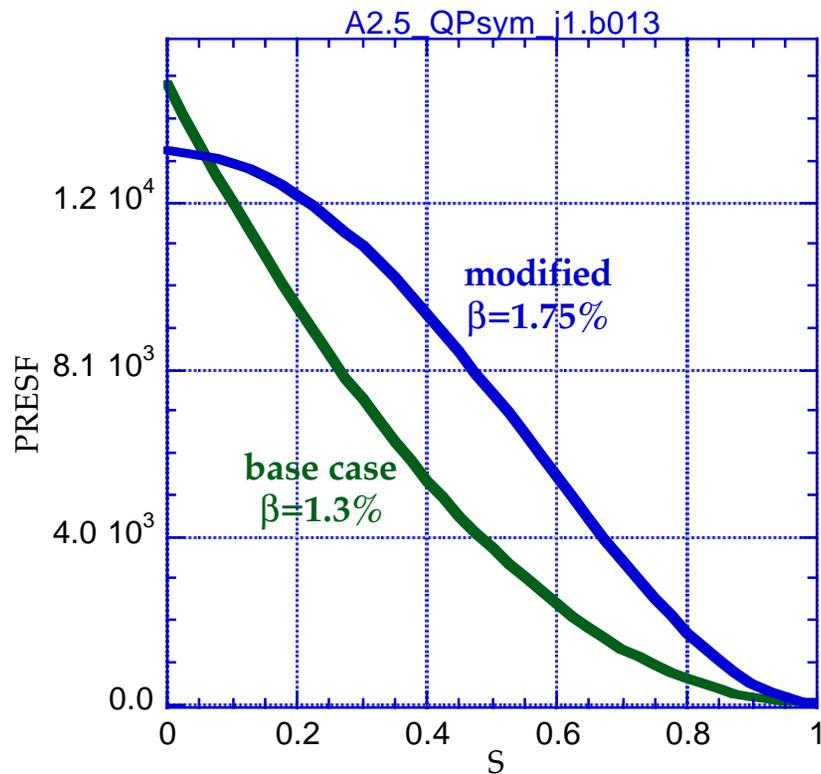
- Mercier stable due to the well at the center

# QP Symmetry Cases (cont.)



Stability

- Modifying the pressure profile however....

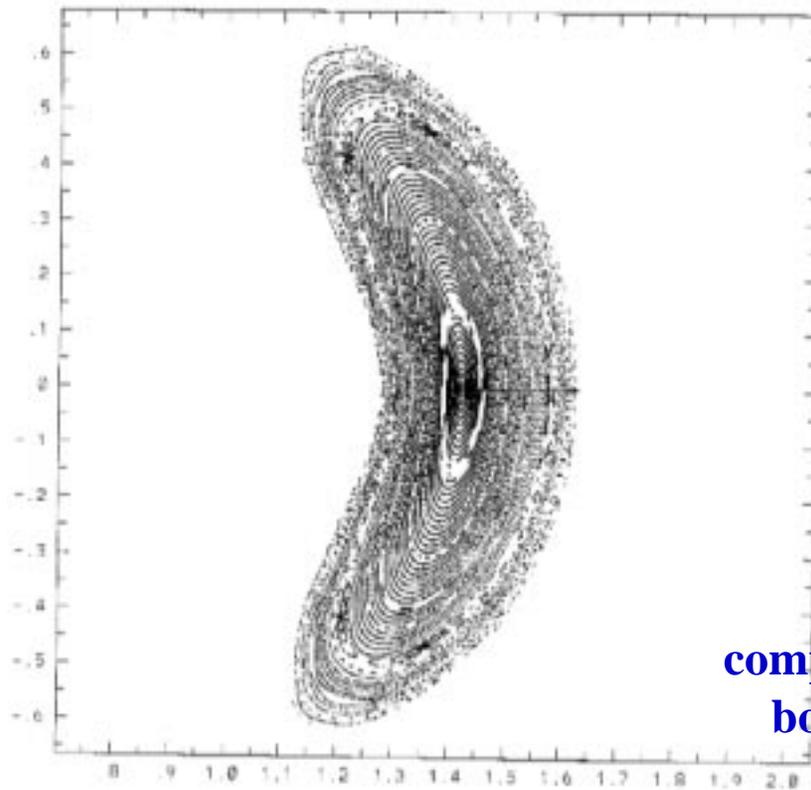


- ... leads to ballooning stability at higher  $\beta$

# PIES Flux Surfaces at $\beta = 1.6\%$

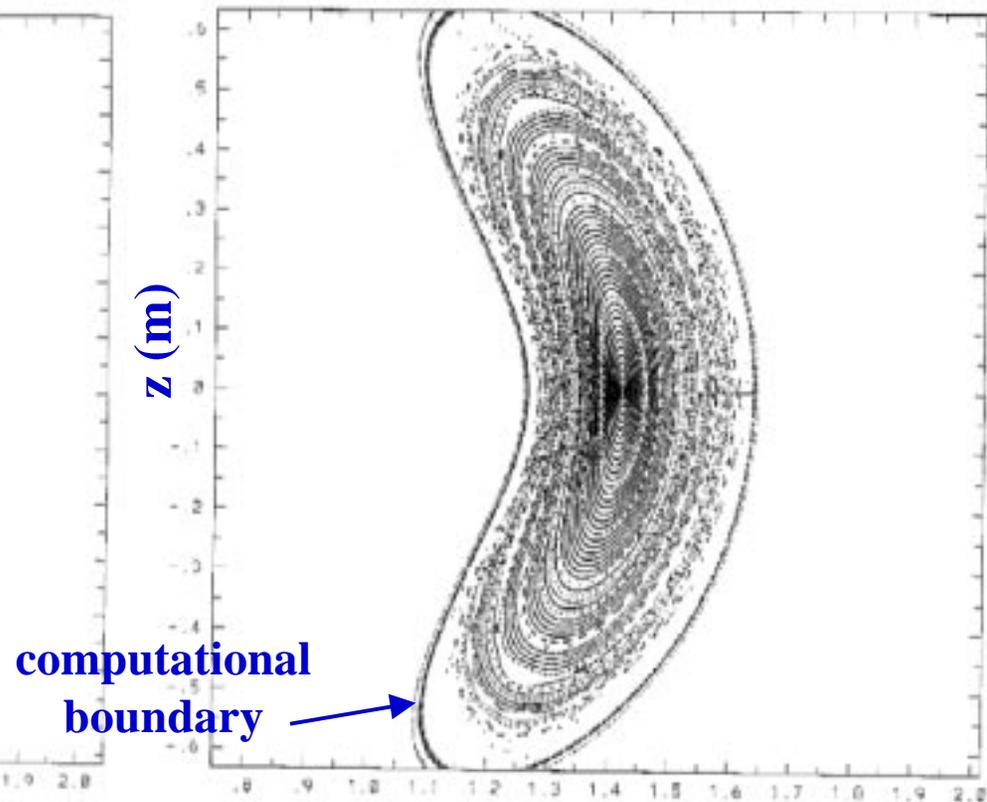
Flux surface fragility

## Fixed Boundary



$R$  (m)

## Free Boundary



$R$  (m)

D. Monticello

# High $\beta$ Configurations

Equilibrium

- A class of configurations with high  $\beta$  MHD stability limits
  - Rotational transform primarily from plasma current
  - Better alignment with self-consistent bootstrap current than advanced tokamaks
  - Stable at higher  $\beta$  than comparable tokamak due to lower current

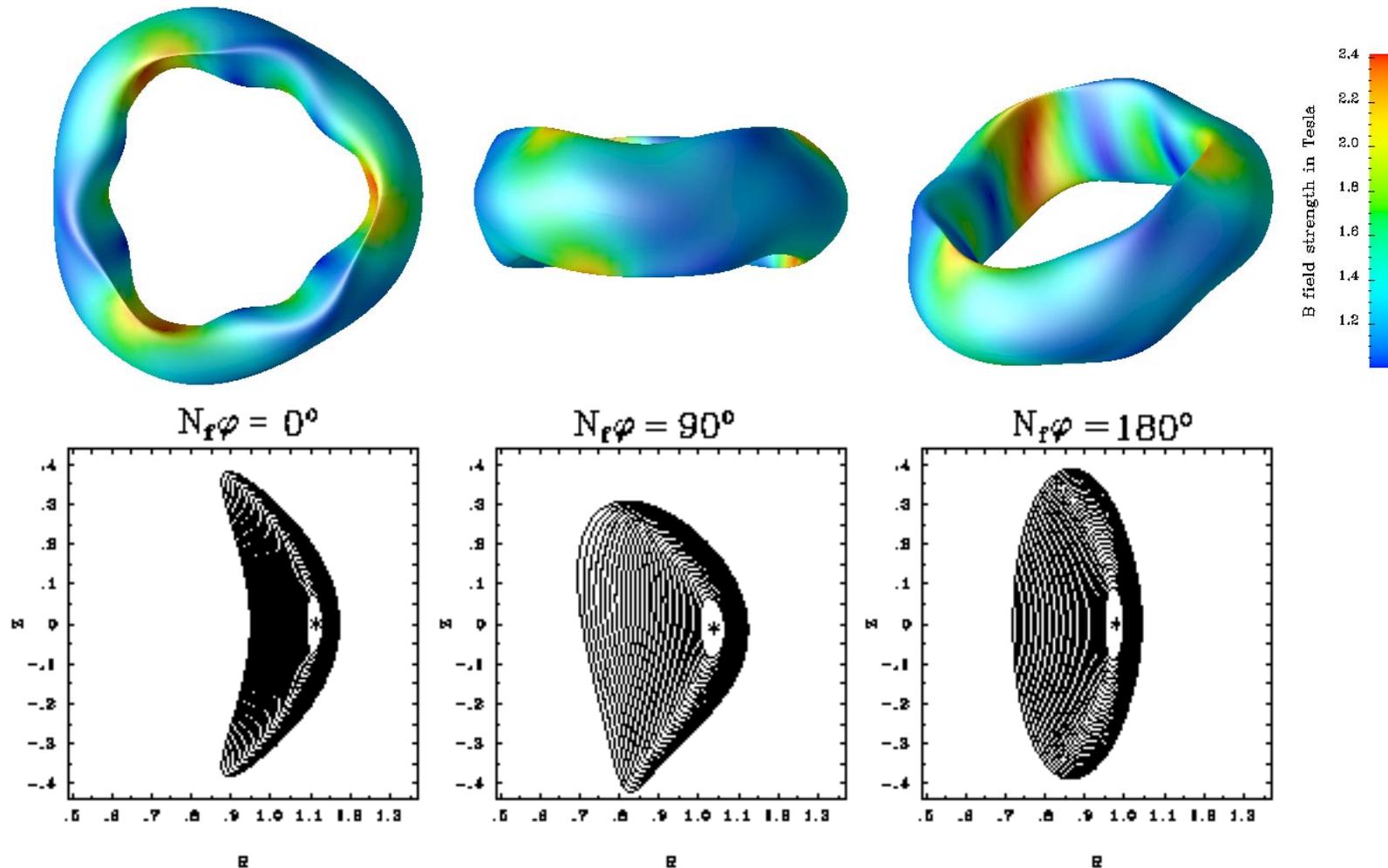
# High $\beta$ Configurations (cont)

- Have obtained 3 field period configurations with ballooning stability up to  $\beta=23\%$ , Vertical/Kink stability up to  $\beta =15\%$  (G. Fu), aspect ratios  $A\sim 3.5 - 4.5$
- For lower aspect ratio ( $A\sim 2.7$ ) 2 field period devices, testing effect of lowering elongation and boosting external rotational transform on vertical stability

# High $\beta$ Case: 3 Field Periods

Equilibrium

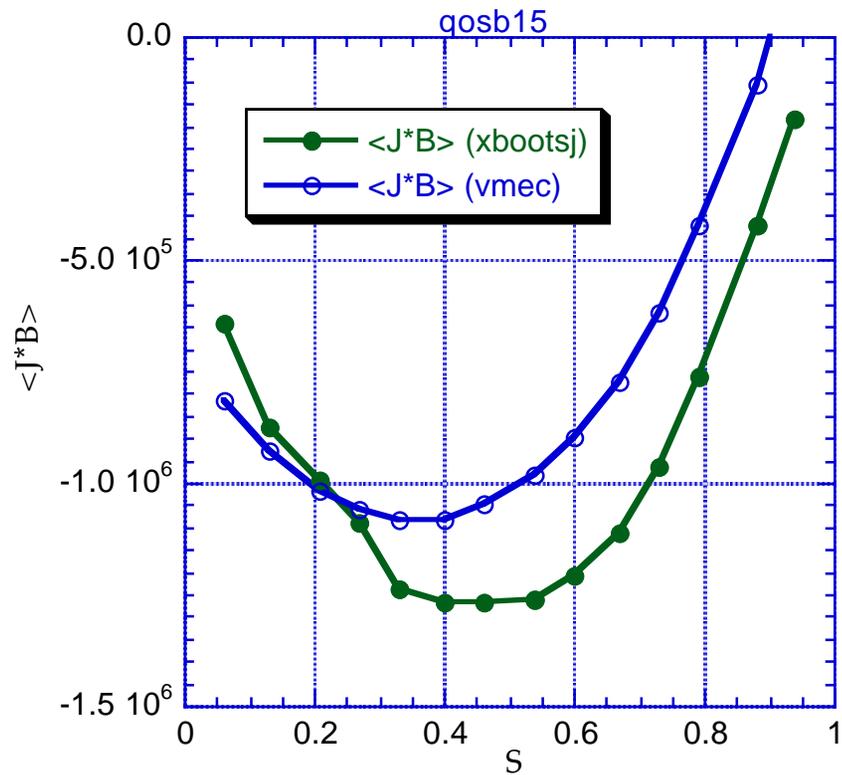
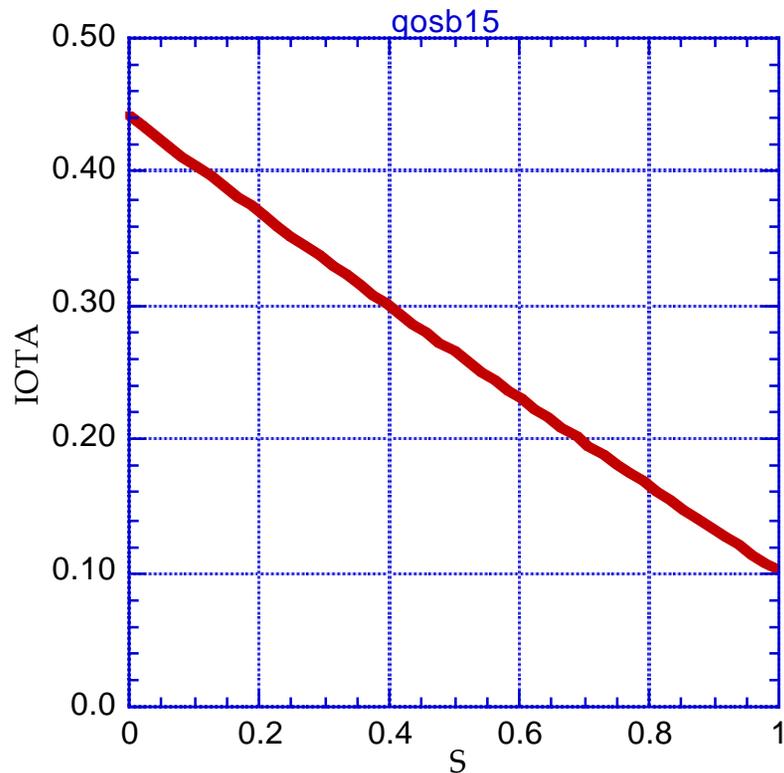
- Outer flux surface/cross sections: 3 FP,  $A=3.7$ ,  $\beta=15\%$



# High $\beta$ Case: 3 Field Periods

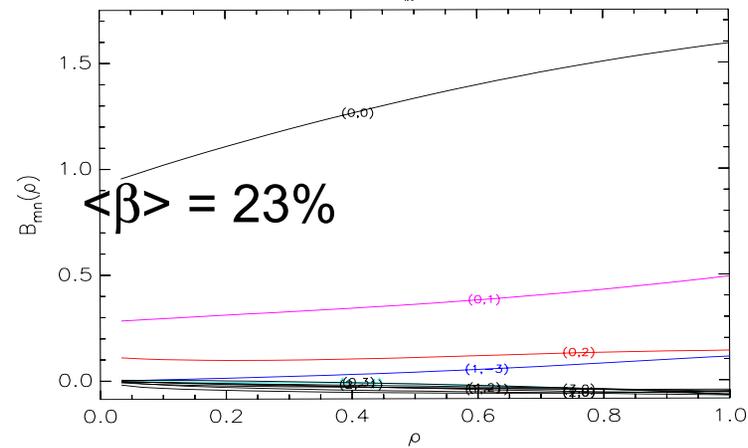
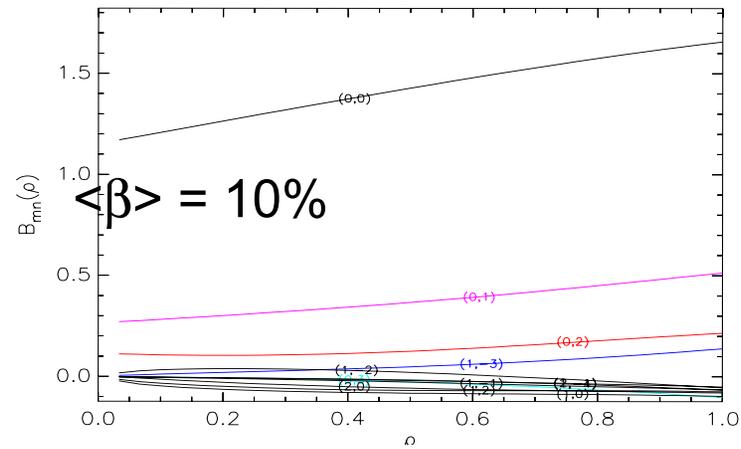
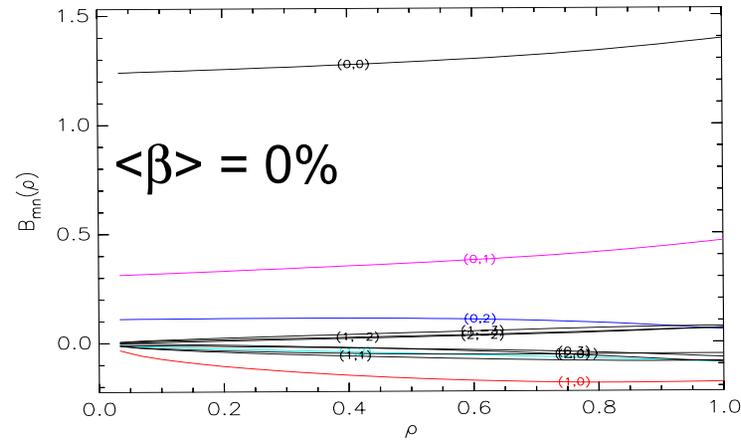
- 3 FP,  $A=3.6$ ,  $\beta=15\%$ ,  $\langle|B|\rangle=1$  T, Max.Tor.Cur.= 155 kA

Bootstrap current



# Variation of $B_{mn}$ Spectra for type II Configurations with $\langle\beta\rangle$

Equilibrium

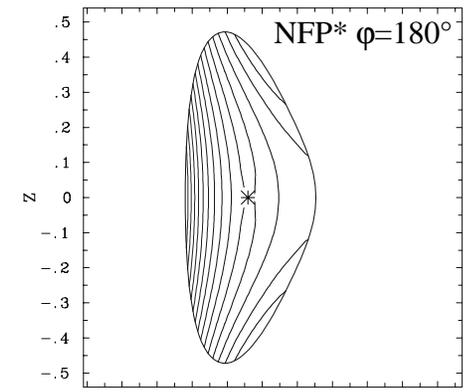
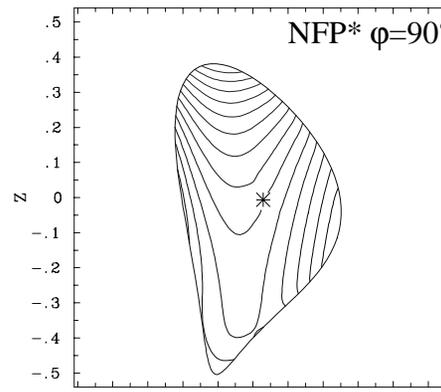
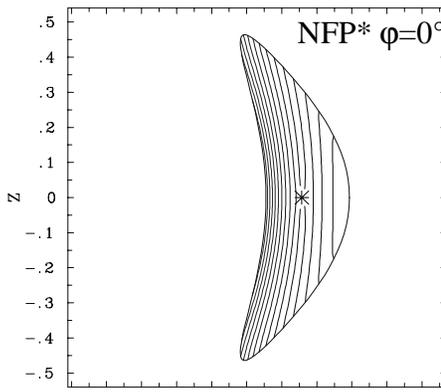


# High $\beta$ Case: $|B|$ /Flux Surface Alignment

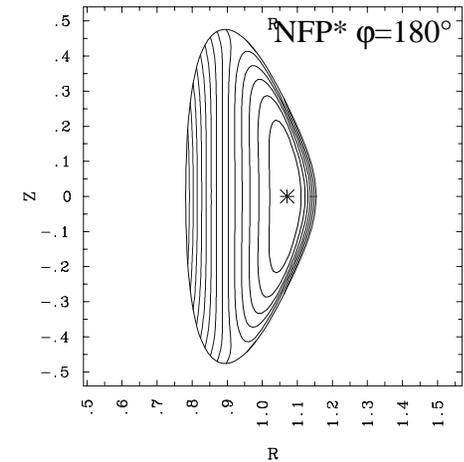
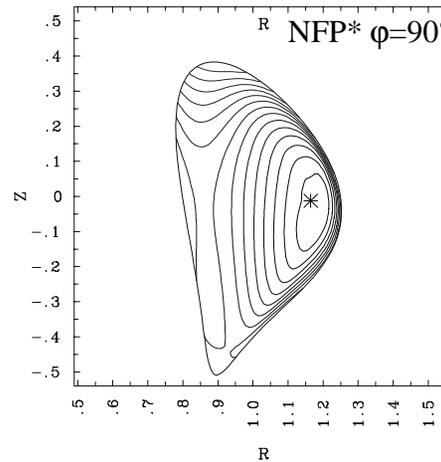
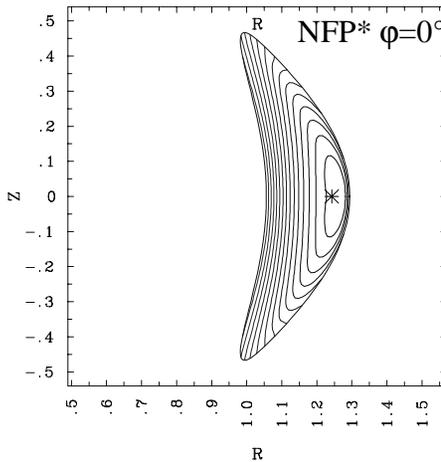
Equilibrium

- $|B|$  surfaces align with flux surfaces at higher  $b$ :

$\beta=0\%$ :



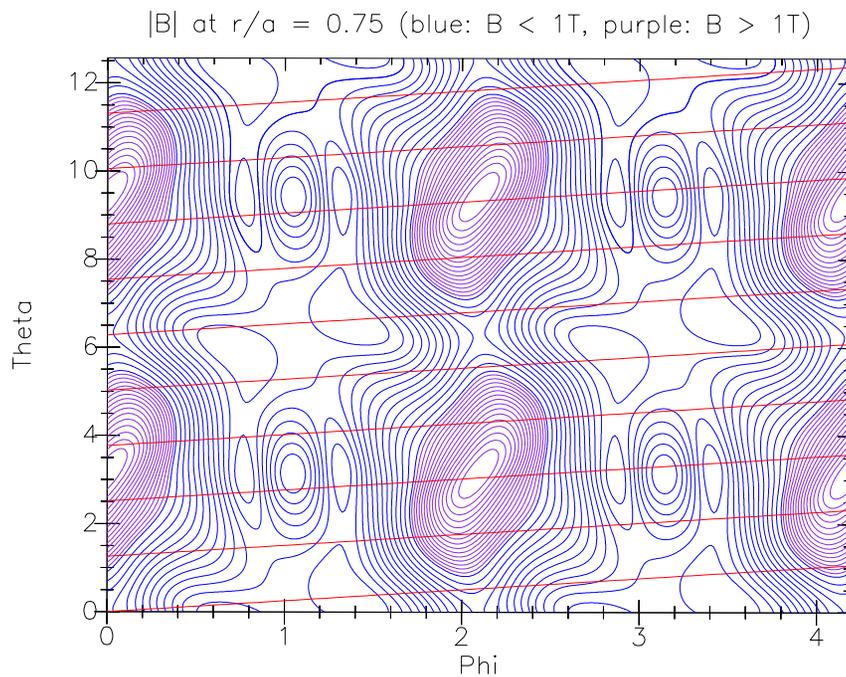
$\beta=23\%$ :



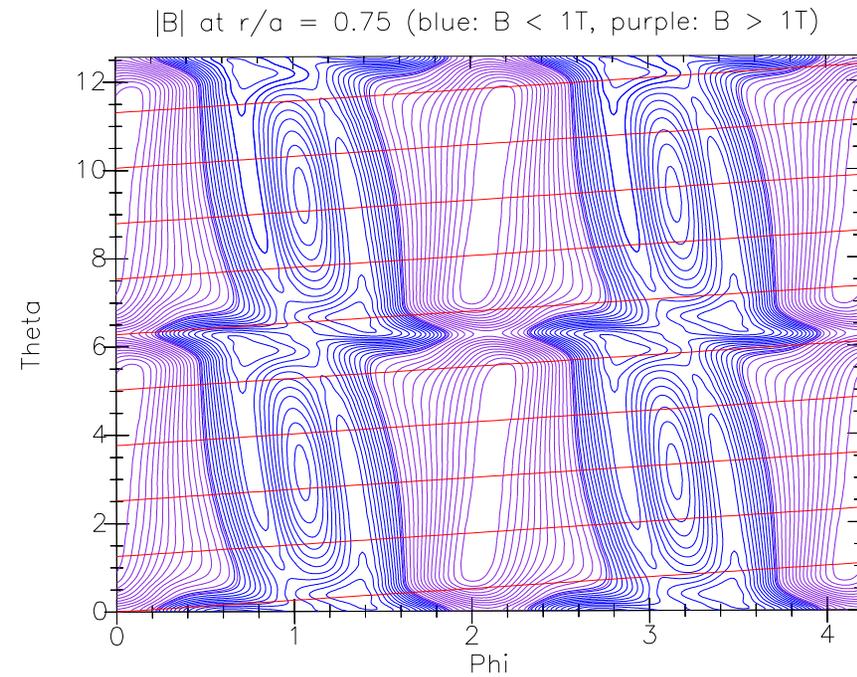
# $|B|$ contours for type II configurations show a significant improvement in poloidal symmetry with increasing $\langle\beta\rangle$

Equilibrium

$\langle\beta\rangle = 0\%$



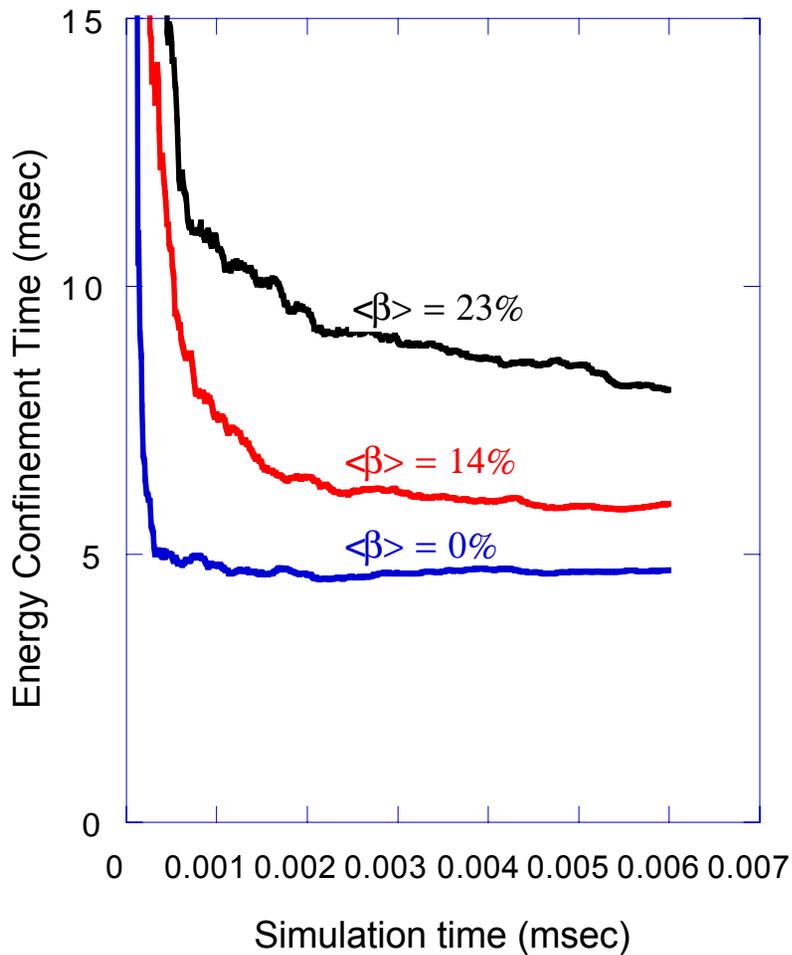
$\langle\beta\rangle = 23\%$



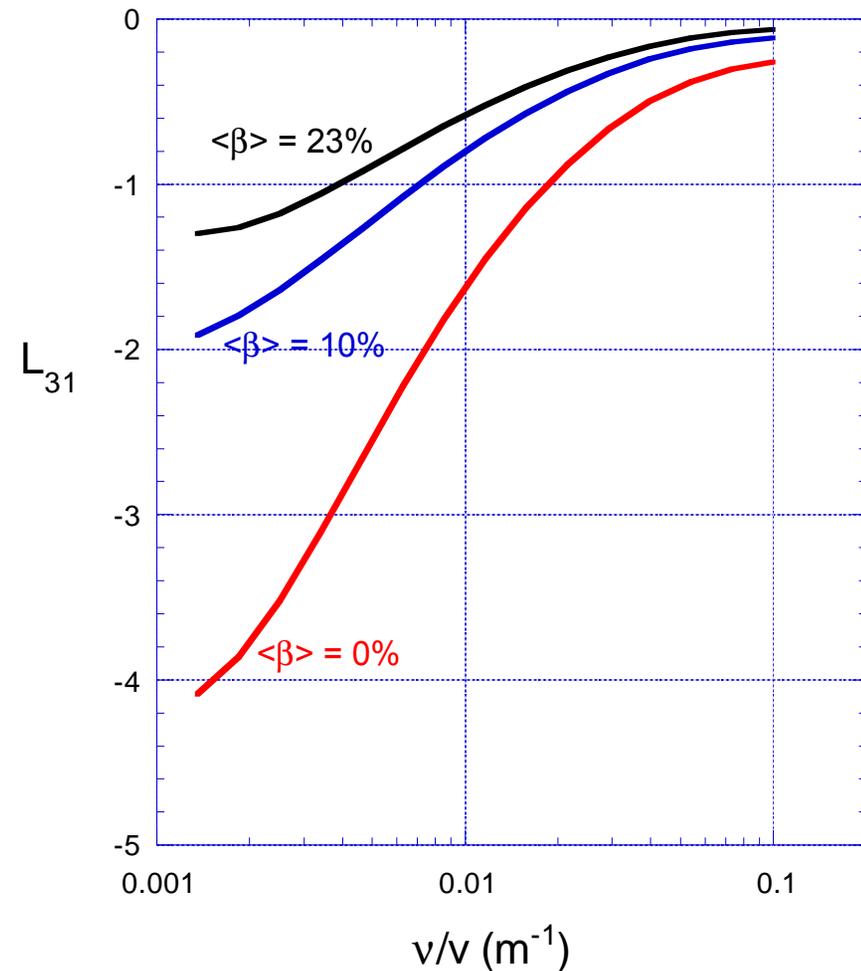
Through its modification of  $|B|$ , high  $\beta$  changes both the thermal neoclassical transport and bootstrap coefficient

Transport analysis

Monte Carlo calculation of energy lifetimes



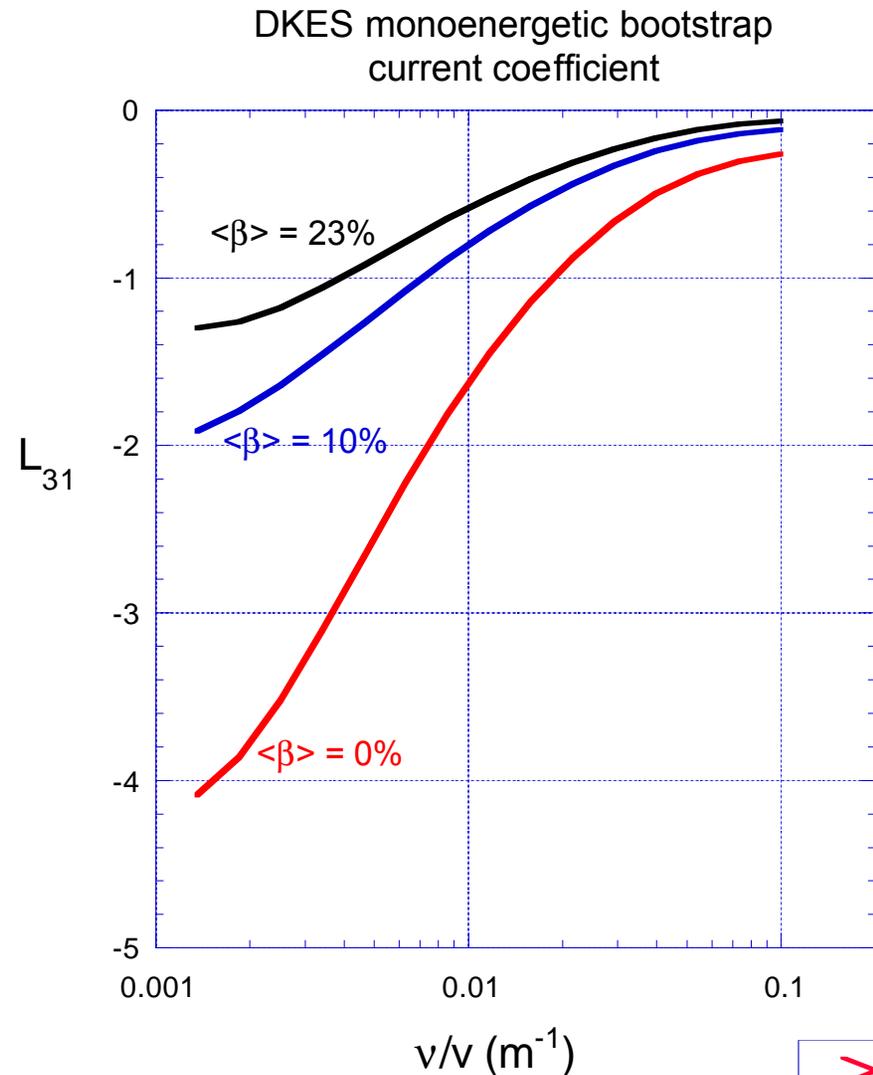
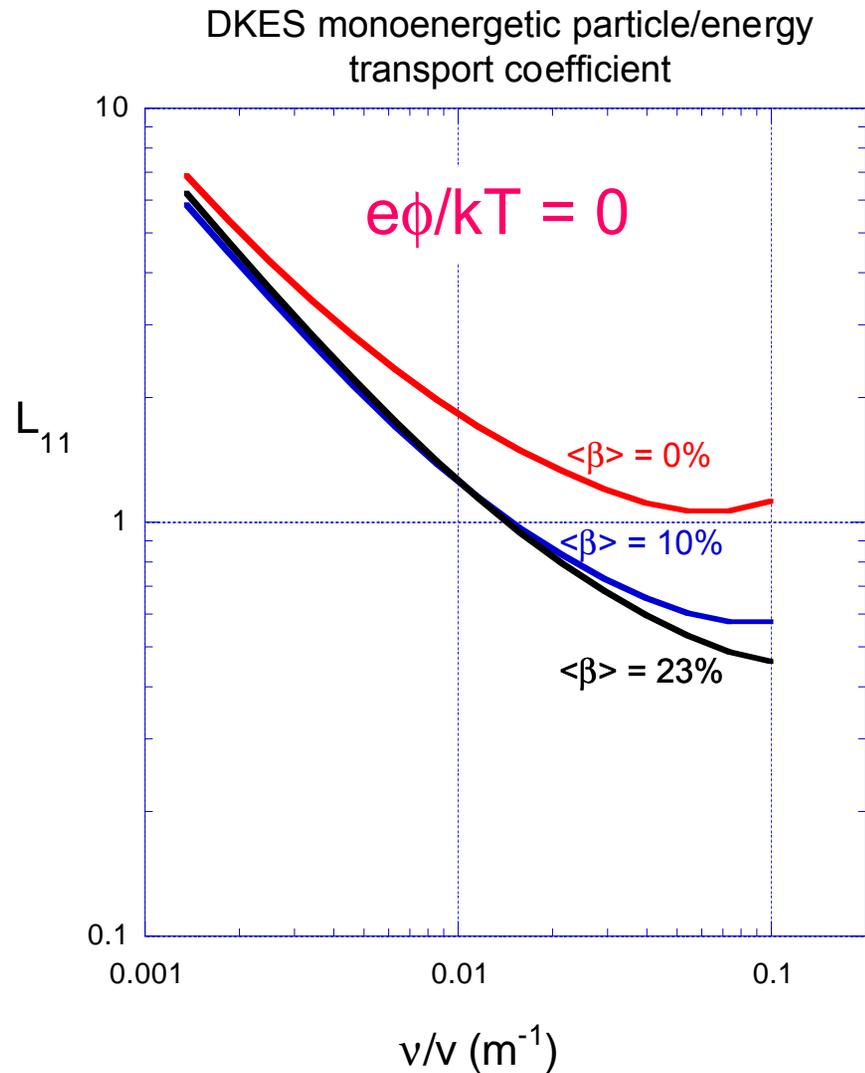
DKES calculation of  $L_{31}$  bootstrap coefficient



# Increasing $\beta$ leads to improved neoclassical transport and to a decreased bootstrap current coefficient.

(results shown are for 3 field period,  $A = 3.4$  device)

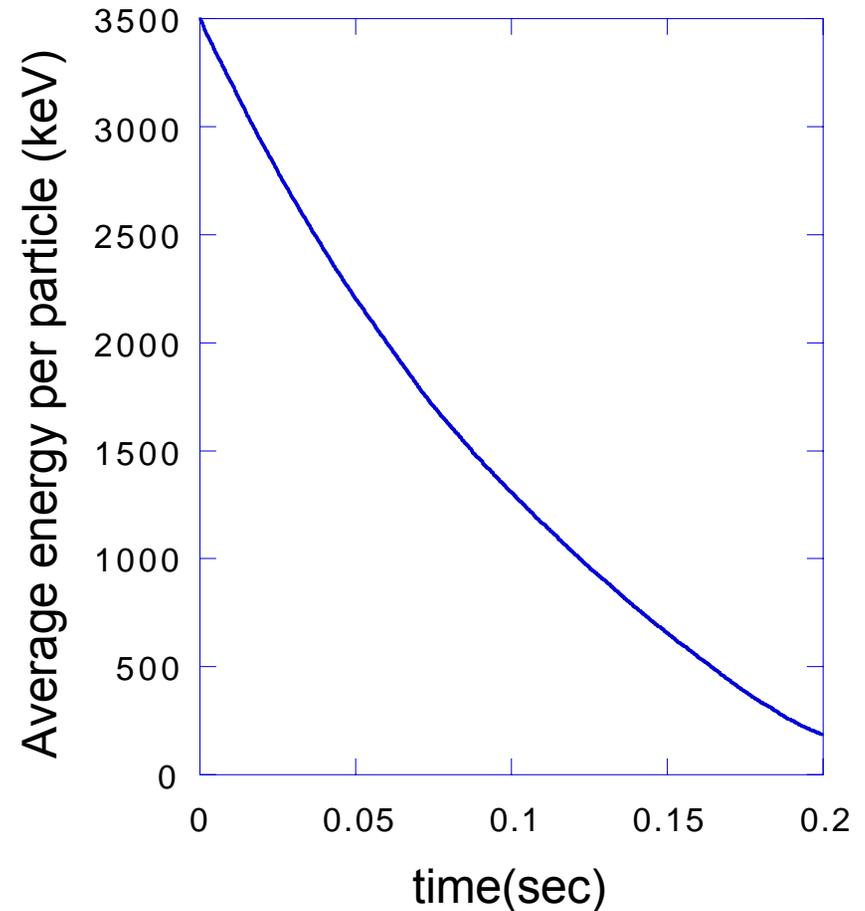
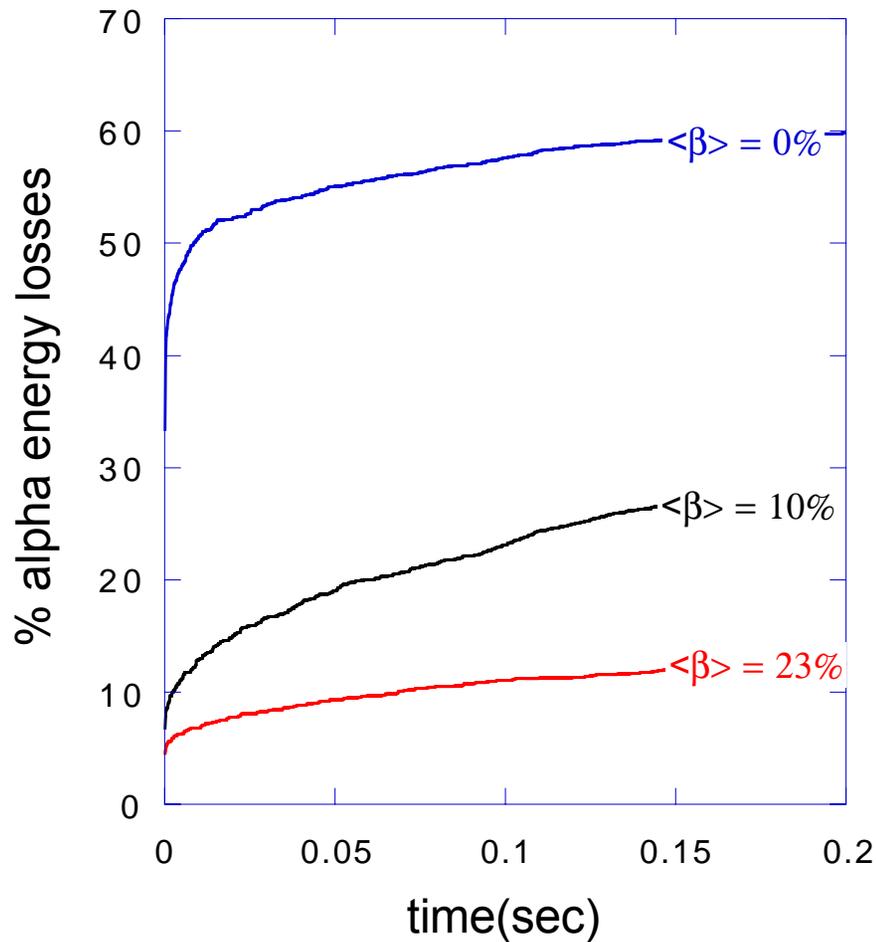
Transport analysis



$\alpha$ -particle slowing-down simulations show these devices indicate very good confinement with increasing  $\beta$ .

Transport analysis

The configuration was scaled to  $\langle B \rangle = 5\text{T}$  and  $R_0 = 10\text{m}$  for alpha confinement studies



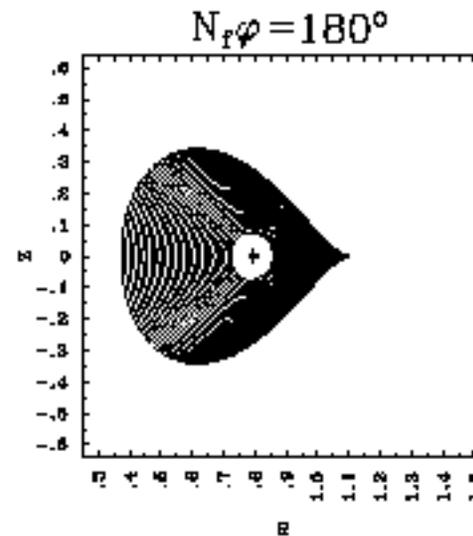
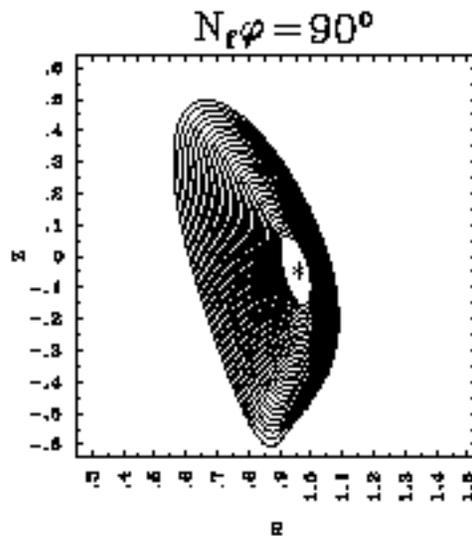
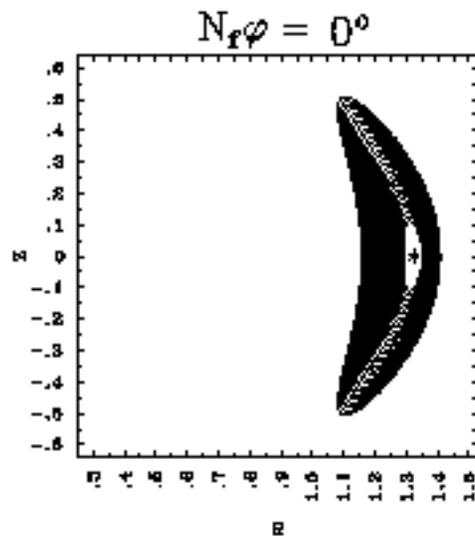
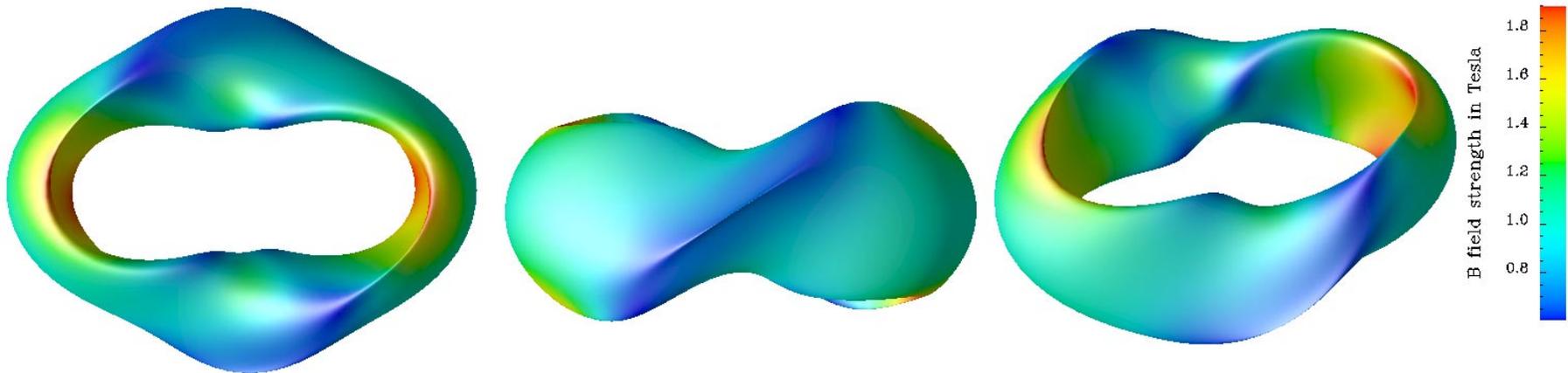
# High $\beta$ Case: Ballooning Stability

- For the 3 FP,  $\beta=15\%$ ,  $A=3.7$  case: (R. Sanchez)
- Edge becomes ballooning unstable for  $\langle\beta\rangle > 0.25\%$ , Second regime stabilization begins at edge above  $\langle\beta\rangle = 0.6\%$ , and stabilizes it beyond 1%.
- The region of the plasma in second regime moves inwards from the edge for increasing  $\langle\beta\rangle$ .
- Plasma becomes totally stable above  $\langle\beta\rangle = 7\%$
- Innermost part of the plasma always in first stability regime.

# High $\beta$ Case: 2 Field Periods

Equilibrium

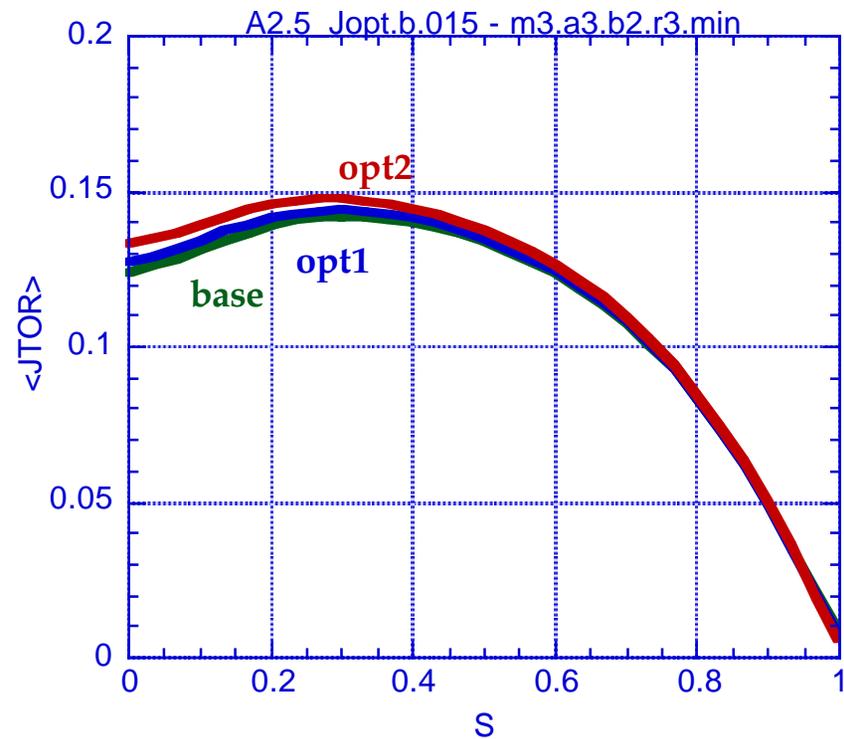
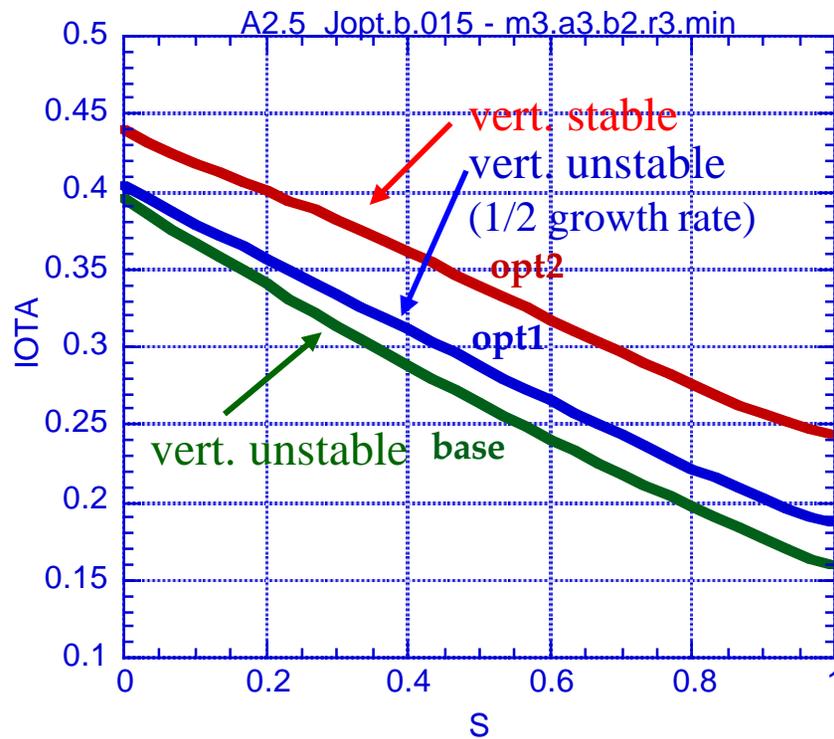
- Outer flux surface/cross sections: 2 FP,  $A=2.7$ ,  $\beta=5\%$



# High $\beta$ Case: MHD Stability

Bootstrap current

- Have been able to affect the stability by increasing the amount of external transform ( $F_u$ )

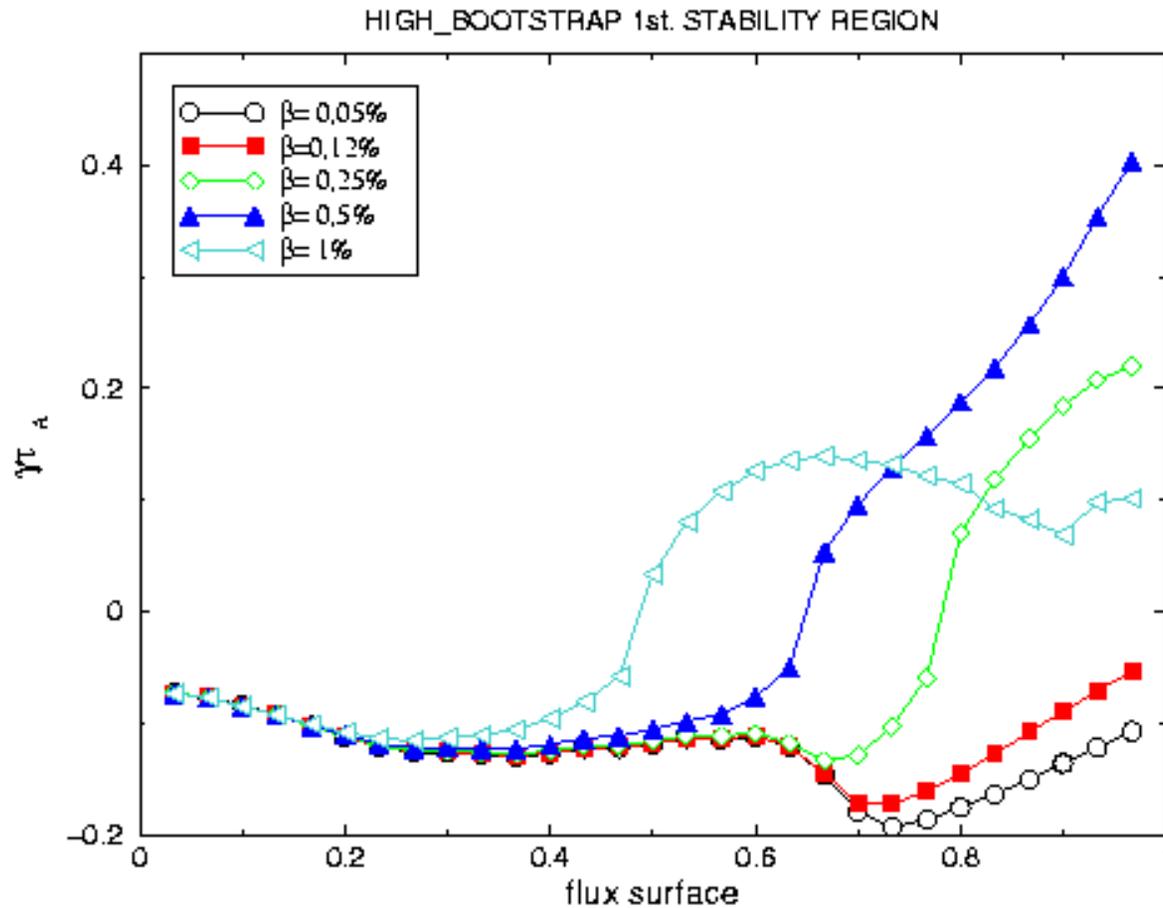


# STABILITY REGIMES

- Edge becomes ballooning unstable above  $\langle\beta\rangle = 0.25\%$ .
- **Second regime stabilization** begins to be effective at edge above  $\langle\beta\rangle = 0.6\%$ , and stabilizes it beyond 1%.
- The region of the plasma in second regime moves **inwards** from the edge for increasing  $\langle\beta\rangle$ .
- Plasma becomes totally stable above  $\langle\beta\rangle = 7\%$
- **Most inner** part of the plasma stays always in **first stability regime**.

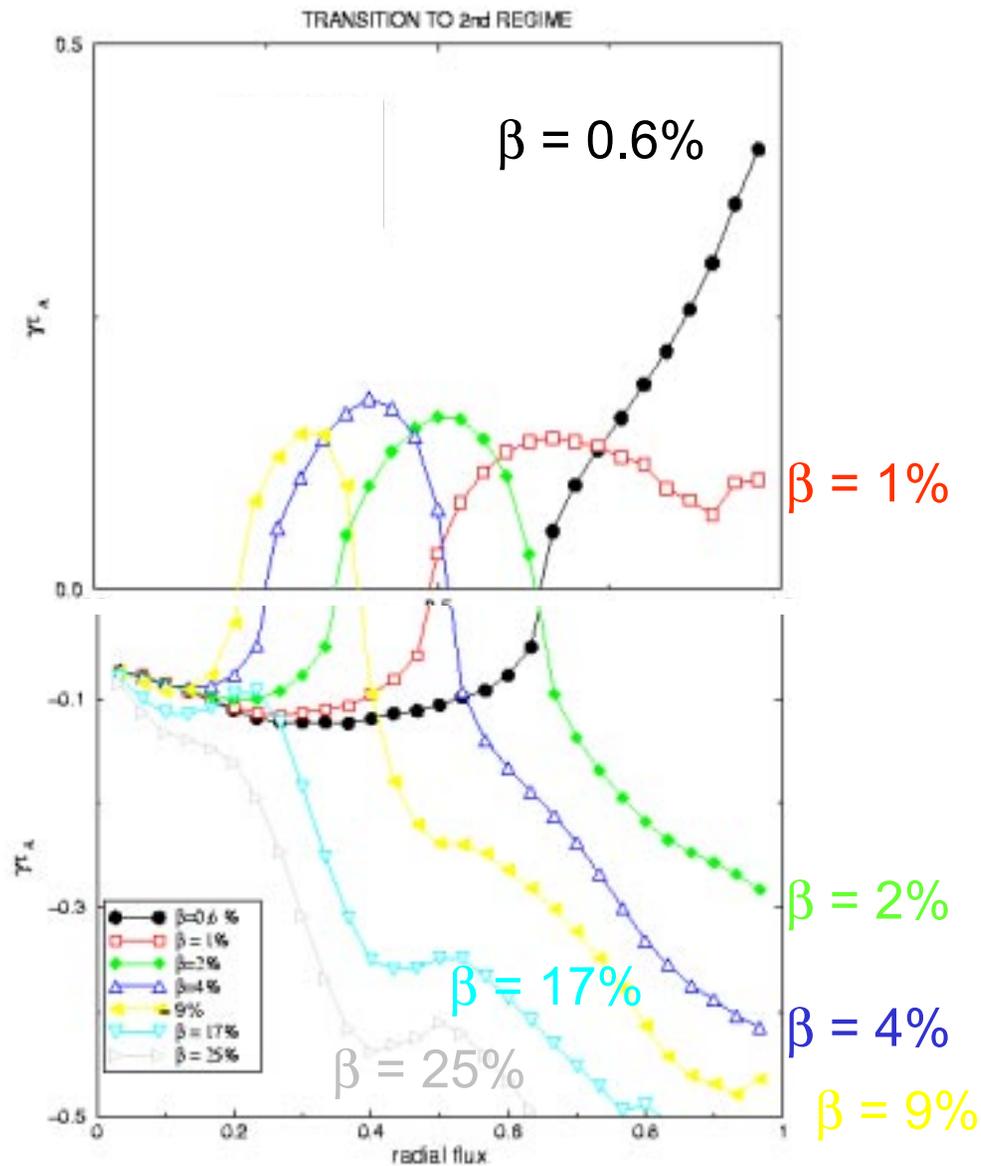
# BALLOONING SPECTRUM (LOW- $\beta$ )

Stability



# BALLOONING SPECTRUM (HIGH - $\beta$ )

Stability

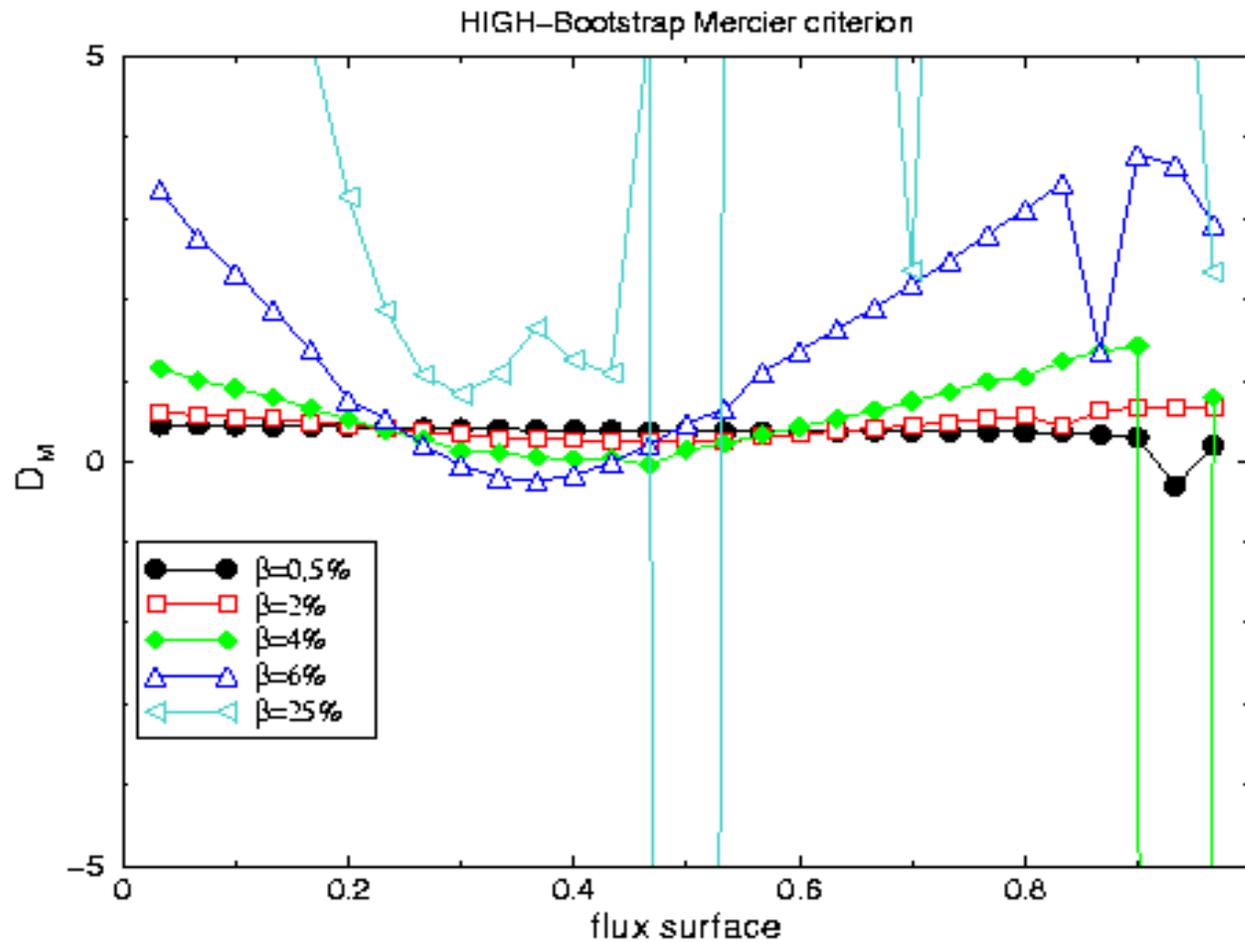


# MERCIER STABILITY

- Plasma remains Mercier stable except for a range of  $\langle\beta\rangle$  between 3-6%.
- Mercier modes are stabilized due to the existence of a large magnetic well that increases with  $\langle\beta\rangle$ .
- The radial region of instability is identical to the region of ballooning instability for the same values of  $\langle\beta\rangle$ .
- This might help to optimize both type of unstable modes in the same way.

# MERCIER STABILITY

Stability



# Summary

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- Attractive 2 and 3 field period devices have been found for  $A = 2.5 - 3.5$ 
  - Attain good confinement by being near quasi-poloidal symmetry
  - Modular coils: good flux surface reconstruction, preserves physics
- Different heating options and magnetic field variation (0.5 – 1T) allow exploration of different confinement regimes
  - ECH:  $\tau_{\text{neo}}/\tau_{\text{ISS95}}$  from 1.4 to 2
  - ICH:  $\tau_{\text{neo}}/\tau_{\text{ISS95}}$  from 3 to 3.6
- Quasi-poloidal symmetry minimizes viscous damping in the direction of the  $E_r \times B$  drifts
  - lower parallel flows
  - influences accessibility of enhanced confinement regimes which rely on  $E_r \times B$  shear

# Summary (contd.)

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- High  $\beta$  configurations offer improved confinement with increasing  $\beta$ 
  - Large fraction of the transform from plasma current
  - Similar to advance tokamak, but bootstrap current is well aligned and not too large (as it is in an axisymmetric device)
  - Stability limits (ballooning, kink, vertical) allow operation at  $\langle\beta\rangle \sim 15\%$  (second regime stability)
  - Have achieved lowest alpha losses ( $\sim 12\%$ ) of any of our configurations