**PRELIMINARY** 

# **Energy Industries of Ohio**

Contract # S005242-F

Modular Coil Winding Forms

# **A-1 Documentation Package**

Part 1 – Metal Tek International Casting Data Package

# 1/3/2006

Note – Documents in red (next page) not yet inserted

# **A-1 Documentation Package**

## List of Documents 1-3-2006

Doc #	Description	#
	•	Pages
1	MTR for weighted average of chemistry – 3 ladles replaced by product	1
	analysis	
2	MTR from Wisconsin Centrifugal	1
3	MTR for C-4 Shim revised 9/24/05	1
4	Lincoln weld metal product conformance spec Lot 3018926/78309	1
5	St Louis Test Lab dated 8/9/05 mech test results at RT & CVN @ 293°k for Lincoln lot 3018926/78309 (Note – page 3 of 3 unrelated & omitted)	2
6	Westmoreland mech test & CVN @ -320°F dated 9/13/05 Lot 3018926/78309	2
7	Westmoreland Tensile test report @ -320°F dated 9-9-05	1
8	St Louis Test Lab dated 10-10-05 – incl. tensile test results @ room temp & Charpy V Notch (CVN) at 77°K & 293°K	3
9	Weld map	9
10	MQS Radiographic Technique for A coils	15
11	MQS Radiographic Inspection Report dated 8/13/05	6
12	MTK Radiographic Interpretation Report dated 10/24	1
13	MTK Radiographic Shooting Sketch for A coils	1
14	C-4 Coil heat treat chart dated 7/26/05	1
15	C-4 Coil stress relief dated 10/29/05	1
16	A-1 Shim heat treat chart dated 06/02/05	1
17	MTK signed MTS A-1 Coil	12
18	MTK signed MTS A-1 Coil shim	
19	CA 1308 – shim chemistry out of spec	2
20	CA 1323 – CA for sulfur & phosphorus readings dated 7/26/05 + addendum dated 8/17/05 – 9/8/05 & 9/30/05	10
21	CA 1324 – Major weld defects	2
22	CA 1347 – Thin wall condition on areas of shell	3
23	CA 1371 Lack of fusion in welds	1
24	Final inspection report A-1 coil – dated 8/30/2005	1
25	C of C for A-1 Coil	1
26	Final Inspection report A-1 Shim	1
27	C of C for A-1 shim	1
28	EIO shipping release for A-1 Coil	1
	Thin Wall Addendum	
i	EIO summary of root cause analysis for thin walled condition	2
ii	3D ScanCo explanation of tolerance shift	5
iii	3D ScanCo rescan of A-1	8
iv	3D Scanco – review of initial scan on A pattern	16
V	EIO evaluation of stocked model for A casting	1
vi	EIO discussion slides on thin wall	16
vii	Preliminary FEA analysis on A-1	4
viii	FEA analysis report from PPPL	16
1/3/06		



## **Carondelet Division**

8600 Commercial Blvd. - Pevely, MO 63070 USA Phone: 636-479-4499 - Fax: 636-479-3399

## **Material Test Report**

## ENERGY INDUSTRIES OF OHIO

Purchase Order Number PPPL-FP-LTS-2

Pattern Number MCWF-A1

CAF Metal Designation CF8MNMnMod

Material Spec CF8MNMnMOD

Weighted average of 3 heats - 29516(39%),29517(23%),29519(38%) Total Weight 32422 lbs.

### Revised 12/5/05

Element	Min	Actual	Max
С	0.04	0.04	0.07
MN	2.3	2.4	2.8
SI	0.0	0.4	0.5
CR	18.0	18.2	18.5
NI	13.0	13.3	13.5
MO	2.1	2.4	2.5
P*	0.0	0.022	0.035
S*	0.0	0.009	0.025
Ν	0.24	0.26	0.28

\*P & S taken from cast on bar, zones 1,2,&3 and analyzed by wet chemistries, ASTM E1019-03 for sulfur and Colormetric for phosphorous.

### PRODUCT ANALYSIS

Results of spectrometer analysis of cast on test bar after spectrometer preventive maintenance performed and at Wisconsin Centrifugal.

\*\*\*Not analyzed on spectrograph.

Element	CAF after PM	WC Analysis	
C	***	0.06	
MN	1.6	1.6	
SI	0.6	.06	
CR	18.2	18.1	
NI	13.5	13.7	
MO	2.4	2.4	
P	0.028	0.027	
S	0.009	0.009	
N	***	0.25	

Cert Number 169470-1

Pour Date 5/24/2005

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

## Superior Quality Engineered Metal Products www.MetalTekInt.Com



# Carondelet Division

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## **Material Test Report**

## ENERGY INDUSTRIES OF OHIO

Purchase Order Number PPPL-FP-LTS-2 Pattern Number MCWF-A1 CAF Metal Designation CF8MNMnMod Material Spec CF8MNMnMOD Analysis performed by Wisconsin Centrifugal Revised 11/3/05

Element	Min	Actual	Max
С	0.04	0.06	0.07
MN*	2.3	1.6	2.8
SI	0.0	0.6	0.7
CR	18.0	18.1	18.5
NI*	13.0	13.7	13.5
MO	2.1	2.4	2.5
Р	0.0	0.027	0.035
S	0.0	0.009	0.025
N	0.24	0.25	0.28

\* See Corrective Action Number 1323.

Cert Number 169470-1 Pour Date 5/24/2005

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

Superior Quality Engineered Metal Products www.MetalTekInt.Com

## **Carondelet Division**

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## **Material Test Report**

## **ENERGY INDUSTRIES OF OHIO**

Purchase Order Number PPPL-FP-LTS-2 Heat Number 29198

Pattern Number SE-141-073 COIL C SHIM (-3 thru -6 Parts) Cert Number S73220-2 and

SE-141-033 COIL A SHIM (-1 thru -6 Parts) Cert Number S76220-1

CAF Metal Designation CF8MNMnMod Material Spec CF8MNMN MOD

Revised 9/24/05

Element	Min	Actual	Max
С	0.040	0.070	0.070
CR	18.000	18.100	18.500
MN	2.300	2.970	2.800
MO	2.100	2.450	2.500
Ν	0.240	0.255	0.280
NI	13.000	13.120	13.500
P*	0.000	0.013	0.035
S*	0.000	0.010	0.025
SI	0.000	0.700	0.700

MN & SI previously reported on CA 1308 and were accepted.

\*P & S taken from test from heat parts were poured from and analyzed by wet chemistry, ASTM E1019-03 for sulfur and Gravimetric for phosphorous.

This report covers the eleven castings poured from heat 29198. Only parts listed above however will be shipped for this order. Each casting has a unique number stamped in the part adjacent to the pattern number to differentiate the part and subsequent reporting that will be traced to the casting.

Specification limits have been updated to latest specification.

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

Pour Date 4/28/2005

**Superior Quality Engineered Metal Products** 

www.MetalTekInt.Com

	-045	ER.316 M.	NIN
Class. EN 12072-99: G 20 16 3 Mn L Customer CK SUPPLY Contact Ernie Simpson Eureka (MISSOURI) 63025 UNITED STATES Chemical analysis (%) C Si Mn P S Cr Ni Mo Cu 0,02 0,4 7,3 0,019 0,001 20,1 16,3 2,9 0,1 Mcchanical tests, all weld metal Mcchanical information Other tests			
Product Class.		Lot/Batch	1,: 3018926/78309 692129
Customer	Contact Ernie Simpson Eureka (MISSOURI) 63025	18 N N N N N N N N N N N N N N N N N N N	450,0 KG P.O.: SL 057549 . SD424496
Chemical ar	nalysis (%)		EN10204 3.1B
0,02 0,4	7,3 0,019 0,001 20,1 16,3	2,9 0,1 (	0,201)
Mechanical	tests, all weld metal		EN10204
Additional in			EN10204
Additional in			
Additional in			
Additional in Other tests			
Additional in Other tests Remarks Che product ide vith a Quality 2 SO 9000/BS 5		29000/	



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METALTEK INTERNATIONAL 8600 Commercial Blvd. Pevely, MO 63070 August 8, 2005 Lab No. 05P-2334 P.O. No. 21324 Page 1 of 3 10

## Attention: CHUCK RUUD

## REPORT OF MECHANICAL TESTS

SAMPLE ID: 1) STOCK# LNM 4455, LINCOLN LOT 3018926/78309 2) STOCK# LNM 4455, LINCOLN LOT 3017006/72262 3) STOCK# LNM 4455, LINCOLN LOT 3012668/82743 4) STOCK# B316NF METRODE, W021735

Sample ID	Original Area Sq. Inches	Reduced Area Sq. Inches	Reduction in Area %	Modules of Elasticity	Yield Strength PSI	Tensile Strengt n PSI		gation le Length) %	
1	1 0.1385 0.08		54.3	24.5 Msi	56900	93900	0.84	42.0	
2	0.1886	0.0935 50	50.4	50.4	24.9 Msi	54900	92100	0.85	42.5
3	0.1909	0.0951	50.2	22.6 Msi	57400	93700	0.83	41.5	
4	0.1901			23.0 Msi	54800	88200	0.75	37.5	

Round, reduced section all weld tensiles

Yield taken at .2% offset

Tested in accordance with ASTM A 370-03a

Identification of tested specimens provided by the client.

chmitz, Director erials Testing

KS/tlv







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METALTEK INTERNATIONAL 8600 Commercial Blvd. Pevely, MO 63070

August 8, 2005 Lab No. 05P-2334 P.O. No. 21324 Page 2 of 3

Attention: Chuck Ruud

## REPORT OF CHARPY IMPACT TEST

MATERIAL (SAMPLE ID): STOCK# LNM 4455, LINCOLN LOT 3018926/78309 STOCK# LNM 4455, LINCOLN LOT 3017006/72262

SPECIFICATION: ASTM A 370-03a

SPECIMEN TYPE: "A" Vee Notch

SPECIMEN SIZE: 10 mm x 10 mm (All Weld)

TEMPERATURE OF TEST: 293°K

## REQUIREMENTS:

ALL WELD	FOOT LBS.	LATERAL EXPANSION	% SHEAF		
78309-7	97	0.074	50		
78309-8	96	0.076	50		
78309-9	108	0.075	50		
Average	100	0.075	50		
ALL WELD	FOOT LBS.	LATERAL EXPANSION	% SHEAR		
72262-7	126	0.098	50		
72262-8	102	0.080	50		
72262-9	123	0.087	50		
Average	117	0.088	50		

Identification of tested specimen provided by client.

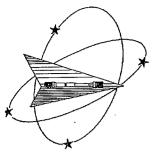
Schmitz, Director aterials Test ng



AN OFFICIAL COPY OF TEST REPORT WILL BE PROVIDED BY THIS LABORATORY ON REQUEST. NOT OFFICIAL WITHOUT THE RAISED SEAL OF ST. LOUIS TESTING LABORATORIES, INC. SEE REVERSE FOR CONDITIONS.

KS/tlv





Westmoreland Mechanical Testing & Research, Inc. P.O. Box 388 Westmoreland Drive Youngstown, Pa. 15696-0388 U.S.A. Fax: 724-537-3151 Telephone: 724-537-3131 Website: www.wmtr.com WMT&R is a technical leader in the material testing industry.



WMT&R Report No. 5-34328 P.O. No. 19386 Rel No.18

Reguisition No. 4934



621-01 & 621-02

September 13, 2005

MetalTek International The Carondelet Division 8600 Commercial Blvd. I-55 Industrial Park Pevely, MO 63070-1528

#### Jim Galaske Attention:

All processes, performed upon the material as received, were conducted at WMT&R, Inc. in accordance with the WMT&R Quality Assurance Manual, Rev. 9, dated 4/1/2000. Subject: The following tests were performed on this order: IMPACT and TENSILE

### TENSILE RESULTS: ASTM E21-03a

Requirements: UTS ksi (Min 95\Max ---) 0.2% YS ksi (Min 72\Max ---) 4D Elong. % (Min 32\Max ---) Modulus Msi (Min 21\Max ---)

SOAK TIME: 5 Minutes

SPEED OF TESTING: 0.0030 in./in./min., 0.0500 in./min./in.

CERTIFICATION

#### MATERIAL: 316 S/S

#### **DISPOSITION:** Acceptable

		Teetlog	Temp.	UTS	0.2% YS	Elong	RA	Modulus	Ult. Load	0.2% YLD.
Reference	Lot No.   Batch	TestLog	remp.	010					11.5	, lbf
	No.   Specimen ID	Number	۴F	ksi	ksi	%	%	Msi	lbf	
	3018926   78309   Tensile	C43938	-320	182.1	128.2	34	24	27.0	17560	12360
Lincoln LNIVI4455	3010920   70309   161300	0.0000	0							B BEBODT

A\U\R: A=ACCEPTABLE, U=UNACCEPTABLE, R=REPORT

**DISPOSITION:** Acceptable

Reference	Lot No.   Batch	TestLog	Orig.	Final	4D Orig	4D Final	Orig. Area	Machine	A\U\R
Kelerence		Number	Dia. (in.)	Dia. (in.)	GL (in.)	GL (in.)	(sq. in.)	Number	
Lincoln   NM4455	3018926   78309   Tensile			0.3048	1.40	1.87	0.09643131	M9	А
LINCOIN LININA455	3010320   10000   Tenene						-UNACCEDT/	DIE D-E	EDORT

A\U\R: A=ACCEPTABLE, U=UNACCEPTABLE,

Requirements supplied by MetalTek International.

Tensile Supervisor Technical Services Manager

September 13, 2005

IOWINGLY OR WILLFULLY FALSIFYING OR CONCEALING A MATERIAL FACT ON THIS FORM ALSE, FICTITIOUS OR FRAUDULENT STATEMENTS OR REPRESENTATIONS HEREIN COULD CONSTITUTE A FELONY PUNISHABLE UNDER FEDERAL STATUTES. THIS CERTIFICATE OR REPORT SHALL NOT BE REPRODUCED CEPT IN FULL, WITHOUT THE WRITTEN APPROVAL OF WMTR, INC

Testing Specialists for Aerospace, Automotive, and Material Testing Fields Locations in Youngstown, PA U.S.A. ~ Tel. (724) 537-3131 and Banbury U.K. ~ Tel. +44 (0) 1295 261211

September 13, 2005

MetalTek International The Carondelet Division 8600 Commercial Blvd. I-55 Industrial Park

Pevely, MO 63070-1528

Attention:

All processes, performed upon the material as received, were conducted at WMT&R, Inc. in accordance with the WMT&R Quality Assurance Manual, Rev. 9, dated 4/1/2000. Subject: The following tests were performed on this order: IMPACT and TENSILE

## IMPACT RESULTS: ASTM E23-02

REQUIREMENTS: Energy (Min 35\Max ---)

Jim Galaske

MATERIAL: Lincoln LNM4455

### SAMPLE TYPE: Charpy V-Notch

0, 111 ==		·······					0/ Ol	A\U\R
Reference	Lot No.   Batch	TestLog	Sample	Temp.	Energy	Mils	% Shear	AUUK
	No.   Specimen ID	Number	Size	°F	ft-lbs	Lat Exp	Fracture	
	3018926   78309   Cvn-1	C43939	Standard	-320	56 .	18	<u>,</u> 40	Acceptable
	3018926   78309   Cvn-2		Standard	-320	52	18	40	Acceptable
				-320	53	12 ·	40	Acceptable
Lincoln LNM4455	3018926   78309   Cvn-3	043941	Januaru	020	L			

P.O. Box 388

Westmoreland Drive

CERTIFICATION

Telephone: 724-537-3131

Youngstown, Pa. 15696-0388 U.S.A.

## Requirements supplied by MetalTek International.

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Tensile Supervisor Technical Services Manager

September 13, 2005

WMT&R Report No. 5-34328 P.O. No. 19386 Rel No.18

Requisition No. 4934

CCREDITED

621-01 & 621-02



Page 1 of

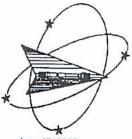
### **DISPOSITION:** Acceptable

Westmoreland Mechanical Testing & Research, Inc.

Website: www.wmtr.com

WMT&R is a technical leader in the material testing industry.

Fax: 724-537-3151



Westmoreland Mechanical Testing & Research, Inc. P.O. Box 388 Westmoreland Drive Youngstown, Pa. 15696-0388 U.S.A. Telephone: 724-537-3131 Fax: 724-537-3151 Website: www.wmtr.com WMTOR is a technical leader in the material testing industry.



Section 1 of 1

Reg. No. 5394

WMT&R Report No. 5-29323

June 17, 2005

CERTIFICATION

MetalTek International The Carondelet Division 8600 Commercial Blvd. I-55 Industrial Park Pavely, MO 63070-1528

Attention: Rick Suria

Subject:

All processes, performed upon the material as received, were conducted at WMT&R, Inc. in accordance with the WMT&R Quality Assurance Manual, Rev. 9, dated 4/1/2000. The following tests were performed on this order: TENSILE

TENSILE RESULTS: ASTM E21-03a

SOAK TIME: 5 Minutes

SPEED OF TESTING: 0.0030 In./in./min., 0.0500 in./min./in.

MATERIAL: Metaltek CF8MNMnMOD

Sample	TestLog	Temp.	UTS	0.2% 45	Elona	DA	Madulus	Orde	1.0.	0.2% YLD.					DISI	POSITION	: Repor
	Number	۰F	ksi	ksi	%	%	Msi	Codes	Ibf		Orlg. Dia. (in.)		4D Orig			Machine	ANUNR
A1 (Z1)	C03040	-320	165.1	95.5	51	37	25.9		33210	19210	0.5060	0.4002				Number	-
A1 (Z2)	C03041	-320	165.1	94.6	59	51	25.4		33120	18980	0.5054		2.00	3.02	0.20109020	M9	R
A1 (Z3)	C03042	-320	168.7	101.8	58	57	25.2		33840	20420		0.3543	2.00	3.18	0.20061359	M9	R
C2 (Z1)	C03043	-320	163.6	94.0	51	41	25.9		A CARLEND AND A CARLEND		0.5054	0.3305	2.00	3.16	0.20061359	M9	R
C2 (Z2)	C03044	-320	162.4	91.7			10000	D	32840	18880	0.5056	0.3891	2.00	3.03	0.20077240	M9	R
C2 (Z3)	C03045	-320			61	61	25.0	-	32580	18390	0.5054	0.3163	2.00	3.21	0.20061359	M9	R
02 (20)	00045	-020	165.5	93.9	61	61	25.7	-	33230	18850	0.5058	0.3163	2.00	3.21	0.20077240	M9	R

D - Failed outside middle half of gage length.

A/UAR: A=ACCEPTABLE, U=UNACCEPTABLE, R=REPORT

KNOWTHICLY OR WILLPULLY FALMITTHIS OR CONCEALING A MATERIAL FACT ON THIS FORM OR MANING FALSE, FICTITIOUS OR PRAUDULENT STATISMENTS OR REPRESENTATIONS NUMERI COLLD CONSTITUTE & FELCINY PURCH VIOLE UNCOM FELCING STATUTES. THE CERTINICATE OR REPORT SHALL NOT BE REPRODUCED EXCEPT IN PULL WITHOUT THE WANTTEN APPROVAL OF WATE, INC.

6-17-05 Technical Services Mariane Tensile Supervisor

June 17, 2005

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## METALTEK INTERNATIONAL

8600 Commercial Blvd. Pevely, MO 63070 June 14, 2005 Lab No. 05P-1741 P.O. No. 12516 Page 1 of 3

Attention: Chuck Ruud

## **REPORT OF CHARPY IMPACT TEST**

MATERIAL (SAMPLE ID): Alloy CF8 MNMn-Mod, A-1 COIL

SPECIFICATION: ASTM A 370-03a

SPECIMEN TYPE: "A" Vee Notch

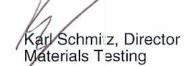
SPECIMEN SIZE: 10 mm x 10 mm

TEMPERATURE OF TEST: 293°K / 68° F

**RESULTS:** 

BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z1-7	152	0.125	100
Z1-8	152	0.086	100
Z1-9	182	0.089	100
Average	162	0.100	100
BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z2-7	152	0.131	100
Z2-8	164	0.084	100
Z2-9	170	0.105	100
Average	162	0.107	100
BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z3-7	196	0.117	100
Z3-8	164	0.104	100
Z3-9	142	0.088	100
Average	167	0.103	100

Identification of tested specimen provided by client.





Certificate No. 0397-01 Certificate No. 0397-02





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## METALTEK INTERNATIONAL

8600 Commercial Blvd. Pevely, MO 63070 June 14, 2005 Lab No. 05P-1741 P.O. No. 12516 Page 2 of 3

Attention: Chuck Ruud

## **REPORT OF CHARPY IMPACT TEST**

MATERIAL (SAMPLE ID): Alloy CF8 MNMn-Mod, A-1 COIL

SPECIFICATION: ASTM A 370-03a

SPECIMEN TYPE: "A" Vee Notch

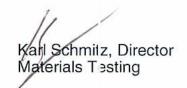
SPECIMEN SIZE: 10 mm x 10 mm

TEMPERATURE OF TEST: 77°K / -320°F

**RESULTS:** 

BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z1-7	82	0.040	6()
Z1-8	73	0.053	60
Z1-9	78	0.045	60
Average	78	0.046	6()
BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z2-7	94	0.061	70
Z2-8	90	0.053	70
Z2-9	76	0.057	70
Average	87	0.057	70
BASE METAL	FOOT LBS.	LATERAL EXPANSION	% SHEAR
Z3-7	59	0.028	30
Z3-8	83	0.059	40
Z3-9	72	0.043	40
Average	71	0.043	37

Identification of tested specimen provided by client.





Certificate No. 0397-01 Certificate No. 0397-02





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## METALTEK INTERNATIONAL

8600 Commercial Blvd. Pevely, MO 63070 June 14, 2005 Lab No. 05P-1741 P.O. No. 12516 Page 3 of 3

## Attention: CHUCK RUUD

## **REPORT OF MECHANICAL TESTS**

SAMPLE ID: 3 EA., A-1 COIL, Z1, Z2, Z3

Sample ID	Original Area Sq. Inches	Reduced Area Sq. Inches	Reduction in Area %	Modules of Elasticity	Yield Strength PSI	Tensile Strengt∣ı PSI	Elong (2.0" Gage in.	
Z1	0.1886	.0716	62.0	21.8 Msi	37600	85700	1.06	53.0
Z2	0.1886	0.0707	62.5	21.5 Msi	35500	79300	1.11	55.5
Z3	0.1940	0.0855	55.9	21.7 Msi	36800	82100	1.02	51.0

Round, reduced section room temperature tensiles

Yield taken at .2% offset

Tested in accordance with ASTM A 370

Identification of tested specimens provided by the client.

Schmitz, Director ar Materials Testing

KS/tlv



Certificate No. 0397-01 Certificate No. 0397-02



# A-1 COIL WELD MAP

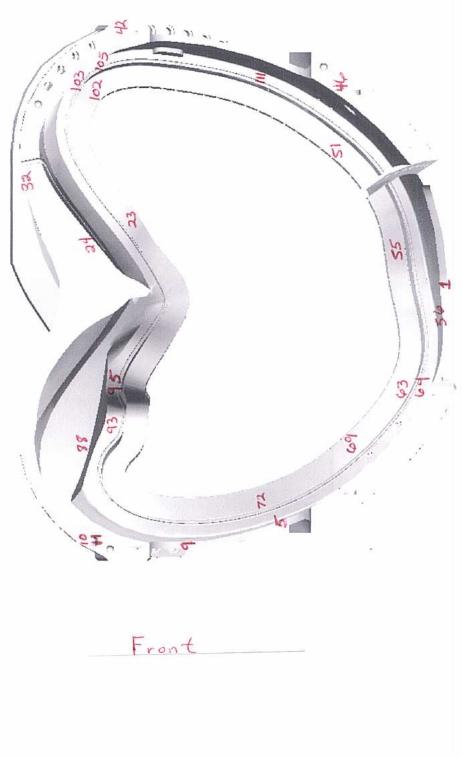
Defect Number	Drawing View	Length Inches	Width Inches	Depth Inches	Over 20% wall Over 1 inch Over 10 <sup>2</sup> inches Yes/No
1	Front	48	11/2	1/2	Yes
5	Front	7	51/4	1	Yes
9	Front	3 3/4	2	1 18	Yes
10	Front	51/2	41/2	13/4	Yes
()	Frunt	2112	2	1	YPS
23	Front	7	21/2	1/2	Yes
24	Front	11	21/2	11(2	Yes
32	Front	4	214	1	Kes
42	Front	5	21/2	2/14	. Yes
46	Front	2812	6	Through	Yes
51	Front	9	3	14	405
55	Front	10	1112	1	Yes
56	Front	6	2 14	2	4-s
63	Front	10	8112	3/4	Yes
64	Frint	7	3	14	Yes
69	Front	5 14	5	1/2	Tes
72	Front	9	612	1	Yes
88	Front	13	1/12	21/2	Yes
93	Front	il	142	(12	Yes
95	Front	8	4	t	Yes
102	Front	31/2	3 14	11/8	Yes
103	Front	13	3	1	Yes
105	Front	8	3	2	405
111		G	4		Yes
116	Front	21/2	Z	7/8	Yes
117	τυρ	1/4		3/4	Yes
118	Top	2	11/2	3/4	Yes
119	Top	21/2	21/2	1	Yes
123	Top	9314	412	2	Yes
128	Top	4114	4	1/4	Yes
(3)	Tup	5	3	1	Yes
135	Top	9112	2	414	Yes
140	Right	5112	5	1	Yes
144	Right	6	3	1/4	Yes
145	Right	33	312	1 3/4	405
146	Right	1634	144	1/4	yes
147	Right	9	6	1/4	Yes
152	Right	5	33/4	Through	Yes
154	Right	S	4	Through	4-5

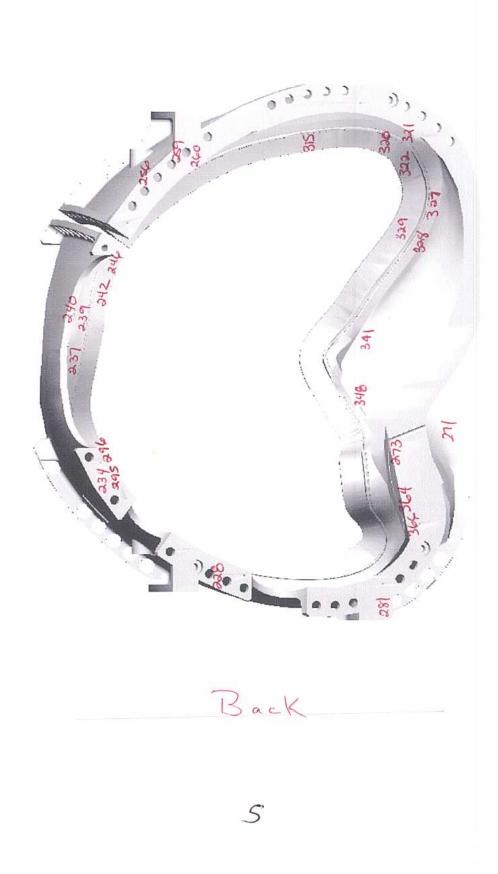
# A-1 COIL WELD MAP

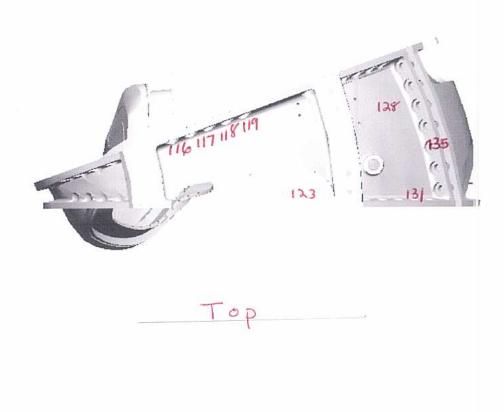
Defect Number	Drawing View	Length Inches	Width Inches	Depth Inches	Over 20% wall Over 1 inch Over 10 <sup>2</sup> inches Yes/No
155	Right	81/2	7	14	Yes
157	Right	63/4	4	4	Yes
158	Right	71/2	31/4	1/4	Yes
162	Right	7	2	1/2	Yes
166	Right	43/4	2	1	Yes
168	Right	9	4112	1/4	Yes
170	Right	53/4	2	3/4	Yes
171	Right	10	3	Through	405
172	Right	7112	3	1/2	1-5
173	Right	9	31/2	1/2	Yes_
176	Right	51/2	3	Through	Tes
177	Right	9112	1314	5/14	Yes
181	Risht	4	31/2	1/4	Yes
183	Right	10	2	1/2	Yes
191	Right	33/4	31/2	2	Yes
197	Right	45	31/2	314	(rs
198	Right	5	23/4	Through	Ves .
204	Right	16	21/2	5/16	Yes
205	Bottom	71/2	61/2	Through	Yes
206	Betton	31/2	13/4	N.	Tes
207	Batton	8	21/2	3/14	tes
212	Bottom	9	4	1/4	405
214	Bottom	83/4	5	3/4	Yes
216	Better	7	Z	1	Yes.
220	Left	6314	4	Through	tes
222	Left	41/2	2	1	Yes
228	BACK	13	\$	Through	Yes
234	BACK	13/4	13/4	114	Yes
237	BACK	5	2114	3/4	les
239	BACK	51/2	5	3/4	Tes
240	BACK	61/2	23/4	1	Yes
242	BACK	9	31/2	Through	Yes
246	BACK	5314	412	3/4	Yes
256	BACK	3	2 3/4	7/8	Yes
259	BACK	6	212	ì	Yes
260	BACK	6	2	3/4	les
271	BACK	4	21/2	)	Yes
273	BACK	61/2	412	Through	Yes
281	BACK	31/2	2	}	Tes

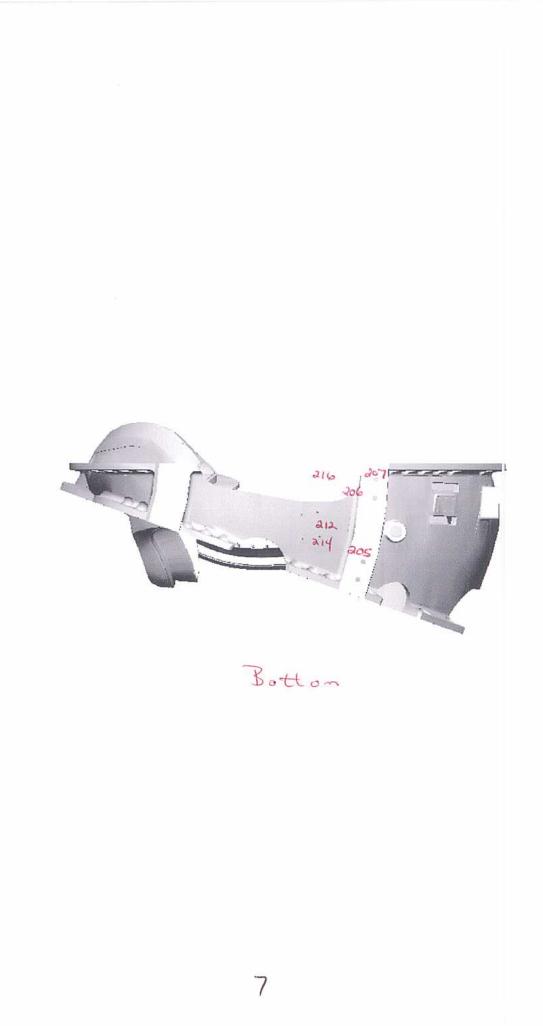
# A-1 COIL WELD MAP

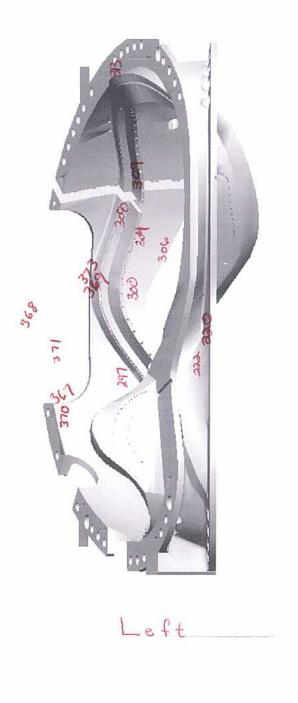
Defect Number	Drawing View	Length Inches	Width Inches	Depth Inches	Over 20% wall Over 1 inch Over 10 <sup>2</sup> inches Yes/No
295	BACK	111/2	41/2	3/4	Yes
244	BACK	4	4	3/4	Yes
297	Left	642	242	3/4	4.5
300	Left	11	a	1	Yes
304	Left	10	11/2.	1	Yes
366	Left	8	6	3/4	4-5
308	Left	8112	4 12.	3/4	4es_
309	Left	41/2	4	1/2	Pes
312	Lest	-7	2714	244	Yes
315	BACK	9	21/2	1(2	Yes
320	BACIC	1(	\$( 1/2	2	Yes
321	BACK	5	3	1/4	Yes_
322	BACK	8314	3	3/4	405
327	BACK	4	2	2	20
328	BACK	3	2		405
329	BACK	23/4	2	1	<u>les</u>
341	BACK	8	8	1/2	iles
348	BACK	(e	3	1/2	Yes
364	BACK	614	212	3/4	tes
3ib	BACIC	3314	3314	- 1	Yes
367	1-ft	3112	21/2	Through	Yes
368	Lefi	7112	3	Through	405
369	Left	5	43/4	14	Yes
155RI	Right	6	4/12	1	Yes
162 R1	Right	8	244	144	Ye
170 R	Right	43/4	3112	112	Ye!
145RI	Right	512	21/2	140	Y.e.
155R2	Right	7	5	11/2	Yes
170RZ	Right	7 1/8	244	1/4	4e- 4c.s
370	Right	33/14	23/8		Ye.r
37	Right Left	5	37/8	13/4	yes
37)	Left	6718	13/4	3/4	ley
				-	
				A.	

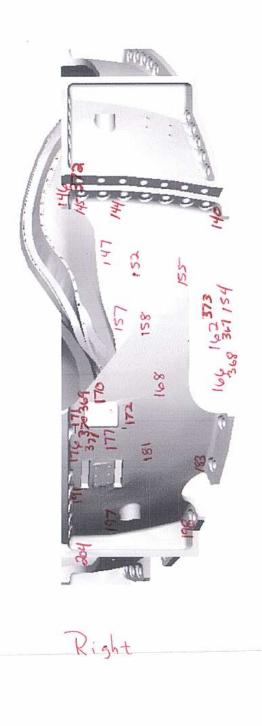












COOPERHEAT MQS

### 2 002

# TEAM COOPERHEAT-MQS, INC.

RADIOGRAPHIC TECHNIQUE SHEET

FORM 20.3-61 Rev. 4

CUSTOMER RSS NO::         MADE SECH NO.:         13043           CUSTOMER         METALTEK INTERNATIONAL / CARONODIET DIV.         DATE:         6/16/2005           PART NO.         MCWF-A         DESCRIPTION         A-COLL         MATERIAL         SS           TOTAL NUMBER OF VIEWS         117         NUMBER X-RAY VIEWS         117         NUMBER GAMMA RAY VIEWS         0           MACH(s)         MAKE(s)         VARIAN         MODEL(s)         L2000         S/N(s)         20         MAX KV(s)         7500           SOURCE(s)         N/A	5512 W. State St-Milwauke	, WI 53208 (414) 7	71-3060 Fax (414)7	71-9481 (80	0) 818-6403 www.	cooperheat-mqs.cor	n
CUSIONER         METALLER INTERNATIONAL / CARONODLET DIV.         DATE:         6/16/2005           PART NO.         MCWF-A         DESCRIPTION         A-COIL         MATERIAL         SS           TOTAL NUMBER OF VIEWS         117         NUMBER X-RAY VIEWS         117         NUMBER GAMMA RAY VIEWS         0           MACH(s)         MAKE(s)         VIARIAN         MODEL(s)         12000         S/N(s)         20         MAX KV(s)         7500           SOURCE(s)         N/A         PROCEDURE SPECIFICATION         ASTM E94-93         ACCEPTANCE CRITERIA         MSS-SP-54-1999           MQS PROCEDURE NO.         20.H.010 RFV. 0         PENETRAMETER SPEC.         ASTM E142-86           PROCESSING:         AUTOMATIC X         PROCESSING         B2000         MANUAL         TEMPERATURE         27.5°           TECHNICIAN JP,SS.ST         NDT LEVEL         II         ARPROVED BY C RUDOLPH         NDT LEVEL         III         APPENTING           SOURCE/X-RAY MACH USED         VARIAN         III         IIII         IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	CUSTOMER RSS NO .:		SH	EET:	REV:	MQS TECH. NO.	:13043
TAIL NU.       MC.WF-A       DESCRIPTION       A-COIL       MATERIAL       SS         TOTAL NUMBER OF VIEWS       117       NUMBER X-RAY VIEWS       117       NUMBER GAMMA RAY VIEWS       0         MACH(s)       MAKE(s)       VARIAN       MODEL(s)       12000       S/N(s)       20       MAX KV(s)       7500         SOURCE(s)       N/A	CUSTOMERMETAL	TEK INTERNATION	AL / CARONDOLET	DIV.	DATE	C /1 C /2	0.00F
101AL NUMBER OF VIEWS       117       NUMBER X-RAY VIEWS       117       NUMBER GAMMA RAY VIEWS       0         MACH(s)       MAKE(s)       VARIAN       MODEL(s)       L2000       S/N(s)       20       MAX KV(s)       7500         SOURCE(s)       N/A	PART NO.	MCWF-A	DESCRIPTI	ON	A-COIL	MATERIAI	2003
SOURCE/SUBJ       N/A       MODEL(S)       L2000       S/N(S)       20       MAX KV(S)       7500         PROCEDURE SPECIFICATION       ASTM E94-93       ACCEPTANCE CRITERIA       MSS-SP-54-1999         MQS PROCEDURE NO.       20.H.010 REV. 0       PENETRAMETER SPEC.       ASTM E142-86         PROCESSING: AUTOMATIC X       PROCESSOR       B2000       MANUAL       TEMPERATURE       27.5°         TECHNICIAN JP.SS.ST       NDT LEVEL       II       APPROVED BY C RUDOUPH       NDT LEVEL       1         VIEW IDENTIFICATION       SEE ATTACHED       NDT LEVEL       II       APPROVED BY C RUDOUPH       NDT LEVEL       1         SOURCE/X-RAY MACH USED       VARIAN       I       I       III       IIII       IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	TOTAL NUMBER OF VIEW	S 117 NUN	BER X-RAY VIE	WS 117			
DOUBLING         N/A           PROCEDURE SPECIFICATION         ASTM E94-93         ACCEPTANCE CRITERIA         MSS-SP-54-1999           MQS PROCEDURE NO.         20.H.010 REV. 0         PENETRAMETER SPEC.         ASTM E142-86           PROCESSING: AUTOMATIC X         PROCESSOR         B2000         MANUAL         TEMPERATURE         27.5°           TECHNICIAN JP.SS.ST         NDT LEVEL         II         ARPROVED BY C RUDOLPY         MOT LEVEL         1           VIEW IDENTIFICATION         SEE ATTACHED         I         I         I         I         I           SOURCE/X-RAY MACH USED         VARIAN         I	MACH(s) MAKE(s)	ARIAN MOD	EL(s) 120	))))) ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( ( (	NOMBER GAI		<u> </u>
PROCESSING:         ATTOMATIC         X         PROCESSOR         B2000         MANUAL         TEMPERATURE         27.5°           TECHNICIAN         JP,SS,ST         NDT LEVEL         I         ARPROVED BY C RUDOLPH         NDT LEVEL         I           VIEW IDENTIFICATION         SEE ATTACHED         Image: Construct of the construction of the construc	SOURCE(s) N	'A	Contraction of the last		20 <u>20</u>	MAX KV(S)	7500
PROCESSING:         AUTOMATIC         X         PROCESSOR         B2000         MANUAL         TEMPERATURE         27.5°           TECHNICIAN         JP_SS,ST         NDT LEVEL         I         'APROVED BY C RUDOLPH         NDT LEVEL         I           VIEW IDENTIFICATION         SEE ATTACHED         Image: Construct of the construct of	PROCEDURE SPECIFICAT	ON A	STM E94-93	٨٥			
TECHNICIAN JP,SS,ST       NDT LEVEL       I       ARPROVED BY C RUDOLPH       NDT LEVEL       I         VIEW IDENTIFICATION       SEE ATTACHED       I       ARPROVED BY C RUDOLPH       NDT LEVEL       I         SOURCE/X-RAY MACH USED       VARIAN       I       I       I       I       I         SOURCE/X-RAY MACH USED       VARIAN       I       I       I       I       I       I         CURIES OR KV       7500 KV       I	MQS PROCEDURE NO.	20.H.0	10 REV. 0		STRANCE CKI	ERIA MSS-	SP-54-1999
TECHNICIAN _P_3STS1NDT LEVEL _I       ARPROVED BY C_RUDOLPHNDT LEVEL _I         VIEW IDENTIFICATION       SEE ATTACHED         SOURCE/X-RAY MACH USED       VARIAN         CURIES OR KV       7500 KV         MA OR PULSES       N/A         SOURCE TO FILM DISTANCE       *         SOURCE TO FILM DISTANCE       *         SOURCE TO FILM DISTANCE       *         ATERIAL THICKNESS       *         WATERIAL THICKNESS       *         MATERIAL THICKNESS       *         MATERIAL GROUP       1         SIZE/(AMT)       GP.[1]         FILM SIZE       *         SIZE/(AMT)       GP.[1]         B SCREEN, FRONT       010         B SCREEN, FRONT       010         B SCREEN, FRONT       010         MASKING TYPE/LOCATION       N/A         MASKING TYPE/LOCATION       N/A         MALE       1         MASKING TYPE/LOCATION       N/A         MALE       1         MASKING TYPE/LOCATION       N/A         MCA       1         MALE       1         MALE       1         MALE       1         MALE       1	PROCESSING: AUTOMATI	C X PROCESS	OR B2000	MANU	AL TEMPE	PEC. ASTI	<u>M E142-86</u>
VIEW IDENTIFICATION         SEE ATTACHED           SOURCE/X-RAY MACH USED         VARIAN           CURIES OR KV         7500 KV           MA OR PULSES         N/A           SOURCE TO FILM DISTANCE         *           MATERIAL THICKNESS         *           MATERIAL GROUP         1           PENETRAMETRER         I           SIZE/(AMT)         GP. 1           SIZE         *           SIZE/(AMT)         GP. 1           B SCREEN, FRONT         .010           B SCREEN, FRONT         .010           B SCREEN, BACK         .010           ILL TE TYPE/LOCATION         N/A           MASKING TYPE/LOCATION         N/A           MASKING TYPE/LOCATION         N/A<	TECHNICIAN JP, SS, ST	N				ERATURE 27.	5
SOURCE/X-RAY MACH USED       VARIAN       I       I         CURIES OR KV       7500 KV       I       I         MA OR PULSES       N/A       P       I         SOURCE TO FILM DISTANCE       *       I       I         EXPOSURE TIME OR RADS       *       I       I         MATERIAL THICKNESS       *       I       I         MATERIAL GROUP       1       I       I         PENETRAMETRER       GP. 1       I       I         SIZE/(AMT)       GP. 1       I       I         FILM SIZE       *       I       I         ILM TYPE/BRAND       *       I       I         ''LLM TYPE/BRAND       I       I       I         ''LLM SIZE       *       I       I         ''LLM TYPE/BRAND       I       I       I         ''LLM TYPE/BRAND       I       I       I         ''LLM SIZE       *       I       I       I         ''LLM TYPE/BRAND       I       I       I       I         ''LLM TYPE/LOCATION       N/A       I       I       I         ''LLM SIZE       I       I       I       I       I	VIEW IDENTIFICATION	SEE ATTACHED		ANTROVE		N	
CURIES OR KV       7500 KV	and the second	Lawrence and the second se					
MA OR PULSES     N/A     Image: Constraint of the second s					1		
SOURCE TO FILM DISTANCE       *	MA OR PULSES		L <u> </u>	4			
MATERIAL THICKNESS       *	SOURCE TO FILM DISTANC			, in the second s		3.	ч. 
MATERIAL GROUP       1         PENETRAMETRER       GP. 1         SIZE/(AMT)       GP. 1         SHIM BLOCK SIZE       GP. 1         FILM SIZE       *         FILM SIZE       *         FILM SIZE       *         ILM TYPE/BRAND       *         *       1         *	XPOSURE TIME OR RADS	*		· · · · · · · · · · · · · · · · · · ·			
PENETRAMETRER       GP. 1       *	ATERIAL THICKNESS	*		<u>,</u>		*	
SIZE/(AMT)       GP. 1       *         SHIM BLOCK SIZE       GP. N/A		1			N N		
SHIM BLOCK SIZE       GP.       N/A         FILM SIZE       *		] *		4) 7_2			<i>y</i> 1
ILM TYPE/BRAND       *       Image: Stress of the s		N/A					
PB SCREEN, FRONT       .010         PB SCREEN, BACK       .010         SENSITIVITY       2-2T         PILTER TYPE/LOCATION       N/A         MASKING T	ILM SIZE	*				1	
PB SCREEN, BACK     .010       SENSITIVITY     2-2T       ILTER TYPE/LOCATION     N/A       MASKING TYPE/LOCATION     N/A       MASKING TYPE/LOCATION     N/A       IO. OF FILMS IN CASSETTE     *       IVEWING: SING./DOUB./BOTH     B       OCAL SPOT SIZE     2 MM       KETCH AND/OR REMARKS     *	ILM TYPE/BRAND	*	T				<u> </u>
SENSITIVITY     2-2T       ILTER TYPE/LOCATION     N/A       MASKING TYPE/LOCATION	B SCREEN, FRONT	.010					
ILTER TYPE/LOCATION     N/A       MASKING TYPE/LOCATION	B SCREEN, BACK	.010				1	
ASKING TYPE/LOCATION N/A NGLE N/A NGLE N/A NGLE N/A SUBJECT SING./DOUB./BOTH B SUBJECT SING./DOUB./BOTH B SUBJECT SIZE 2 MM SUBJECT SIZE 2 MM SUBJECT SIZE 2 MM SUBJECT SIZE X SUBJECT SI	ENSITIVITY	2-2T		·····			
NGLE N/A IO. OF FILMS IN CASSETTE * IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	LTER TYPE/LOCATION	N/A					
IO. OF FILMS IN CASSETTE * IEWING: SING./DOUB./BOTH B ICOCAL SPOT SIZE 2 MM IEWING: SING./DOUB./BOTH B ICOCAL SPOT SIZE 2 MM ICOCAL	ASKING TYPE/LOCATION	N/A					
IEWING: SING./DOUB./BOTH B OCAL SPOT SIZE 2 MM KETCH AND/OR REMARKS *	NGLE	N/A				1	
OCAL SPOT SIZE 2 MM KETCH AND/OR REMARKS *	D. OF FILMS IN CASSETTE	*		y .	1 1		[]
	EWING: SING./DOUB./BOTH	ВТ	1			<u> </u>	
	OCAL SPOT SIZE	2 MM				1.	
EOMETRIC UNSHARPNESS N/A	ETCH AND/OR REMARKS	*	1			1 ° · · · · · · · · · · · · · · · · · ·	
	OMETRIC UNSHARPNESS	N/A			+**ATTACLED DUPTTO		

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Form 20.4 - 61 Attachment A

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CUSTOMER	METALTEK INT./CARONDOLET	RSS #	13043	PART NO.	MCWF-A

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RAIL

VIEW_	SFD	EXP. TIME	FILM TYPE	FILM SIZE	THK, RANGE	IQI
1-2	58"	62 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
2-3	58"	62 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
3-4	60"	62 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
4-5	65"	80 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
5-6	54"	70 KR	AA-M100-T	14 X 17	2.75-5.5	50(2), 80, 100
6-7	50"	52 KR	AA-M100-T	44 X 17	2.75 - 5.5	50(2), 80, 100
7-8	54"	70 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
8-9	56"	70 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
9-10	60"	75 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
10-11	65"	80 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
11-12	70"	80 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
12-13	<b>7</b> 7"	90 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
13-14	77"	90 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
V15	<b>6</b> 0"	65 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
16-17	60"	60 KR	AA-M100-T	14 X 17	2.75 - 5.5	50(2), 80, 100
17-18	60"	60 KR	AA-M100-T	14 X 17	2.75 - 5.5	
18-19	60"	60 KR	AA-M100-T	14 X 17 -	2.75 - 5.5	<u>50(2), 80, 100</u> 50(2), 80, 100
19-20	60"	60 KR	AA-M100-T	14 X 17	2.75 - 5.5	
20-21	61"	56 KR	AA-M100	14 X 17	2.75-5.5	50(2), 80, 100
21-22	57"	62 KR	AA-M100	14 X 17	2.75 - 5.5	50(2), 80, 100
22-23	65"	60 KR	AA-M100	14 X 17	2.75 - 5.5	50(2), 80, 100
23-24	65"	72 KR	AA-M100	14 X 17	2.75 - 5.5	50(2), 80, 100
24-25	65"	60 KR	AA-M100	14 X 17		50(2), 80, 100
25-26	65"	75 KR	AA-M100-T	14 X 17	2.75 - 5.0 2.75 - 7.0	50(2), 80
26-27	65"	75 KR	AA-M100-T	<u>14 X 17</u> 14 X 17		50(2), 80, 100, 120
27-28	65"	60 KR	AA-M100	<u>14 X 17</u> 14 X 17	2.75 - 7.0	50(2), 80, 100, 140
28-29	65"	60 KR	AA-M100		2.75 - 5,5	50(2), 80, 100
29-1	65"	60 KR	AA-M100	<u>14 X 17</u> 14 X 17	2.75 - 5.5 .	50(2), 80
			AA-WII00		2.75 - 5.5	50(2), 80, 100
				<i>¥</i>		
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## CUSTOMER METALTEK INT./CARONDOLET RSS # 13043 PART NO. MCWF-A

VIEW	SFD	EXP. TIME	FILM TYPE	FILM SIZE	THK. RANGE	IQI
30-31	75"	35 KR	Т	14 X 17	2.75"	50 (2)
31-32	75"	<u>35 KR</u>	Т	14 X 17	2.75"	50 (2)
32-33	75"	35 KR	Т	14 X 17	2.75"	50 (2)
33-34	75"	35 KR	Т	14 X 17	2.75"	50 (2)
34-35	75"	35 KR	Т	14 X 17	2.75"	50 (2)
35-36	75"	35 KR	Т	14 X 17	2.75"	50 (2)
37-38	75"	35 KR	Т	14 X 17	2.75"	50 (2)
38-39	75"	35 KR	Т	14 X 17	2.75"	50 (2)
39-40	75"	35 KR	Т	14 X 17	2.75"	50 (2)
41-42	75"	90 KR	AA-M100-T	14 X 17	2.75 X 5.5"	50 (2), 100 (2)
43-44	75"	90 KR	AA-M100-T	14 X 17	2.75 X 5.5"	50 (2), 100 (2)
44-45	75"	75 KR	AA-M100	14 X 17	2.75 X 5.5"	50 (2), 100 (2)
45-46	, 75"	75 KR	AA-M100	14 X 17	2.75 X 5.5"	50,100(2)
46-47	75"	75 KR	AA-AA	14 X 17	5.5"	100 (2)
47-48	75"	75 KR	AA-AA	14 X 17	5.5"	100 (2)
48-49	75"	75 KR	AA-AA	* 14 X 17	5.5"	100 (2)
50-51	75"	35 KR	Т	14 X 17	2.75"	50 (2)
51-52	75"	35 KR	Т	14 X 17	2.75"	50 (2)
52-53	75"	35 KR	T	14 X 17	2.75"	50 (2)
54-55	75"	35 KR	T	14 X 17	2.75"	50 (2)
55-56	75"	35 KR	Т	14 X 17	2.75"	50 (2)
57-58	97"	45 KR	M125-T	14 X 17	1.5 – 1.75"	30, 35
58-58A-59	80"	110 KR	D8-R50-T-D8	14 X 17	1.5 - 8"	30, 100, 140, 160
59-60	80"	30 KR	M125-T	14 X 17	1.5"	30 (2)
60-61	80"	30 KR	M125-T	*14 X 17	1.5"	30 (2)
61-62	80"	30 KR	M125-T	14 X 17	1.5"	30 (2)
62-63	85"	90 KR	D8-M125-D8	14 X 17	3-8"	60, 120, 160
62A-63A	85"	90 KR	D8-M125-Dumb	+ 14 X 17	3-6"	60, 120
63-64	80"	45 KR	АА-М125-М100-Т	14 X 17	1.5-4"	30 (2), 50, 80
64-65	80"	45 KR	M125-M100	14 X 17	1.5"	30 (2)
65-65A-66	80"	95 KR	AA-M125-T	14 X 17	1.5 - 5.5"	30, 100 (2)
66-67	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
67-68	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
68-69	80"	40 KR	M125-M100	+ 14 X 17	1.5"	30 (2)
69-70	80"	40 KR	AA-M100-T	14 X 17	1.5 - 3"	30 (2), 50, 60
70-71	80"	40 KR	AA-M100-T	14 X 17	1.5-4"	30 (2), 60, 80
71-72	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
72-73	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
73-74	80"	60 KR	AA-AA	14 X 17	3-6"	60, 100, 120
74-75	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
75-76	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
76-77	80"	40 KR	M125-M100	14 X 17	1.5"	30 (2)
77-78	80"	150 KR	D8-AA-T-D8	14 X 17	3-8"	60, 80, 100, 120, 160
78-79	80"	40 KR	AA-M125-T	14 X 17	1.5 - 3"	30 (2), 40 60
79-80	85"	50 KR	T/M100	14 X 17	1.5 - 3"	30 (2), 40 80
80-81	80"	40 KR	T/M100	14 X 17	1.5 - 2.5"	30 (2), 40, 50, 60
				<u>ITAI</u>		30(2), 40, 50

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Form 20.4 - 61 Attachment A

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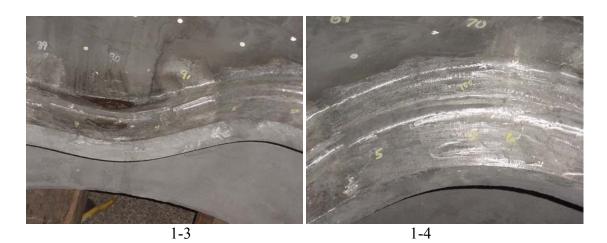
CUSTOMER METALTEK INT./CARONDOLET RSS # 13043 PART NO. MCWF-A

VIEW	SFD	EXP. TIME	FILM TYPE	FILM SIZE	THK. RANGE	IQI
81-82	80"	40 KR	T-M100	14 X 17	1.5 - 2.5"	30(2),40,50
82-83	80"	40 KR	T-M100	14 X 17	1.5 - 2.50"	30(2),40,50
84-85	75"	90 KR	D8-R50-M125-T	14 X 17	1.5 - 6"	30,50,60,80,100,120
85-86	75"	60 KR	T-R50-M125	14 X 17	1.5 - 4"	30,40,50,60,80
86-87	75"	60 KR	AA-M125-T	14 X 17	1.5 – 5"	30, 50, 60, 80, 100
87-88A	70"	60 KR	AA-M125-T	14 X 17	3"-5"	60,80,100
88-89	80"	40 KR	M125-M100	14 X 17	1.5"	30(2)
89-90	80"	40 KR	M125-M100	14 X 17	1.5"	30(2)
90-91	80"	40 KR	M125-M100	14 X 17	- 1.5"	30(2)
92-93	65"	30 KR	T-M125	14 X 17	1.5 - 3"	30(2),40,60
94-95	84"	40 KR	Т	14 X 17	2.75"	50(2)
95-96	84"	40 KR	Т	14 X 17	2.75"	50(2)
96-97	· 84"	40 KR	Т	14 X 17	2.75"	50(2)
97-98	84"	40 KR	Т	14 X 17	2.75"	50(2)
98-99	84"	40 KR	Т	14 X 17	2.75"	50(2)
99-100	84"	40 KR	Т	14 X 17	2.75"	50(2)
100-101	84"	40 KR	T	14 X 17	2.75"	50(2)
102-103	84"	40 KR	Т	14 X 17	2.75"	50(2)
103-104	· 84"	40 KR	Т	14 X 17	2,75"	50(2)
104-105	84"	40 KR	Т	14 X 17	2.75"	50(2)
106-107	84"	40 KR	Т	14 X 17	2.75"	50(2)
107-108	84"	40 KR	Т	14 X 17	2.75"	50(2)
108-109	84"	40 KR	T/M125	14 X 17	1.5 - 2.75"	30,50(2)
109-110	84"	40 KR	T/M125	14 X 17	1.5 - 2.75"	30,50(2)
111-112	84"	40 KR	Т	14 X 17	2.75"	50(2)
112-113	84"	40 KR	Т	14 X 17	2.75"	50(2)
113-114	84"	40 KR	Т	14 X 17	2.75"	50(2)
115-116	84"	40 KR	Т	14 X 17	2.75"	50(2)
116-117	84"	40 KR	Т	14 X 17	2.75"	50(2)
118-119	80"	55 KR	M125/M100	14 X 17 *	1.5"	30(2)
119-120	80"	55 KR	M125/M100	14 X 17	1.5 - 2"	30(2), 40
121-122	80"	40 KR	M125/M100	14 X 17	1.5 - 2"	30(2), 40
122-123	80"	40 KR	M125/M100	14 X 17	1.5-2"	30(2), 40
123-124	80"	40 KR	M125/M100	'14 X 17	1.5 - 2"	30(2), 40
124-125	80"	40 KR	M125/M100	14 X 17	1.5 - 2"	30(2), 40
125-126	80"	40 KR	M125/M100	14 X 17	1.5 - 2"	30(2), 40
126-127	. 80"	40 KR	M125/M100	14 X 17	1.5-2"	30(2), 40
127-128	80"	50 KR	D8/M100/M125	14 X 17	1.5 - 6"	30(2),120
128-129	80"	40 KR	M125/M100	14 X 17	1.5"	30(2)
130-131	80"	40 KR	M125/M100	14 X 17	1.5"	30(2)
131-132	80"	40 KR	M125/M100	14 X 17	1.5"	30(2)
V133	80"	50 KR	D8/M125/AA	7 X 17	1.5 - 6"	30(2),120,140
V134	80"	50 KR	D8/M125/AA	(7 X 17	1.5-6"	30(2),120,140

## Form 20.4 - 61 Attachment A

Page 4 of 4













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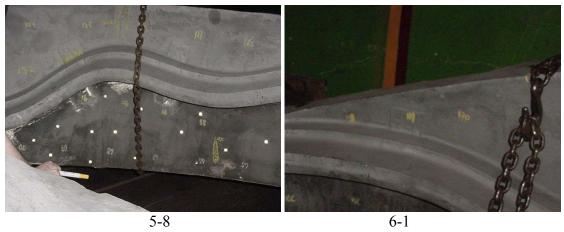


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COOPERHEAT MQS



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CUSTOMER												DAT	E			1	WORK	ORDE	R NO.
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. ACCEPTED MMENTS		{	Ø	NO.	REJEC	TED	_/				MQS	TECH.	NO.	12	970	5	SHT.	REV.	
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#### RADIOGRAPHIC INTERPRETATION REPORT

CUSTOMER		PURCH									CONTROL NO. PAGE
Energy Industri PART NO!	AC = for	IO P	PPI	-1	FP_	LT	5-2	2	8-21-	05	40851 lof
		SPE	CIFICA	TION		CLAS	SS			TOTA	L PIECES PIECES ACCEPTED
MCWFA-1 RADIOGRAPHED BY:		Ē	146/	EIE	E FED BY	S	ee s	Spec	-		
RADIOGRAPHED BY:	1.		INTI	ERPRET	TED BY KE OPE	: . /1 .				ASNT	
Midgett/Kel	MATERIA	AL.	1	ISOT	OPE	1104			CC	DE	
29/59/80	CF8M			mm	11114 101	10	OBALT			TM E94	ASME MIL-STD-453
21/24/20	V	P	A	R	S	1	P	L	S	L	COMMENTS
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	68-69	30	X	×			3				
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	113-114	1		X						X	
	124-125	30/40	1		2		2		1		
	125-126	1		x			4			×	
R-3	6.8-69			X						X	
	69-70	3060		×						×	
	125-126	30/40		X						X	
	113-114			×	2010/01/01					X	
RY	68-69	30		X			4			x	
-	69-70	3010	/			]	2		/		
V	125-126	-		X			4			X	
Ţ	113-114	50		x			4			X	
R5	68-69	30			2	١	2		/		Lead Crimps
1	113-114	50	/			Î	3		/		
V	125-126			X			3			×	
R6	125-126	1	/				2				Film Scrathee / Legeloring
											5



#### RADIOGRAPHIC STANDARD SHOOTING SKETCH

Customer IndusTries OF OHio Material	Pattern Number MCULEA-1
Material CFSMNMN MOD	Traceability Number
Film Manufactuer	Source Number 42.5 c; TR 192
IQI LEVEL 2-2T From CQP 401 X Other (Specify	r, E.G. 2-4T, 2-1T) <u>N/A</u>

Exposures (views)	35-36	68-69	69-70	104-105	113-114	124	125	12,8		
Thickness (IN.)	23/4	1/2	1%-3	2 <sup>3</sup> /4		11/2-2	11/2-2	11/2		
S/F Distance (IN.)	16	20″	20"	16"	16''		20 <sup>11</sup>	20"		
Penetrameter	50x2	30X2	30x 7 50/60		50XZ	30XZ 40	30X2 40	30X2		
Time (MIN.)	30m	12m	12m 32mil	30m	28 m	12m	IZm	12m		
Focal Spot (IN.)	, (							>		
Film Size (IN.)	<i>ו</i> 4(גוז							$\rightarrow$		
Screen Size (Pb) Front/Back	,01									
S.W.E./D.W.E.	SWE	à						$\rightarrow$		 
S.W.V/D.W.V.	SW1/									
Film Type	59/80	59/80	59 29 80	5%	59/	59/80	591	59/80		
Acceptance Standard		E446	E446 E186	E 186	E186	E446	E446	E445		
Severity Level	see	Ac	cep	Tanc	e S	Tan	la rd			

Shooting Sketch (Use Additional Pages as Needed)

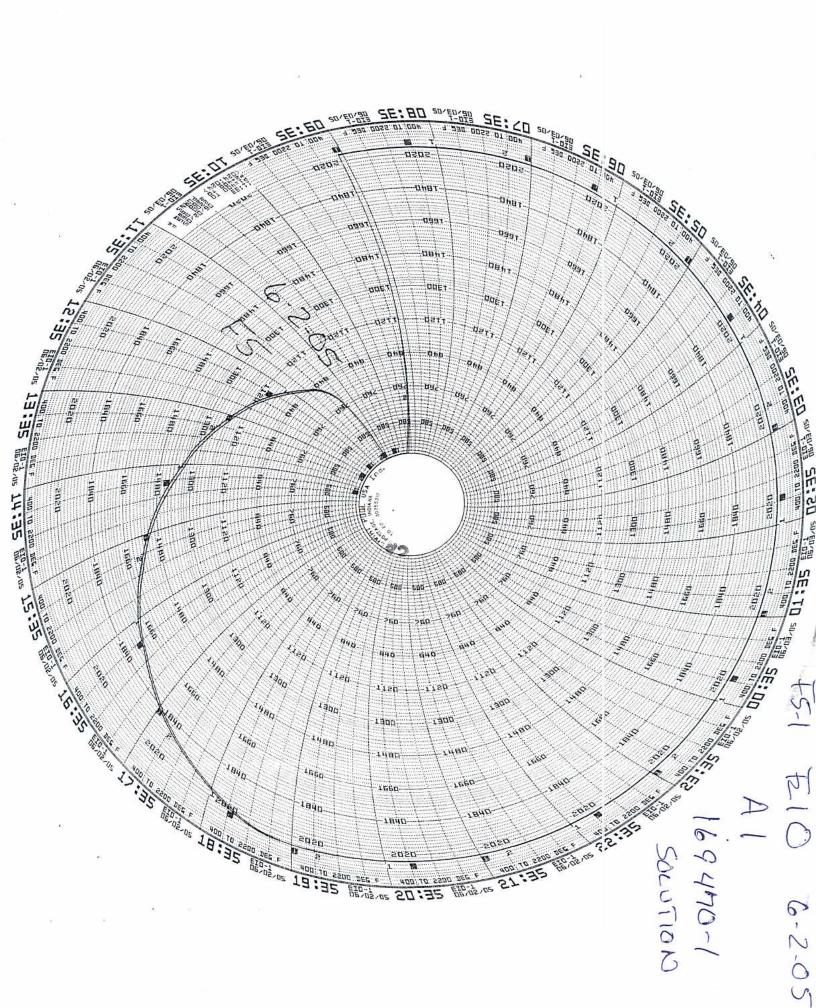
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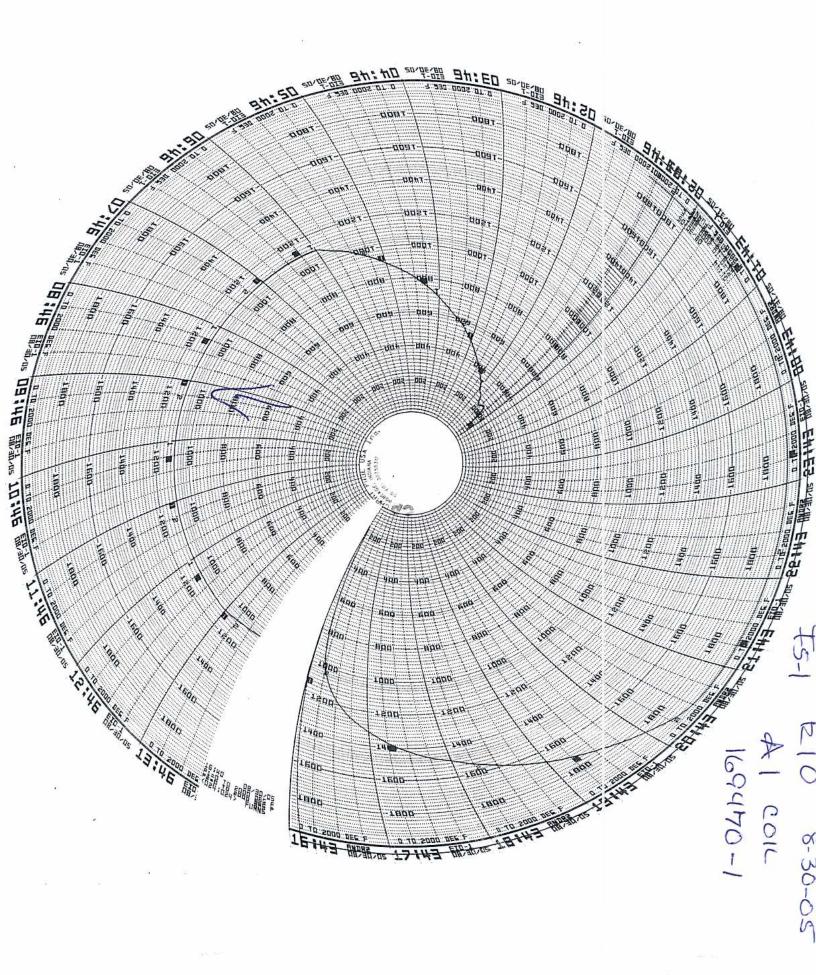
## see originall Drawing

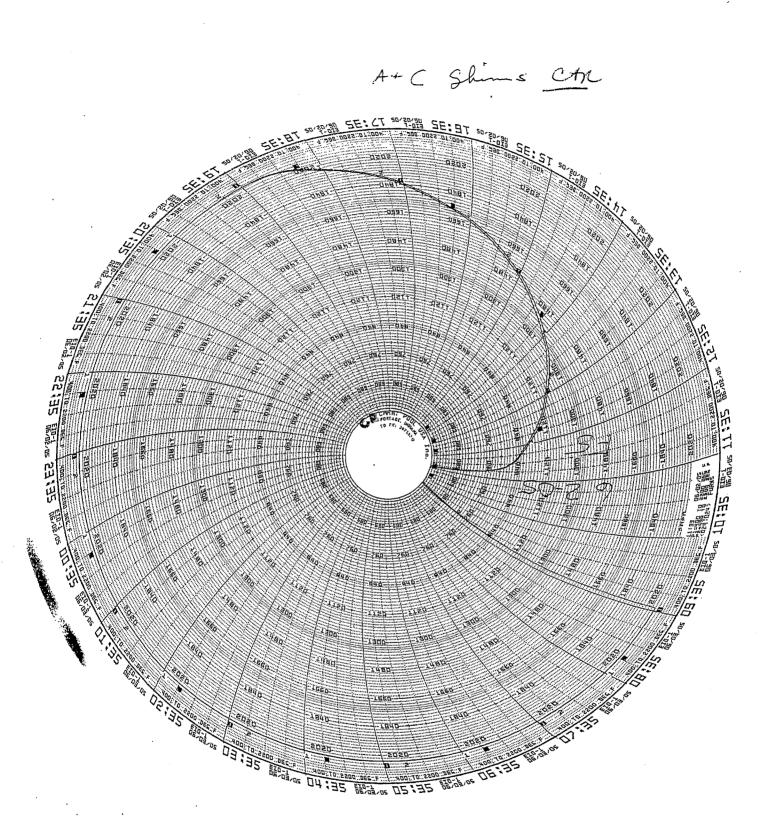
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Technique Approved By:		γ ·	Level:	<i>b</i>

Date: 30-05 Date:

S:DRIVE/MANUAL FORMS/RADIOGRAPHY RSS-01 REV. 4 2/9/02







File

A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1

DED //	CT LTION:	1 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 5 Dated Issued: 5-10-05		
OPER. #	STATION	DESCRIPTION OF PROCESS	Name	Date
10	QUALITY RELEASE	REVIEW AND APPROVE MTS. RECEIVED APPROVAL FROM EIO ON 5/10/05 FROM	Chr	5/12/05
15	PATTERN NPAT SOP 0100REV2	APPLY APPROPRIATE PART NUMBER, SERIAL NUMBER, AND FOUNDRY MARK, TO THE PATTERN. CAST ON BARS REQUIRED. Place numbers on the bars as to their location.	Biji	500
20	COREMAKE CORE SOP 0100 REV 6 CALIBRATION PER CORE SOP 0200R4/0300R6	MAKE CORES IN SAND MIXTURES AS DESCRIBED BY METALTEK ENGINEERING AND VERIFIED IN MODELING TRIALS. METALTEK CORE SOP 0100 REV 6) CORE WASH WITH ZIRCONIUM CORE WASH. (CALIBRATION OF EQUIPMENT REQUIRED PER CORE SOP 0200,R4 / 0300,R6) VERIFY COUNT AND INSPECT.	Anc	Sty
30	MOLD MOLD SOP 0400 REV 8 CALIBRATION PER MOLD SOP 0900 REV 5 PREPARATION PER MOLD SOP 1100R2/1200R2/13 00R1 SAND TESTING PER MOLD SOP 1400R2/1500R3/16 00R2	MOLD PER WORK INSTRUCTIONS IN MAPICS ROUTING AND SOPS REFERENCED. ENGINEER OF RECORD – ROGER BROMAN, CONSULT ON MOLD-RELATED CONCERNS. MOLD MATERIALS REQUIRED PER MAPICS BOM. NOTIFY ENGINEER OF ANY SUBSTITUTIONS.	delle la	Signe our
40	POUR MELT SOP 0100R5 MELT SOP 0700R2 MELT SOP 0600R2	METAL MUST BE AOD REFINED OR AOD INGOT. VIRGIN METAL ADDITIONS ALLOWED. RECORD POURING TEMPERATURE: 750 CASTING POURED AT: DATE: 52505 HEAT #"s: 295(4), 295(7) 295(8, 295(9) 29520 Montre ELAPSED POUR TIME 1:25 KEEL BLOCKS POURED: 24 Cost on bos Sample from ladle to be analyzed for final chemical analysis and reported on material certifications. Sample Taken by: 58 Analyzed: 6, Hort Date: 5-25-05	J. Golaste	S25S

					25
1, 2		A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1 2 OF 11 CO# 40851 Dated 3-9-05 Revision:/ Rev 6 Dated Issued: 5-29-05		i	Rep
50	MELT SOP 0800R2	SHAKEOUT	CA	5-28	
50	ARC RISE SOP 0100R1	REMOVE RISERS AS DIRECTED BY SUPERVISOR.	REC	5-31	
70	HEAT TREAT HEAT SOP 0103R5	SOLUTION ANNEAL. MAKE SURE TO BLOCK ALL FLANGES OF FORM AND RACETRACK TO MINIMIZE CREEP DISTORTION. Soak Temp: 2050F, Soak Time: 4HR + 1/2 HR/IN, Quench Type: Air Cool	RLS	6-6-0	
75	PHYSICAL TESTING	OBTAIN TEST SPECIMENS AND SUBMIT FOR PHYSICAL TESTING. REPORT RESULTS AS PART OF STEP 510.	WLH	6/6/05	Ļ
NOTE		THE ORDER OF CLEANING PROCESSES MAY BE ALTERED DUE TO CAPACITY CONSTRAINTS. HOLD POINTS AND COMPLIANCE WILL NOT BE COMPROMISED. EIO WILL BE ADVISED OF ALL CHANGES THAT MAY RESULT IN A REQUEST FOR DEVIATION FROM REQUIREMENTS.			
30	GRIND GSWA SOP 0100R3	SWING GRIND TO REMOVE RISER REMAINS AND FLASH IF REQUIRED.	AB	6-6-	05
35	GRIND GCHI SOP 0100R2	CHIP AND HAD GRIND SURFACE OF PART AS REQUIRED FOR CONTOUR.	CS	6-10.	05
90	SAND BLAST BLAS SOP 0100R6	SANDBLAST (REMOVE ALL BLAST MATERIAL FROM CASTING) SANDBLASTING WILL BE DONE USING RECYCLED SHARP ANGULAR AGGREGATE.	MTW	6/6	
NOTICE	WITNESS NOTIFICATION HOLD FOR EIO APPROVAL	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF LAYOUT. EIO NOTIFIED ON $\frac{c/3/ospin}{c/3/ospin}$ DCMA NOTIFIED ON $\frac{c/3/ospin}{c/3/ospin}$ APPROVAL RECEIVED ON $\frac{c/7/ospin}{c/7/ospin}$	MT W Q ENG OR QA MGR	6-10. RS	05
100	LAYOUT SOP LAYOUT 0100	INSPECT CASTING TO VERIFY DIMENSIONS. THIS STEP MAY BE DELAYED. DIMENSIONED DATE RELEASED RELEASED (ENGINEER ONLY) NOTE: THE FIRST PART PRODUCED OF EACH TYPE A, B AND C WILL BE DIMENSIONED BY LAWTON PATTERN. IF DIMENSIONED BY LAWTON IT WILL BE DOCUMENTED HERE. Subsequent casting done internally per Romer Arm.	Laufor Pattern	6/1	67

### A-1 Coil

### Energy Industries of Ohio

	Manufacturing and	Test Sequence (MTS)	Serial Number A 1
143	in an and the second	rest sequence (m15)	Serial Number A-1

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		<u>3 OF 11</u> CO# 40851 Dated 3-9-05 Revision: Rev 6 Dated Issued: 5-29-05		
110	VISUAL INSPECTION CQP-500 REV 4	VISUALLY INSPECT 100% of COMPONENT ACCORDING TO ASTM A802 LEVEL 3 ALL CONDITIONS. IF OK CHECK HERE IF REJECTED CHECK HERE MARK AND REPAIR AT STEP 120.	VT - LEVEL II	Synd to P
NOTICE	NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF LP STEP. EIO NOTIFIED ON DCMA NOTIFIED ON (7/2) / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2	Q ENG OR QA MGR	Plan
115	100% L.P. CQP 0300 REV 10	L.P. 100% OF COMPONENT. ACCEPTANCE PER ASTM A903. ACCEPTANCE CRITERIA- LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING. IF OK CHECK HERE	LP - LEVEL II	retur
120	WELD SOP 0100 REV 7	EXCAVATE ANY DEFECTS FOUND DURING 100% VISUAL AND LP INSPECTION.		
125	GRIND GCHI SOP 0100R2	CHIP AND HAND GRIND EXCAVATION AS REQUIRED.		
130	L.P. EXCAVATION CQP-300 REV 10	L.P. ALL EXCAVATIONS PRIOR TO WELDING TO ENSURE REMOVAL OF DEFECT. ACCEPTANCE PER A903. ACCEPTANCE CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING. IF OK CHECK HERE IF REJECTED SEND BACK TO STEP 125.	LP - LEVEL II	
165	SAND BLAST BLAS SOP 0100R6	SANDBLAST (REMOVE ALL BLAST MATERIAL FROM CASTING) SANDBLASTING WILL BE DONE USING RECYCLED SHARP ANGULAR AGGREGATE.		
170	HOLD POINT WELD MAP	MAP ALL WELDS WITH DIGITAL PHOTO/MAPS INDICATING LOCATION. SERIALIZE         DEFECTS ON CASTING, USE SCALE IN PHOTOS AND DOCUMENT SIZE. THIS IS TO BE         PERFORMED BY SUPERVISOR, INSPECTION LEAD MAN OR THEIR DESIGNEE, FILE WITH         QA. USE YELLOW MARKER.         MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO         CUSTOMER.         DEFECTS>10% YES, REPORT SENT BY DATE         DEFECTS < 10 % SIGN BY QA ENG.		
NOTICE	WITNESS NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF X-RAY AND DIMENSIONAL STEPS. EIO NOTIFIED ON $-\frac{1}{2}$ DCMA NOTIFIED ON $-\frac{1}{2}$	Q ENG OR QA MGR	RS

#### A-1 Coil

### Energy Industries of Ohio

100	V DAVATA (OR	Manufacturing and Test Sequence (MTS) Serial Number A-1           4 OF 11         CO# 40851         Dated 3-9-05         Revision: Rev 6         Dated Issued: 5-29-05	
190	X-RAY AT MQS MQS PROCEDURE 20.H.010 REV 0	X-RAY PER TECHNIQUE # 12726 USE CALIBRATED DENSITOMETER FOR DENSITY VERIFICATION. WHEN MARKING USE BLACK MARKERS. ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET.	RT- LEVEL II RS 424/05
210	X-RAY CQP 401 REV 5	X-RAY INTERPRETATION. ACCEPTANCE MSS SP 54. ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET. IF OK CHECK HERE AND SEND TO STEP 340. REJECTED CHECK HERE MARK UP DEFECTS AND SEND THE CASTING TO STEP 220.	RT –
220	WELD SOP 0100 REV 7	EXCAVATE ANY DEFECTS FOUND DURING RADIOGRAPHY.	
225	GRIND GCHI SOP 0100R2	CHIP AND HAND GRIND EXCAVATION AS REQUIRED.	
230	L.P. EXCAVATION CQP-300 REV 10	L.P. ALL EXCAVATIONS PRIOR TO WELDING TO ENSURE REMOVAL OF DEFECT. ACCEPTANCE PER A903. ACCEPTANCE CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING. IF OK CHECK HERE IF REJECTED SEND BACK TO STEP 225.	LP - LEVEL II
240	HOLD POINT WELD MAP	MAP ALL WELDS WITH DIGITAL PHOTO/MAPS INDICATING LOCATION . SERIALIZE DEFECTS ON CASTING, USE SCALE IN PHOTOS AND DOCUMENT SIZE. THIS IS TO BE PERFORMED BY SUPERVISOR, INSPECTION LEAD MAN OR THEIR DESIGNEE, FILE WITH QA. MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO CUSTOMER. DEFECTS>10% YES, REPORT SENT BY DATE DEFECTS < 10 % SIGN BY QA ENG. MAJOR WELD REPAIRS MAY NOT PROCEED UNTIL INFORMATION IS SUBMITTED. MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO CUSTOMER PRIOR TO REPAIR. ONCE THE REPORT IS SENT WELDING MAY START	
NOTICE	WITNESS NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF WELD STEP. EIO NOTIFIED ON DCMA NOTIFIED ON	Q ENG OR QA MGR
260	QA APPROVAL HOLD POINT	QA TO APPROVE ELECTRODE PRIOR TO USE.     PROCEDURE USED:	
270	WELD SOP 0100 REV 7	WELD REPAIR DEFECTS AS MARKED. FOR WELDS <2" - WPS 10-SMAW-CF8MNMN MOD REV 1 FOR WELDS <8" - WPS 15-GMAW-CF8MNMN MOD REV 2	

25

A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serie

90	X-RAY AT MQS	4 OF 11         CO# 40851         Dated 3-9-05         Revision: Rev 7         Dated Issued: 6-14-05           X-RAY PER TECHNIQUE # 12726 USE CALIBRATED DENSITOMETER FOR DENSITY	RT –	r
	MQS .	VERIFICATION. WHEN MARKING USE BLACK MARKERS.	LEVEL IV	all and the
	PROCEDURE	ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE	LEVELI	1. 1
	20.H.010	RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET.	185/1	471
N er	REV 0		re/ P	105
10	X-RAY .	X-RAY INTERPRETATION. ACCEPTANCE MSS SP 54.	RT -	1
	CQP 401 "	ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE	LEVEL II	1 A
1	REV 5	RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET.		1/11
		IF OK CHECK HERE AND SEND TO STEP 340.	OV	e
		REJECTED CHECK HERE MARK UP DEFECTS AND SEND THE CASTING TO STEP	KC	1.
170		220.	1~	
20	WELD SOP 0100	EXCAVATE ANY DEFECTS FOUND DURING RADIOGRAPHY.	BM	1:123
	REV 7		BM	2-20
25	GRIND	CHIP AND HAND GRIND EXCAVATION AS REQUIRED.	C M	0 4.3
	GCHI SOP	· · ·	VIX	6.25
Sec. Sec.	0100R2		- H	8:22
30	L.P.	L.P. ALL EXCAVATIONS PRIOR TO WELDING TO ENSURE REMOVAL OF DEFECT.	LP-CC	1.2
	EXCAVATION	ACCEPTANCE PER A903. ACCEPTANCE CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS	LEVEL II	6-26
1.	CQP-300	LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING.		
Sec. 25.	REV 10 .	IF OK CHECK HERE IF REJECTED SEND BACK TO STEP 225.	CC	6-27
40	HOLD POINT	MAP ALL WELDS WITH DIGITAL PHOTO/MAPS INDICATING LOCATION . SERIALIZE	and the second second	
	WELD MAP	DEFECTS ON CASTING, USE SCALE IN PHOTOS AND DOCUMENT SIZE. THIS IS TO BE	1. 1. 1. 1. 1.	10.200
		PERFORMED BY SUPERVISOR, INSPECTION LEAD MAN OR THEIR DESIGNEE, FILE WITH		Prove Set
	a de la companya de l	QA.	State Section	1 4, 53
		MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO	1	51
1. 1. 1.		CUSTOMER.	al	1111
1.1.1		DEFECTS>10% YES, REPORT SENT BY DATE DATE	CAR	118
		DEFECTS < 10 % SIGN BY QA ENG.		
100		MAJOR WELD REPAIRS MAY NOT PROCEED UNTIL INFORMATION IS SUBMITTED.	Territory of	
1.1		MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO	5 A. T.	1 - 2 - 3 - 3
OTICE	WITNESS	CUSTOMER PRIOR TO REPAIR. ONCE THE REPORT IS SENT, WELDING MAY START.		· All
onep.	NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF WELD STEP. EIO NOTIFIED ON 7/10 DCMA NOTIFIED ON 7/10	Q ENG	.1.
1. 1. 2.			OR QA	Ch
	Read to a second		MGR	U.
60	QA APPROVAL	QA TO APPROVE ELECTRODE PRIOR TO USE. D. 1 PROCEDURE USED: 45-6-MAY-CE8M. M. MATERIAL/LOT USED: 316MNNS/78309		A. 4
12.54	HOLD POINT	PROCEDURE USED: 15-6MW CE8MM MATERIAL/LOT USED: 316MNNE/78309		
		QUALITY ENG. Name: Kil M Date: 7/12/05	a states	- 1.
70 👷	WELD SOP 0100	WELD REPAIR DEFECTS AS MARKED.	1	0/
Charles .	REV 7	FOR WELDS <2" - WPS 10-SMAW-CF8MNMN MOD REV 1	TLS	8/12
		FOR WELDS <8" - WPS 15-GMAW-CF8MNMN MOD REV 2		111-

# A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1

		5 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Issued: 6-14-05		i.
		ADD WPS FOR VERTICAL WELDS.	-	
280	GRIND GCHI SOP 0100R2	HAND GRIND WELDS.	MoG	8/12
290	L.P. WELD	L.P. WELD REPAIRS ACCEPTANCE PER ASTM A903. ACCEPTANCE CRITERIA-LEVEL 1	LP -	
a.	CQF 0300 REV 10	FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING. IF OK CHECK HERE WASH AND SEND TO STEP 300. IF REJECTED CHECK HERE	LEVEL II CC	8/12
	REPEAT	REPEAT STEPS220 TO 290AS REQUIRED TILL CLEAR THROUGH VISUAL INSPECTION& PENETRANT INSPECTION. DOCUMENT REWORK ON STEPS S220 TO S290 ON LAST PAGEOF MTS.IF OK CHECK HEREAND PROCEED TO STEP 295.	N/A	
295	TEST MAG PERM SOP MAG PERM 100, REV 1	TEST MAG PERMEABILITY REPAIR AREAS RECORD ON WELD MAP LIST. TEST AT LEAST 5 POINTS PER WELD. ACCEPTANCE 1.02. IF OK CHECK HEREAND GO TO STEP 300. IF REJECTED CHECK HERE	CJA	8/12
296	GRIND GCHI SOP 0100R2	GRIND AREAS OF NON COMPLIANCE AND RETURN TO STEP 295. REPEAT UNTIL COMPLIANCE IS ACHIEVED.	NIA	
300	X-RAY ( NOTE)	IF RADIO GRAPHED AREAS ARE GREATER THAN FOUR TO FIVE INCHES THE CASTING WILL BE SENT TO MQS. SEND TO MQS CHECK HERE RADIOGRAPH AT CAF CHECK HERE	QA ENGINE ER	8-21-05
310 A	MQS X-RAY DEFECTS REPAIRED BY WELDING	X-RAY PER TECHNIQUE # 12726 USE CALIBRATED DENSITOMETER FOR DENSITY VERIFICATION. ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET.	LEVEL II	
310 B	CAF X-RAY DEFECTS REPAIRED BY WELDING CQP 401	X-RAY PER TECHNIQUE # 12726 USE CALIBRATED DENSITOMETER FOR DENSITY VERIFICATION. ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET.	RT - LEVEL II RBIC	8-21-05
N.	REV 5		Â.	-

		A-1 Coil			
		Energy Industries of Ohio			
		Manufacturing and Test Sequence (MTS) Serial Number A-1 6 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Issued: 6-14-05			
320	X-RAY CQP 401 REV 5	X-RAY INTERPRETATION. ACCEPTANCE MSS SP 54. ATTACH TECHNIQUE, READER SHEET FOR ALL RADIOGRAPHS. MUST INDICATE RADIOGRAPHER AND ASNT CERTIFICATION LEVEL ON READER SHEET. IF OK CHECK HERE AND SEND TO STEP 340. REJECTED CHECK HERE MARK UP DEFECTS AND SEND THE CASTING TO STEP 220.	RT - LEVEL II RBK	8-21-05	-
	REPEAT	REPEAT STEPS220 TO 320AS REQUIRED TILL WELDS CLEAR X-RAY. DOCUMENT REWORK ON A SUPPLEMENTAL MTS	QA ENG.		10 5 220
340	SAND BLAST BLAS SOP 0100R6	SANDBLAST (REMOVE ALL BLAST MATERIAL FROM CASTING) SANDBLASTING WILL BE DONE USING RECYCLED SHARP ANGULAR AGGREGATE.	MW	8/31/	85
NOTICE	WITNESS NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF VISUAL AND LP STEPS. EIO NOTIFIED ON $\frac{g}{2}$ DCMA NOTIFIED ON $\frac{g}{2}$	Q ENG OR QA MGR	R	
350	FINAL VISUAL INSPECTION CQP-500 REV 4	VISUALLY INSPECT 100% of COMPONENT ACCORDING TO ASTM A802 LEVEL 2 ALL CONDITIONS. IF OK CHECK HERE IF REJECTED CHECK HERE MARK AND REPAIR AT STEP 385. MUST BE PERFORMED BY LEVEL II in VT.	VT- LEVEL II KRA	3 05	
360	FINAL L.P. CQP 0300 REV 10	FINAL L.P. 100% OF COMPONENT. ACCEPTANCE PER ASTM A903. ACCEPTANCE         CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP         DRAWING.         IF OK CHECK HERE         WASH AND SEND TO STEP 455.         IF REJECTED CHECK HERE         CC.	LP- LEVEL II T.C. SY-31-0		
380	WELD SOP 0100 REV 7	EXCAVATE ANY DEFECTS FOUND DURING FINAL PENETRANT INSPECTION.	.1	e76-8-	31-05
385	GRIND GCHI SOP 0100R2	CHIP AND HAD GRIND EXCAVATION AS REQUIRED.	DWP 8-3105		
390	L.P. EXCAVATION CQP-300 REV 10	L.P. ALL EXCAVATIONS PRIOR TO WELDING TO ENSURE REMOVAL OF DEFECT. ACCEPTANCE PER A903. IF OK CHECK HERE IF REJECTED SEND BACK TO STEP 385.	LP- LEVEL II KLA 8-		

#### A-1 Coil

#### Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1

		Manufacturing and Test Sequence (MTS) Serial Number A-1 7 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Issued: 6-14-05		
400	HOLD POINT WELD MAP	MAP ALL WELDS WITH DIGITAL PHOTO/MAPS INDICATING LOCATION. SERIALIZE DEFECTS ON CASTING, USE SCALE IN PHOTOS AND DOCUMENT SIZE. THIS IS TO BE PERFORMED BY SUPERVISOR, INSPECTION LEAD MAN OR THEIR DESIGNEE. FILE WITH QA. MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO CUSTOMER. DEFECTS.>10% YES, REPORT SENT BY DATE DEFECTS < 10 %SIGN BY QA ENG. MAJOR WELD REPAIRS MAY NOT PROCEED UNTIL INFORMATION IS SUBMITTED. MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO CUSTOMER PRIOR TO REPAIR. ONCE THE REPORT IS SENT, WELDING MAY START.	NA	•
420	QA APPROVAL HOLD POINT	QA TO APPROVE ELECTRODE PRIOR TO USE.         PROCEDURE USED:	-	
430	WELD SOP 0100 REV 7	WELD REPAIR DEFECTS AS MARKED. FOR WELDS <2" - WPS 10-SMAW-CF8MNMN MOD REV 1 FOR WELDS <8" - WPS 15-GMAW-CF8MNMN MOD REV 2 ADD WPS FOR VERTICAL WELDS.		
440	GRIND GCHI SOP 0100 REV 2	HAND GRIND WELDS.		
450	L.P. WELDS CQP 0300 REV 10	L.P. WELD REPAIRS ACCEPTANCE PER ASTM A903. IF OK CHECK HERE WASH AND SEND TO STEP 460. IF REJECTED CHECK HERE AND RETURN TO STEP 440.	LP - LEVEL II	
	REPEAT	REPEAT STEPS350 TO 450AS REQUIRED TILL WELDS CLEAR FINAL LIQUID PENETRANT INSPECTION. DOCUMENT REWORK ON A SUPPLEMENTAL MTS	QA ENG.	
NOTICE	WITNESS NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF VISUAL AND LP STEPS. EIO NOTIFIED ON 20 20 DCMA NOTIFIED ON 92	Q ENG OR QA MGR	A
460	FINAL VISUAL INSPECTION CQP-500 REV 4	VISUALLY INSPECT 100% of COMPONENT ACCORDING TO ASTM A802 LEVEL 2 ALL CONDITIONS. IF OK CHECK HERE IF REJECTED CHECK HERE MARK AND REPAIR AT STEP 390. MUST BE PERFORMED BY LEVEL II in VT. GRIND ONLY	VT- LEVEL II KRA 831	-05

See.

#### A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1

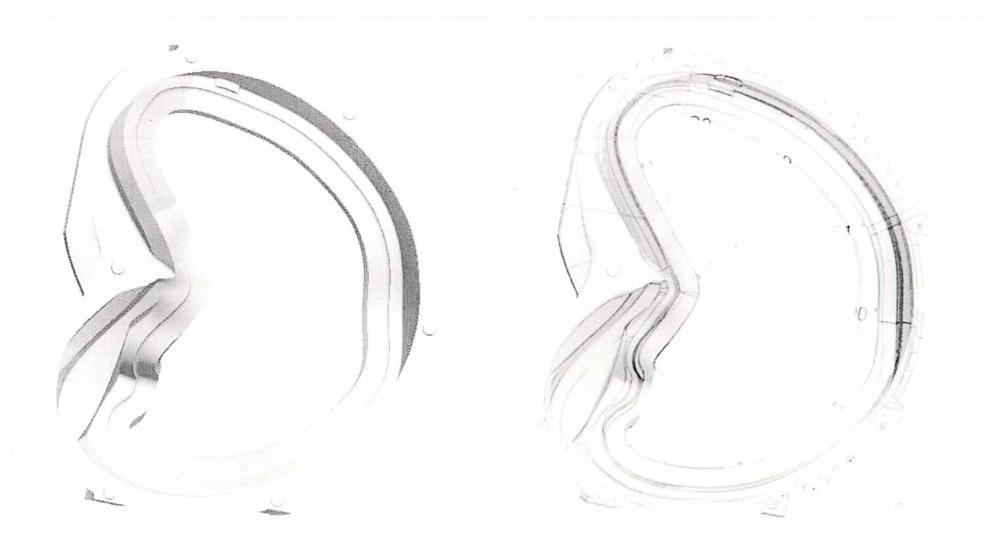
		8 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Issued: 6-14-05		
470	FINAL L.P.	FINAL L.P. 100% OF COMPONENT. ACCEPTANCE PER ASTM A903. ACCEPTANCE	LP -	
	CQP 0300	CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP	LEVEL II	. 1
	REV 10	DRAWING. IF OK CHECK HEREWASH AND SEND TO STEP 455.	VIA	831
		IF OK CHECK HERE WASH AND SEND TO STEP 455.	FUN	-1-(
480	TEST MAG	TEST MAG PERMEABILITY REPAIR AREAS. RECORD ON WELD MAP LIST. TEST AT LEAST		
1400	PERM	5 POINTS PER WELD.	1	
	SOP MAG PERM	ACCEPTANCE 1.02.	UN	
	100, REV 1	IF OK CHECK HEREAND GO TO STEP 430. IF REJECTED CHECK HERE	Pr	
490	GRIND GCHI	GRIND AREAS OF NON COMPLIANCE AND RETURN TO STEP 451.		
	SOP 0100R2	REPEAT UNTIL COMPLIANCE IS ACHIEVED.	/	
			$\checkmark$	
NOTICE	WITNESS	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF MAG PERM	Q ENG	
1.1	NOTIFICATION	STEPS.	OR QA	
		EIO NOTIFIED ON $\mathcal{V}$ dcma notified on $\mathcal{V}$	MGR	
500	FINAL MAG	PERFORM MAG PERM TESTING WITH SEVRIN GAUGE. ACCEPTANCE 1.02. CHECK THE		61
	PERM	ENTIRE SURFACE ON A 6"BY6" GRID. REPORT RESULTS. USE A 6" SQUARE BLOCK TO	1	$\mathcal{O}$
	INSPECTION	INDICATE TEST LOCATIONS AND RECORD RESULTS. COMPLIANT AREAS WILL NOT BE	nfn	031
	SOP MAG PERM	MARKED. MARK NONCOMPLIANT AREAS WITH AN "X" FOR REPAIR.	Nic	
	100, REV 1	OK CHECK HERE 📝 AND GO TO STEP 530.		
	CODINIO	IF REJECTED CHECK HERE		
510	GRIND	HAND GRIND WITH SUITABLE CONE OR OTHER SIMILAR GRINDER AS REQUIRED TO	1 a	
	GCHI SOP 0100 REV 2	ENSURE REMOVAL OF MATERIAL TO ACHIEVE MAG PERM REQUIREMENT. CIRCLE	NA	
520	RETEST MAG	AREA REMEDIATE FOR RETEST. RETEST MAG PERMEABILITY AT FAILED TEST POINTS. MARK NONCOMPLIANT AREAS		
520	PERM	WITH AN "X" FOR REPAIR.	d,	
	SOP MAG PERM	ACCEPTANCE 1.02.		
	100, REV 1	IF OK CHECK HERE . IF REJECTED CHECK HERE RETURN TO STEP 510.	V	
530	DOC. REVIEW	REVIEW DOCUMENTS AS REQUIRED IN CAF CHECKLIST, ALL DOCUMENTS NOTED TO BE		1
550	DOC. REVIEW	ACCESSIBLE FOR AUDITING. (SHIPPER, C OF C, M.T.R., M.T.S., INSPECTION REPORT, X-	1 9	60
		RAY READER SHEETS AND HEAT TREAT CHARTS)	ang	20
NOTICE	RELEASE FROM	PROVIDE DOCUMENTS TO EIO. SENT ON 9/30 BY	Q ENG	1 /
	EIO	RECEIVED RELEASE FROM EIO ON	OR QA	
			MGR	
540	PACK AND SHIP	PACKAGE AND SHIP TO MAJOR TOOL.		
1000	REVISION	ORIGINAL 12-14-04. Approved 12-14-04. Revision level 1- Revised 1-26-05 new page 8, correct High	CARUUD	
1000	HISTORY	stress areas, Revision level 2 3-16-05, delete LO step 455. Revision 3 3-28-05 Added note regarding	CAROOD	
		entre anna, terraria entre entre entre de se, delete de step four rechtston 5 5-20-05 Auded note regarding		

- California

#### A-1 Coil Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1 9 OF 11 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Issued: 6-14-05

hold point at weld step 400. Revision level 4 written for C-2 casting 4-18-05. Rev 5 added Layout SOP# and note regarding first casting layout responsibility. 5-10-05. Rev 6 5-29-05 added "LOT" to weld
material steps. Rev 7 6-14-05 added "LOT to supplement page weld step.

#### RED AREA INDICATES HIGH STRESSED AREA



#### A-1 Coil

Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Iss 10 OF 11 Dated Issued: 6-14-05

	REPEAT STEPS	SUPPLEMENTAL REPAIR STEPS	1 <sup>ST</sup>	2N D	3 <sup>RD</sup>	4 <sup>TH</sup>	5T H
S220	WELD SOP 0100 REV 7	EXCAVATE ANY DEFECTS FOUND DURING RADIOGRAPHY.	nG 8/2/	8/26			Н
S230	L.P. EXCAVATION CQP-300 REV 10	L.P. ALL EXCAVATIONS PRIOR TO WELDING TO ENSURE REMOVAL OF DEFECT. ACCEPTANCE PER A903. ACCEPTANCE CRITERIA-LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING.	LEVE L II				
S240	WELD MAP	MAP ALL WELDS WITH DIGITAL PHOTO/MAPS INDICATING LOCATION . SERIALIZE DEFECTS ON CASTING, USE SCALE IN PHOTOS AND DOCUMENT SIZE. THIS IS TO BE PERFORMED BY SUPERVISOR, INSPECTION LEAD MAN OR THEIR DESIGNEE, FILE WITH QA. MUST SEND REPORT ON ALL WELDS OVER 10% OF NOMINAL WALL THICKNESS TO CUSTOMER. DEFECTS>10% YES , REPORT SENT BY DATE SIGN BY QA ENG. REPAIRS MAY NOT PROCEED UNTIL INFORMATION IS SUBMITTED.	8/21	8/25			
NOTICE	WITNESS NOTIFICATION	PROVIDE NOTICE TO EIO AND DCMA AT LEAST FIVE DAYS IN ADVANCE OF WELD STEP. EIO NOTIFIED ON 8/2/ DCMA NOTIFIED ON 9/2/	Q ENG OR QA MGR				
S260	QA APPROVAL HOLD POINT	QA TO APPROVE ELECTRODE PRIOR TO USE. PROCEDURE USED:	MGK				
S270	WELD SOP 0100 REV 7	WELD REPAIR DEFECTS AS MARKED. FOR WELDS <2" - WPS 10-SMAW-CF8MNMN MOD REV 17 FOR WELDS <8" - WPS 15-GMAW-CF8MNMN MOD REV 2 ADD WPS FOR VERTICAL WELDS.	TAP 8/23	15 8/27			
S280	GRIND GCHI SOP 0100R2	HAND GRIND WELDS.	AB 8/24	OFB	/		
S290	L.P. WELD CQP 0300 REV 10	L.P. WELD REPAIRS ACCEPTANCE PER ASTM A903. ACCEPTANCE CRITERIA- LEVEL 1 FOR HIGH STRESSED AREAS, LEVEL 2 FOR ALL OTHER AREAS. SEE LP DRAWING. IF OK CHECK HERE WASH AND SEND TO STEP 300.	LP - LEVE LII	OK REIZ	OK REJ	OK REJ	OK RE

2

DK

R

#### A-1 Coil

## Energy Industries of Ohio Manufacturing and Test Sequence (MTS) Serial Number A-1 CO# 40851 Dated 3-9-05 Revision: Rev 7 Dated Iss

11 OF 11 Dated Issued: 6-14-05

The second s	IF REJECTED CHECK HEREAND RETURN TO STEP 220.	DA J
REPEAT	REPEAT STEPS S220 TO S290 AS REQUIRED TILL CLEAR THROUGH VISUAL INSPECTION & PENETRANT INSPECTION. DOCUMENT REWORK ON A	$QA = \frac{\delta}{28}$
	SUPPLEMENTAL MTS	Veri



Corrective Action 1308 Carondelet Division - CA / PA / RGA Database Corrective Action Type NCR Date 6/13/2005 CA Originator C. Ruud Pattern Number: C and A Coil Shims 11 Pieces

#### **Description of Defect / Non-Conformance**

Chemistry for 11 shim castings is out of specification.

#### **Root Cause**

Chemistry specification was not changed in system and not communicated to Lab personnel.

#### **Corrective Action**

Specification was corrected in system and Lab personnel trained. Mag permeability was checked on the parts and are less than 1.02u.

#### **Verification of Corrective Action**

Chemistries were checked on subsequent parts and are within specification.

#### Preventive Action

Create Inspection and Test Plan summarizing all requirements.

## Estimated Completion Date 6/15/05

Actual Completion Date Complete.

Signed: C. Ruud

CC: Roger Broman, Barry Craig, Joe Edwards, E.J. Kubick

#### Nonconformance Report: MetalTek CA 1308

**Project Disposition**: Use as is.

Approvals

Procurement Technical Representative \_\_\_\_\_\_ Wayne Reiersen for Phil Heitzenroeder

Responsible Line Manager \_\_\_\_\_

Mike Cole for Brad Nelson



Corrective Action 1323 Carondelet Division - CA / PA / RGA Database Corrective Action Type NCR Date 7/27/2005 CA Originator C. Ruud Applies to: Coil castings C-1, C-2, C-3, C-4 and A-1 and C 1 shim and four C coil and six A coil shims

#### **Description of Defect / Non-Conformance**

Phosphorus levels in material produced to date exceed specification limits. Both phosphorus and sulfur readings reported erroneously in certifications.

Certification reports have shown phosphorus and sulfur levels in the <.01% range. Independent laboratory data confirmed phosphorus in the .018 to .033% range and sulfur in the .005 to .022% range. Actual levels of some tests are above those in PPPL Specification NCSX-CSPEC-141-03-07 Rev 7.

Nonconformance was first suspected as a result of analysis of zoned attached test specimens volunteered by MetalTek International as response to PPPL questions on weighted average chemical analysis and quality of blending in the gating system. Nonconformance was verified on the bars used in the study and has been extended to evaluation of previously poured products.

#### **Root Cause**

Specification limits were set below the levels achievable through use of available raw materials. Spectrometer did not properly calibrate for phosphorus and sulfur at levels of specification due to equipment malfunction.

The chemical specification of EIO heats uses alloy CF8MNMn-Mod which incorporates a type standard calibration with a certified reference material (CRM) BS180. This enables the operator of the spectrometer to match the elemental concentrations of this alloy with corrective factors. These factors are determined by analyzing the CRM and having them compared with the calibration curves for each element. The phosphorus and sulfur content have very low measured intensities due to low concentrations. Intermittent failure of the spectrometer intensity measuring card caused higher intensity readings for phosphorus and sulfur. Subsequent checks with the CRM resulted in low corrective factors that were not detected. This in turn resulted in low reported concentrations for the EIO samples. All the major elements, which are measured on other intensity cards, have been closely monitored and matched very well with the CRM and thus were reported correctly.

#### **Corrective Action**

Modification to specification for phosphorus and sulfur will be requested. Limits will be set based on process capability and consistent with other stainless steel grades. Replacement of deficient card in spectrometer will be made upon delivery.



#### Addendum to CA1323 8-17-05

Historical:

The proto type coil was poured on February 24, 2004. The chemistry specification at that time permitted a maximum of 0.04% for sulfur and phosphorus. The reported values for these elements were 0.01 and 0.02% respectively.

Prior to pouring the C-1 coil casting the specification was revised. MT failed to incorporate the revisions into our system. The contract review procedure did not detect the changes to the specification. Therefore normal change procedures were not implemented. This was reported in corrective action 1308 on June 13, 2005. The error was recognized when the material poured to cast C and A coil shims did not meet the revised specification.

An investigation was begun immediately to determine compliance of the C-1 and C-2 coils. It was determined that both the C-1 and C-2 met the revised chemistry, except for sulfur and phosphorus. To verify the analysis MT analyzed samples from the cast on bars taken from the coils. By this time the optical card had malfunctioned. This fact, in combination with the human error (believing that the type standard was also in the 0.002% range) led MT to believe that the sulfur and phosphorus were actually in the 0.002% range. As a result MT believed the coils to be compliant and no action was taken.

#### Current Activities:

Samples from A-1, C-4 and C-5 have been sent to Wisconsin Centrifugal, our parent company for independent analysis of all reported elements.

Repair to the spectrometer is scheduled for this week. In the mean time we continue our surveillance of the suspect elements during melt and chemistry analysis.

C. Ruud Chlun

CC: Jim Galaske, Barry Craig, Joe Edwards, E.J. Kubick



#### Addendum to CA1323 9-8-05

This is to supplement and report our progress on this corrective action.

As previously committed, samples from A-1, C-4 and C-5 were sent to Wisconsin Centrifugal, our parent company, for independent analysis of all reported elements. The results indicated a discrepancy in the level of manganese in the results of the analyses performed by the two labs. Consistently, the Pevely lab measured Mn about 0.4 to 0.5% higher than WC measured. To confirm this information we sent three samples to an outside laboratory for wet chemistry analysis. The results correlated well with the results achieved at Wisconsin Centrifugal. See attached report.

In follow-up, samples from C-1, C-2 and C-3 were also sent for verification, with similar outcome. We then located and tested a sample from a test heat #21424 of CF8MNMNMOD made in January 2004. Testing indicated similar results.

It can be stated that, for at least the period of time comprising the Prototype and the Production to the repair of the Spectrometer, that our analysis of Manganese levels has been higher than the level actually present in the alloy. Typically, this deviation is on the order of 0.4-0.5%.

The spectrometer received the preventive maintenance on August 29, 2005. The report was submitted on September 2, 2005. The repair made to the optical card was determined to have rectified the previously reported issue with P and S reporting. No other mechanical or software problem that would affect Mn was determined at the time of the preventative maintenance.

In follow up to the Manganese discrepancy, the same samples were analyzed on the Pevely spectrometer. The levels reported after PM now correlate with the results from WC and the independent laboratory. Further investigation indicates that the BS180 standard used for type standardization may be sufficiently outside the range of Mn and inducing error. No other root cause has been determined, but the investigation continues.

In consideration of the erroneous Mn and other elemental readings, the following actions are proposed:

Create a type standard that closely matches the Mn in CF8MNMNMOD. (In process) Request a revision to the chemistry range for Mn. (propose widening of Manganese since it has been proven to be effective at much lower concentrations than previously thought). Have each heat of CF8MNMNMOD verified independently for balance of program.

C. Ruud CC: Jim Galaske, Barry Craig, Joe Edwards, E.J. Kubick

.ab	I.D.	Sample	С	Si	Mn	Cr	Ni	Мо	N	Р	S				
CAF	C-5,1-1	Button #1	0.05	0.3	2.6	18.1	13.4	2.4	0.26	0.023	0.011				
CAF	C-5,I-1	Button #2	0.05	0.4	2.6	18.0	13.4	2.6	0.26	0.026	0.013				
NC	C-5,I-1	Button #2	0.02	0.3	2.2	18.2	13.5	2.4	0.25	0.025	0.010				
STL Wet	C-5,I-1	Button #1			2.2										
CAF	C-5,I-1	Button #1	*	0.3	2.3	18.3	13.4	2.4	*	0.029	0.012	re-run after PM			
Timi												;	· · · · · · · · · · · · · · · · · · ·		
_ab	I.D.	Sample	С	Si	Mn	Cr	Ni	Mo	N	P	S		·		
CAF	C-5,1-3	Button #1	0.05	0.4	2.2	17.9	13.4	2.5	0.24	0.033	0.012				
CAF	C-5,1-3	Button #2	0.05	0.4	2.2	17.9	13.2	2.4	0.24	0.033	0.012	:			
WC	C-5,I-3	Button #2	0.05	0.4	1.8	18.2	13.4	2.5	0.23	0.034	0.018				
STL Wet	C-5,I-3	Button #1			1.8							····			
CAF	C-5,I-3	Button #1	*	0.4	1.8	18.3	13.3	2.5	*	0.034	0.012	re-run after PM			
									N	<u> </u>					
ab	I.D.	Sample	C	Si	<u>Mn</u>	Cr	Ni	Mo	<u>N</u>	P	S			···	
CAF	C-5,I-6	Button #1	0.05	0.3		18.1	13.2	2.4	0.25	0.030	0.012				
CAF	C-5,I-6	Button #2	0.05	0.3	2.4	18.1	13.2	2.4	0.25	0.029	0.011				
WC	C-5,I-6	Button #2	0.04	0.3	2	18.3	13.3	2.4	0.24	0.031	0.018				
STL Wet	C-5,I-6	Button #1			1.9					0.000	0.015				
CAF	C-5,I-6	Button #1	*	0.3	2.0	18.4	13.3	2.4	*	0.033	0.012	re-run after PM			
	i.D.	Sample	C	Si	Mn	Cr	Ni	Мо	N	P	S				
Lab			0.04	0.4	2.4	18.2	13.3	2.4	0.26	* *	*				
CAF	A-1	Reported	<u>0.04</u> *	0.4	2.4	18.0	13.3	2.4	*	0.034	0.009				
CAF	<u>A-1</u>	Cast on sample					13.4	2.4	0.25	0.034	0.009			·····	
WC	A-1	Cast on sample	0.06	0.6	1.6	18.1	13.7	2.4	0.20	0.027		re-run after PM			
CAF	A-1	Cast on sample		0.6	1.6	18.2	13.5	2.4		0.028	0.009	re-run alter Pivi			
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Мо	N	Р	S				
CAF	C-4	Reported	0.04	0.4	2.5	18.2	13.2	2.2	0.26	.030**	.014**	·····			
CAF	C-4	Cast on sample	*	0.6	1.9	17.9	13.5	2.3	*	0.037		1	. i		
WC	C-4	Cast on sample	0.04	0.6	1.5	17.8	13.6	2.4	0.25	0.030	0.012		1		
CAF	C-4	Cast on sample	*	0.6	1.4	18.2	13.6	2.4	*	0.031		re-run after PM			
		Cast on sample	_	0.0		10.2			1	1					
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Мо	N	Р	S				1
CAF	C-1	Reported	0.06	0.5	2.7	18.1	13.1	2.2	0.27	0.018**	0.014**	+			
CAF	C-1	Cast on sample	*	0.7	2.2	18.1	13.1	2.2	*	0.021	0.010				
WC	C-1	Cast on sample	0.06	0.7	1.8	18.3	13.4	2.4	0.24	0.021	0.014				1
CAF	C-1	Cast on sample	*	0.7	1.9	18.3	13.2	2.4	*	0.024	0.013	re-run after PM			F
	~·					1						· · · · · · · · · · · · · · · · · · ·			
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Мо	N	P	S				
CAF	C-2	Reported	0.06	0.5	2.8	18.0	13.2	2.3	0.26	0.023**	0.018**	* ]			
CAF	C-2	Cast on sample	*	0.8	2.2	18.1	13.4	2.2	. *	0.030	0.012				;
WC	C-2	Cast on sample	0.07	0.9	1.6	18.2	13.7	2.2	0.23	0.023	0.014	:			
CAF	C-2	Cast on sample	*	0.8	1.6	18.2	13.5	2.3	*	0.024	0.012	re-run after PM	1		
											-				
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Mo	N	P	S	•	· · · · · ·		
CAF	C-3	Reported	0.04	0.4	2.5	18.2	13.3	2.3	0.25		0.013**	•	!		
CAF	C-3	Cast on sample	*	0.6	1.9	18.0	13.3	2.4	*	0.027	0.010				
WC	C-3	Cast on sample	0.06	0.6	1.6	18.3	13.7	2.4	0.24	0.029	0.009				_, _, _,
CAF	C-3	Cast on sample	*	0.6	1.6	18.1	13.5	2.4	*	0.028	0.011	re-run after PM			
Test Hea	t poured 1/			<u> </u>		<u> </u>			L.						
	I.D.	Sample	C	Si	Mn	<u>Cr</u>	Ni	Mo	<u>N</u>	P	S				
Lab		24 Button	0.05	0.4	2.8	18.1	12.9	2.2	0.27	0.020	0.010				
Lab CAF CAF		24 Keel bar	*	0.4	2.2	18.2	13.2	2.2				re-run after PM			



#### Addendum to CA1323 9-30-05

This is to supplement and report our progress on this corrective action.

We have discussed the variation in reading the Mn levels with the service technician and the spectrometer manufacturer. No new information has been obtained to explain the differences in reading Mn levels.

The chemistry for the shims poured from heat 29198 has been analyzed and is added to the spreadsheet attached. It shows similar readings for Mn.

The chemistry for the C-6 coil is also added to the spreadsheet. We aimed for higher Mn at the furnace to assure the higher Mn levels. The results indicate the effort was successful.

Update as to action steps:

Create a type standard that closely matches the Mn in CF8MNMNMOD.

Completed at WC and has been sent to another laboratory.

Request a revision to the chemistry range for Mn. (propose widening of Manganese since it has been proven to be effective at much lower concentrations than previously thought).

Pending.

Have each heat of CF8MNMNMOD verified independently for balance of program.

Complete for all coils to date.

C. Ruud CC: Jim Galaske, Barry Craig, Joe Edwards, E.J. Kubick

Chemistr	v Check v	vith WISCO	Revised	9-30-05	,	Informati	ion in blu	le addeo	d 9-30-0	5		
Chemisu	y Check v										S	
Lab	I.D.	Sample	С	Si	Mn	Ċr	Ni	Мо	N	Р	5	
	98 for 5 C a	nd 6 Å shims		0.7	0.07	10.1	13.12	2.45	0.255	0.013**	0.01**	
CAF	29198	Reported 9/24/05	0.07	0.7	2.97	18.1 18.2	13.12	2.4	*	0.025	0.011	re-run after PM
CAF	29198	Separate Test bar		0.0	2.1	10.2	10.2	6.1		0.000		
		0 la	С	Si	Mn	Cr	Ni	Mo	N	Р	S	
	I.D.	Sample Button #1	0.04	0.3	2.5	18.2	13.5	2.4	0.25	0.028	0.010	run after PM
CAF	C-6,I-1 C-6,I-1	Button #2	*	0.2	2.4	18.1	13.6	2.4	*	0.031	0.012	run after PM
CAF WC	C-6,I-1	Button #2	0.03	0.2	2.4	17.9	13.7	2.5	0.26	0.028	0.010	
WC	C-0,I-1	Button #2	0.00	0.2					-			
Lab	I.D.	Sample	C	Si	Mn	Cr	Ni	Mo	N	P	S	
CAF	C-6,I-3	Button #1	0.04	0.4	2.4	18.2	13.4	2.3	0.25	0.034	a set of a set of a set of a	run after PM
CAF	C-6,I-3	Button #2	*	0.4	2.4	18.2	13.7	2.3	*	0.033		run after PM
WC	C-6,I-3	Button #2	0.03	0.4	2.2	17.9	13.6	2.4	0.25	0.023	0.013	
110											-	
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Мо	N	P	S	run after PM
CAF	C-6,I-6	Button #1	0.04	0.4	2.6	18.3	13.4	2.4	0.26	0.031		run after PM
CAF	C-6,I-6	Button #2	*	0.4	2.5	18.2	13.7	2.4	0.00	0.031		
WC	C-6,I-6	Button #2	0.04	0.4	2.4	18.2	13.7	2.4	0.26	0.030	0.014	
						0	Ni	Mo	N	P	S	
Lab	I.D.	Sample	C *	Si	Mn 1.7	Cr 18.1	NI 13.6	2.4	*	0.031	0.012	run after PM
CAF	C-6,Z-3	Cast on sample		0.6		17.8	13.8	2.4	0.26	0.025	0.011	run unor r m
WC	C-6,Z-3	Cast on sample	0.04	0.6	1.7	17.0	10.0	2.4	0.20			
		Comple	С	Si	Mn	Cr	Ni	Mo	N	P	S	
Lab	I.D.	Sample Button #1	0.05	0.3	2.6	18.1	13.4	2.4	0.26	0.023	0.011	
CAF	C-5,I-1	Button #2	0.05	0.3	2.6	18.0	13.4	2.6	0.26	0.023	0.013	
CAF WC	C-5,I-1 C-5,I-1	Button #2	0.00	0.3	2.2	18.2	13.5	2.4	0.25	0.025	0.010	
STL Wet	C-5,I-1	Button #1	0.02	0.0	2.2							
CAF	C-5,I-1	Button #1	*	0.3	2.3	18.3	13.4	2.4	*	0.029	0.012	re-run after PM
UAI	0-0,1-1	Button # 1	-									
Lab	I.D.	Sample	C	Si	Mn	Cr	Ni	Mo	N	Р	S	
CAF	C-5,1-3	Button #1	0.05	0.4	2.2	17.9	13.4	2.5	0.24	0.033	0.012	
CAF	C-5,1-3	Button #2	0.05	0.4	2.2	17.9	13.2	2.4	0.24	0.033	0.012	
WC	C-5,1-3	Button #2	0.05	0.4	1.8	18.2	13.4	2.5	0.23	0.034	0.018	
STL Wet	C-5,1-3	Button #1			1.8				*	0.001	0.010	re-run after PM
CAF	C-5,I-3	Button #1	*	0.4	1.8	18.3	13.3	2.5		0.034	0.012	re-run alter Pivi
							- NI		N	P	S	
Lab	1.D.	Sample	C	Si	Mn	Cr	Ni 13.2	Mo 2.4	0.25	0.030	0.012	
CAF	C-5,I-6	Button #1	0.05	0.3	2.4	18.1	13.2	2.4	0.25	0.029	0.012	
CAF	C-5,I-6	Button #2	0.05	0.3	2.4	18.3	13.3	2.4	0.23	0.031	0.018	
WC	C-5,I-6	Button #2	0.04	0.3	1.9	10.5	15.5	2.4	0.24	0.001	0.010	
STL Wet	C-5,I-6	Button #1	*	0.3	2.0	18.4	13.3	2.4	*	0.033	0.012	re-run after PM
CAF	C-5,I-6	Button #1		0.5	2.0	10.4	10.0	<u> </u>				
l ab	ID	Sample	С	Si	Mn	Cr	Ni	Mo	N	P	S	
Lab CAF	I.D. A-1	Reported	0.04	0.4	2.4	18.2	13.3	2.4	0.26	*	*	
CAF	A-1 A-1	Cast on sample	*	0.5	2.1	18.0	13.4	2.4	*	0.034	0.009	
WC	A-1 A-1	Cast on sample	0.06	0.6	1.6	18.1	13.7	2.4	0.25	0.027	0.009	
CAF	A-1	Cast on sample	*	0.6	1.6	18.2	13.5	2.4	*	0.028	0.009	re-run after PM
Lab	I.D.	Sample	С	Si	Mn	Cr	Ni	Mo	N	Р	S	
CAF	C-4	Reported	0.04	0.4	2.5	18.2	13.2	2.2	0.26	.030**	.014**	
CAF	C-4	Cast on sample	*	0.6	1.9	17.9	13.5	2.3	*	0.037		
WC	C-4	Cast on sample	0.04	0.6	1.5	17.8	13.6	2.4	0.25	0.030	0.012	no mun offer DM
CAF	C-4	Cast on sample	*	0.6	1.4	18.2	13.6	2.4	*	0.031	0.009	re-run after PM
						-	- NI	D.C	N	P	S	
Lab	I.D.	Sample	C	Si	Mn	Cr	Ni 13.1	Mo 2.2	0.27	0.01 3**		k
CAF	C-1	Reported	0.06	0.5	2.7	18.1	13.1	2.2	1.27	0.073	0.014	
CAF	C-1	Cast on sample		0.7	1.8	18.1	13.1	2.4	0.24	0.021	0.010	
WC	C-1	Cast on sample	0.06	0.7	1.8	18.3	13.4	2.4	*	0.02.4		
CAF	C-1	Cast on sample		0.7	1.9	10.5	10.2	2,4		0.01.4	1	
1.05	10	Sample	С	Si	Mn	Cr	Ni	Mo	N	P	S	
Lab	I.D. C-2	Reported	0.06	0.5	2.8	18.0	13.2	2.3	0.26	0.023**		*
CAF CAF	C-2 C-2	Cast on sample	*	0.8	2.2	18.1	13.4	2.2	*	0.0:30	0.012	
WC	C-2 C-2	Cast on sample	0.07	0.9	1.6	18.2	13.7	2.2	0.23	0.0:23	0.014	
CAF	C-2	Cast on sample	*	0.8	1.6	18.2	13.5	2.3	*	0.0.24		re-run after PM
CAF	0-2	oust on sample		1 0.0				-				

ab	I.D.	Sample	C	Si	Mn	Cr	Ni	Mo	N	P	S	
CAF	C-3	Reported	0.04	0.4	2.5	18.2	13.3	2.3	0.25	0.023**	0.013**	
CAF	C-3	Cast on sample	*	0.6	1.9	18.0	13.3	2.4	*	0.027	0.010	
VC	C-3	Cast on sample	0.06	0.6	1.6	18.3	13.7	2.4	0.24	0.029	0.009	
CAF	C-3	Cast on sample	*	0.6	1.6	18.1	13.5	2.4	*	0.023	0.011	re-run after PM
est Hea	t poured 1/14	1/04	_									
ab	I.D.	Sample	C	Si	Mn	Cr	Ni	Mo	N	P	S	
CAF	24424	Reported	0.054	0.4	2.8	18.1	12.94	2.21	0.27	0.020	0.010	
CAF		Keel bar	*	0.4	2.2	18.2	13.2	2.2	*	0.013	0.010	re-run after PM
not ana	lyzed by spec	ctrometer.										
* analyz	ed by wet che	emistry. nd N were analyze										

Subsequent immediate analysis of chemistry results, obtained by wet analysis, is attached and demonstrate top of specification for sulfur and over specification for phosphorus. The spectrometer manufacturer has performed an analysis to determine the cause of the malfunction and verified that the intensity card has an intermittent fault and must be replaced. The card has been ordered and scheduled for replacement on August 15, 2005.

Until the card is replaced we will be performing additional type standardizations to ensure accurate sulfur and phosphorus analysis. Additionally, for coils made until the card is replaced, an independent laboratory will perform a verification of the chemical analysis.

#### Verification of Corrective Action

Will be determined at a later date.

#### **Preventive Action**

In addition to spectrometer faults, we have identified that the specification ranges for sulfur and phosphorus is unattainable. Analysis and specifications for virgin charge materials predict sulfur at 0.040% maximum and phosphorus at 0.040% maximum. We have no way to remove phosphorus from the melt and do not intentionally add phosphorus. So, the confirmed coil analyses, along with analyses of virgin material heats, demonstrate sulfur in the range of 0.010% to 0.022% and phosphorus in the range of 0.018% to 0.033%. These results are consistent with our charge material analysis. We will request a deviation for phosphorus in the subject parts and also request a permanent specification change to 0.040% maximum for both phosphorus and sulfur, to allow us to provide non-discrepant material. This change will not affect, in any way, the physical properties or material performance because all coils and test material exhibited sulfur and phosphorus within the new ranges despite inaccurate reporting. Other actions: Specifications have been added to the BS 180 standard and the type standard will be measured against the criteria.

#### **Estimated Completion Date**

August 15, 2005

Actual Completion Date TBD

Signed: C. Ruud

nAn -

CC: Jim Galaske, Barry Craig, Joe Edwards, E.J. Kubick

Sample name	Sample origin
A1Z1	Cast on bar A-1 coil, zone 1
A1Z2	Cast on bar A-1 coil, zone 2
A1Z3	Cast on bar A-1 coil, zone 3
C1	Cast on bar C-1 coil
C2Z1	Cast on bar C-2 coil, zone 1
C2Z2	Cast on bar C-2 coil, zone 2
C2Z3	Cast on bar C-2 coil, zone 3
C3Z1	Cast on bar C-3 coil, zone 1
C3Z2	Cast on bar C-3 coil, zone 2
C3Z3	Cast on bar C-3 coil, zone 3
F1	Final analysis button from ladle for C-4 coil
F2	Final analysis button from ladle for C-4 coil
F3	Final analysis button from ladle for C-4 coil
P1	Preliminary analysis button from ladle for C-4 coil

#### Guide to St Louis Testing Report Dated 7-26-05

Testing is underway of the heat used to pour the four C coil and six A coil shims.

ST LOUIS TESTING LAB

PAGE 01/01



Chemical, Metallurgical, Mechanical, Nondestructive, Environmental Testing, Analyses and Field Service.

July 26, 2005 Lab No. 05C-0608 Invoice No. 59891 P.O. No. 21324 Page 1 of 1

#### METALTEK INTERNATIONAL 8600 Commercial Blvd.

Pevely, MO 63070

#### Attention: Chuck Ruud

#### REPORT OF CHEMICAL ANALYSIS

SAMPLE ID: A1 Z1, A1 Z2, A1 Z3, C1, C2 Z1, C2 Z2, C2 Z3, C3 Z1, C3 Z2, C3 Z3, F1, F2, F3, P1

RESULTS: %									
ANALYTE	A1Z1	A1Z2	A1Z3						
Sulfur	.013	.005	.010						
Phosphorus	.025	.023	.018						

ANALYTE	C1 ,	C2Z1	C2Z2	C2Z3
Sulfur	.014	.022	.018	.015
Phosphorus	.018	.024	.021	.025

ANALYTE	C3Z1	C3Z2	C3Z3	
Sulfur	.013	.014	.012	
Phosphorus	.024	.025	.021	

ANALYTE	F1	F2	F3	P1
Sulfur	.014	.015	.012	.010
Phosphorus	.029	.033	.028	.030

Sulfur Test Method: ASTM E1019-03

Phosphorous Test Method: Colormetric

Identification of tested specimen provided by the client.

Robin E. Sinn Laboratory Director



#### **Corrective Action** 1324

Corrective Action Type FOR CASTING DISCONTINUITIES

Date 7/18/2005

MetalTek International

Carondelet Division - CA / PA / RGA Database

CA Originator C. Ruud Pattern Number: A-L Coil

Description of Defect / Non-Conformance 98 major weld defects found in the A-1 coil casting.

Root Cause : Casting defects primarily due gas and shrink.

**Corrective Action:** Weld upgrade A1 casting. Welding will be performed following the approved procedure FOR WELDS <2" - WPS 10-SMAW-CF8MNMN MOD REV 1. FOR WELDS <8" - WPS 15-GMAW-CF8MNMN MOD REV 2.

Verification of Corrective Action: All repairs will be verified by the inspection method used to discover the original defect.

Preventive Action: We will use the xray information from the A1 casting to determine if changes are required to the tooling.

Verification Of Preventative Action: Radiograph A-2 coil and compare results.

Estimated Implementation Date: Prior to shipment.

Signed: CA Ruud

CC: EIO, Barry Craig, Joe Edwards, E.J. Kubick, Geoff Mergel, File

Disposition for CA 1324: Perform weld upgrades per MTM procedures.

•

Approved:

Tech. Representative

Phil Heitzenroeder 2005.08.25 16:20:38 -04'00'

Brad RLM Nelson Digitally signed by Brad Nelson DN: cn=Brad Nelson, c=US, o=ORNL, ou=FED, email=nelsonba@oml.gov Date: 2005.08.25 17:23:22 -04'00'



Corrective Action 1347 Carondelet Division - CA / PA / RGA Database Corrective Action Type NCR Date 8/1/2005 CA Originator C. Ruud Applies to: A-1Coil

### Description of Defect / Non-Conformance

Wall thickness below model minimum. Localized areas were measured below the 1.375" minimum wall thickness during metrology. MetalTek independently verified wall thickness and confirmed condition.

### **Root Cause**

Cannot be determined at this time. Under evaluation.

### **Corrective Action**

Request "Use As Is" disposition on wall thickness related dimensions on A-1 coil.

#### Verification of Corrective Action

Not required. PPPL independently verified in conjunction with ORNL the design performance at a wall thickness of 1.05". Results were deemed adequate. Minimum measured dimension is 1.18" (to be verified).

#### **Preventive Action**

Several steps need to be taken to resolve and propose:

- 1. Validation of 3D Scanco data. MetalTek proposes to use Romer Arra with Laser scanner as validation technique. This instrument will be used to validate subsequent parts and minimizes measurement technique error. Date TBD.
- Report to PPPL/ORNL. Understanding the concern that the wall not be thinner than measured and the limitations of the process, e.g. setting a large core into a mold with overhead crane, MetalTek will submit layout results to EIO wand set teleconference to review remediations to tool. Date TBD.
- 3. Upon verification of 3D Scanco data, MetalTek will confirm results to EIO team to begin root cause determination. Additional layout may be required to assure compliance of tooling, depending on results of layout. Date TBD.
- 4. Modification to tooling. Limited tooling modifications may be performed without severely impacting schedule or negating previous engineering (solidification modeling, etc.). These will be evaluated and proposed, where appropriate.
- 5. Permanent deviation. Based on results of above, a permanent deviation may be required to dimensional tolerances in limited areas of the component. These will be known in greater detail later.

### Estimated Completion Date TBD

Actual Completion Date TBD

Signed: C. Ruud

Chr

CC: Roger Broman, Barry Craig, Joe Edwards, E.J. Kubick

### NCSX Disposition to CA 1347

Analyses were performed to determine the effect of the thin section on deflections and stresses and are summarized below.

• Thin shell areas like that of A1 has an extremely minor affect on the stresses and displacements in ANY of the coils or shells with the thickness being either 1.18" as for A1 or even with the thickness being 1.05" which MTK projects is the minimum if the shell is not changed. Reasons:

a) The shape of the tee is not changed by this, and the tee provides most of the bending stiffness

b) Some EM forces are transferred to the shell B from the wing.

c) The thin wall region is not the location for the peak stress and much of the area will be machined away.

		Shell Type	<u>a A</u>	Coil Type	A	All Coils	5
		Max.	Max.	Max.	Max.	Max.	Max.
<u>Run #</u>	Configuration	Displacement - mm	Stress - Mpa	Displacement - mm	Stress - Mpa	Displacement -	Stress - Mpa
1	Baseline	0.98	168	1.246	239	2.711	239
5	Updated E	1.17	160	1.513	248	2.934	248
6	Updated E; thin sect. =1.18"	1.169	161	1.516	249	2.984	249
4	Updated E; thin sect. =1.05"	1.168	161	1.517	248	2.971	248

Since the effect has been shown to be extremely minor, the disposition for the A1 winding form is **Accept As Is.** 

However, since the root cause determination is still underway, this NCR should be kept open. It is requested that EIO re-issue an amended CA with the root cause determination and preventive action; PPPL will disposition that portion of the NCR at that time.

#### **Approved:**

Phil Heitzenroeder 2005.08.19 14:10:46 -04'00'

### P. Heitzenroeder, Tech. Rep.

Brad Nelson Digitally signed by Brad Nelson DN: cn=Brad Nelson, c=US, o=ORNL, ou=FED, o=ORNL, ou=FED, ou=RED, ou=State 2005.08.19 16:56:28-04100

B. Nelson, RLM



Corrective Action 1371 Carondelet Division - CA / PA / RGA Database Corrective Action Type NCR Date 8/23/2005 CA Originator R. Suria Applies to: A-1Coil

### Description of Defect / Non-Conformance

Lack of fusion and porosity in weld repairs were observed during radiography of the R-2 through R-6 x-ray confirmation shots.

### **Root Cause**

Porosity was caused by the use of fans in the welding booth. Lack of fusion was the result of poor operator technique and or fatigue. Some repair loops resulted from the original defects not fully being removed during excavation.

### **Corrective Action**

Unplug fans during GMAW welding. Reviewed proper GMAW gun angles and excavation techniques with the welders.

### Verification of Corrective Action

Re x-ray the defective welds.

Estimated Completion Date 8/31/05

Actual Completion Date 8/31/05

Signed: R. Suria

CC: Barry Craig, Joe Edwards, E.J. Kubick



8600 Commericial Blvd. - Pevely, MO 63070 USA Phone: 636-479-4499 - Fax: 636-479-3399

# **Final Inspection Report**

Customer Name: ENERGY INDUSTRIES OF OHIO Pattern: MCWF-A1 COIL

Order Number: PPPL-FP-LTS-2

ASTM Metal CF8MN	MN MOD	Date	8/30/2005	
Type Description	Cert Number	Procedure	Acceptance Criteria	Actual
Liquid Penetrant	169470-1	CQP - 300 Rev 9	SEE NOTE	Acceptable
Notes Acceptance per As	STM A903. Acceptanc	ce criteria - level 1 for high stressed area	as, level 2 for all othe area	IS.
Mag Perm	169470-1	SOP Mag Perm 100 Rev 1	<1.02	Acceptable
Radiographic	169470-1	Technique # 12726	MSS SP 54	Acceptable
Visual	169470-1	CQP - 500 REV 4	ASTM A802 LEVEL 2	Acceptable

Liquid Penetrant Visual Technician: <u>Kevin Anderson</u> ASNT Level II

Respectfully Subrritted, Charles A. Ruud Quality Assurance Manager

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Superior Quality Engineered Metal Products



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# **Certificate of Conformance**

### ENERGY INDUSTRIES OF OHIO

Order Number PPPL-FP-LTS-2

Pattern MCWF-A1 COIL

ASTM Metal CF8MNMN MOD

Date 8/30/2005

Cert Number

169470-1

We certify that we have complied in accordance with the drawings(s) and specifications(s) listed on the above purchase order. The articles furnished were made and/or processed from parts and/or materials in accordance with all applicable drawings(s) and specifications(s) pursuant to the afore mention purchase order.

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

# Superior Quality Engineered Metal Products

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# **Final Inspection Report**

Customer Name: ENERGY Pattern: SE-141-033 COIL A SHIM INDUSTRIES OF OHIO

Order Number: PPPL-FP-LTS-2

ASTM Metal CF8MN	MN MOD	C	Date	8/30/2005	
Type Description	Cert Number	Procedure		Acceptance Criteria	Actual
Liquid Penetrant	S76220-1	CQP - 300 Rev 9		ASTM A903 Level II	Acceptable
Mag Perm	S76220-1	SOP Mag Perm 100 Rev 1		<1.02	Acceptable
Radiographic	S76220-1	Technique # 12726		MSS SP 54	Acceptable
Visual	S76220-1	CQP - 500 REV 4		ASTM A802 LEVEL 2	Acceptable

Liquid Penet	rant
Technician:	Jason Reese
	ASNT LevelII

# Visua1

Technician: <u>Kevin Anderson</u> ASNT Level II

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

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# **Certificate of Conformance**

ENERGY INDUSTRIES OF OHIO

SE-141-033 COIL A SHIM

Order Number PPPL-FP-LTS-2

Pattern

Alloy CF8MNMnMOD

S<u>/</u>N 2

Date 8/30/2005

Cert Number

S76220-1

A shim for A-1 coil was poured from heat number 29198. No weld repairs were necessary.

We certify that we have complied in accordance with the drawings(s) and specifications(s) listed on the above purchase order. The articles furnished were made and/or processed from parts and/or materials in accordance with all applicable drawings(s) and specifications(s) pursuant to the afore mention purchase order except as noted by corrective actions.

Respectfully Submitted, Charles A. Ruud Quality Assurance Manager

# Superior Quality Engineered Metal Products

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### EIO Energy Industries of Ohio SUPPLIER QUALITY RELEASE

Page 1 of 2

							Date: 9-01-05	
I. General Information:								
Project Name:	Modular Coil \		n A1					
PO No:	NCSX-SOW-1	141-02-01					Rev.:	
Supplier:	MetalTek							
Procurement Agent:	EIO							
Shipment:	🛛 Partial	🗌 Final						
II. Material Descript	tion							
Casting A1 Coil								
1								
III. Release Checklis	II. Release Checklist							
Plan Requirements C								
	Complete?	X Y	es 🗌 No	□ N/A	(If identified "No"	provide exp	planation in comments section below)	
Variances?	Complete?			□ N/A □ N/A			planation in comments section below) planation in comments section below)	
Variances? Princeton Notified of	•		es 🗌 No		(If identified "No"	provide ex	,	
	Shipment?	X	es ☐ No es ☐ No		(If identified "No" (If identified "No	provide exp provide exp provide ex	planation in comments section below)	
Princeton Notified of	Shipment?		es ☐ No es ☐ No	□ N/A □ N/A	(If identified "No" (If identified "No	provide exp provide exp provide ex	planation in comments section below)	
Princeton Notified of	Shipment?		es	N/A N/A N/A	(If identified "No" (If identified "No	provide exp provide exp provide exp provide exp	planation in comments section below)	
Princeton Notified of DCMA Notified of Sh	Shipment? ipment?		es	N/A N/A N/A	(If identified "No" (If identified "No (If identified "No	provide exp provide exp provide exp provide exp	planation in comments section below)	
Princeton Notified of DCMA Notified of Sh	Shipment? ipment?		es	N/A N/A N/A	(If identified "No" (If identified "No (If identified "No	provide exp provide exp provide exp provide exp	planation in comments section below)	
Princeton Notified of DCMA Notified of Sh I Conditional	Shipment? ipment? ] Unconditiona	al Expla	es No es No es No ain condition	□ N/A □ N/A □ N/A	(If identified "No" (If identified "No" (If identified "No" (If identified "No" es in comments s	provide exp provide exp provide exp provide exp	planation in comments section below)	

By signing below you acknowledge that the casting has met all applicable standards and contractual requirements

V. Supplier Quality Representative Sign Off		
		9-01-05
Charles Ruud	X Colum	
Supplier Quality Representative (SQR)	Supplier Quality Representative (SQR)	
Print/Type Name	Signature	Date

VI. Supplier Approval For Shipment		
Procurement Agent Notified of Shipment	Date: 9-01-05	
Required Vendor Data Ready for Shipment	Date: 9-01-05	
Peter A Djordjevich	Paka. Palif	9-01-05

# Pg 1 of 2

# **Energy Industries of Ohio**

Corrective Action Report/Request ID#0002

Date 12-28-05

Due: N/A

**Initiated By: Peter Djordjevich** 

Issue/Non Conformance: A series coil, thin wall condition Per previous MTK issue NCR#1347

**Root Cause:** Casting shrinkage in excess of factored pattern shrink. Due to solidification variances casting shrinkage varied from the norm. Although this is not 100% conclusive it is the most likely culprit.

**Corrective Action:** Although the pattern can be stocked, after review it has been determined to use as is. A minimum wall thickness has been established and adhered to.

Verification of Corrective Action: Per team discussions the above has been implemented.

Pg 2 of 2

**Completion / Verification Date 01-03-06** 

Signature EIO Quality

Peter Djordjevich

### EIO Energy Industries of Ohio SUPPLIER QUALITY RELEASE

Page 2 of 2

			Date: 9-0	)1-05	
I. General Information	on:				
Project Name:	Modular Coil Winding Form A1				
PO No:	NCSX-SOW-141-02-01 Rev.:				
Supplier:	MetalTek				
Procurement Agent:	EIO				
Shipment:	🛛 Partial 🛛 🗌 Final				
	Supplier's Representative				
Pr	Print/Type Name Supplier's Signature Date			Date	

- 1. Enter: Project Name PO Number Supplier Procurement Agent
- 2. Enter a brief description of items being released, including applicable drawing number(s), dash or item number(s), drawing revision letter, specification(s), and serial number(s).
- 3. Self-Explanatory
- 4. Record any unusual circumstance, such as a conditional release.
- 5. The Supplier's representative shall sign and date.
- 7. Signature and date of the Supplier's authorized representative indicating shipping date.
- 8. In case of partial release, the supplier shall maintain copies of each sequential "Supplier Quality Release" and establish complete accountability of material release on final shipment.
- 9. Supplier shall include a copy of the completed form with each shipment.

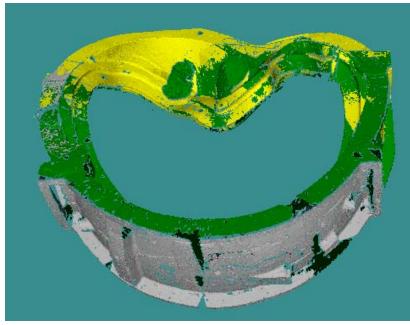


December 28, 2005

## Project # 0412 Fusion Chamber Castings A Casting

Tim Wenninger Project Manager Lawton Pattern Division 1950 De Pere, WI 54115 <u>timw@calawton.com</u> 920-983-4053

This letter is intended to document a tolerance loss observed during dimensional inspection of an A casting and the corrective actions that were used to recover satisfactory tolerances. The tolerance loss occurred due to an unforeseen set of circumstances and Standard Operating Procedures will be updated to prevent future problems even in such a rare occurrence.



The castings were scanned in three separate "sessions" as shown in yellow, green, and gray. Each session was scanned using a Konica-Minolta 9i/PSC-1 measurement system ISO certified to +/-0.05mm (0.002in).

This system uses a widely accepted technique called Photogrammetry to establish the accuracy of the measurement session. Theoretically only 3 points are required to establish a reference system. When more than three points are used the redundancy allows the system to track error. For this part, over 300 reference markers were used.

Figure 1: The part was measured in 3 separate measurement sessions.

Each of the three major sessions shown above when considered independently is known to be within the accuracy capabilities of the system. The task of combining the separate measurement sessions typically relies on simply locking in overlapping data to lock in the separate sessions together. The unique geometries provide a 3d "lock and key" that ensures an accurate alignment.

The problem encountered on this casting occurred when trying to locate the bottom session (in grey above) relative to the main session (in green above). The main session was taken with the part resting on the floor such that the entire grey surface was not accessible as shown in Figure 2.

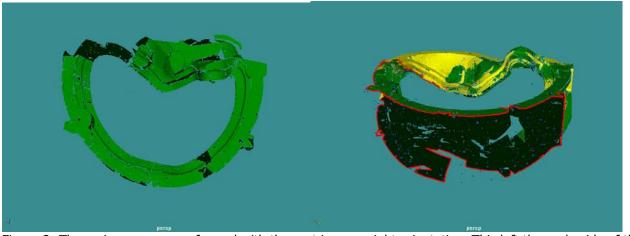


Figure 2: The main scan was performed with the part in an upright orientation. This left the underside of the part un-scanned since it was facing the floor.

Typically the goal is to get enough overlap between any two sessions so as to enable a tight lock between them, as shown between the yellow and green sessions in Figures 2 and 3. When the part was layed down to scan the bottom (grey side) the problem was that the edge of the scan almost exactly matched the edge of the green session. There was some overlap on the left side but the lack of overlap on the right side caused a misalignment to occur that resulted in the grey session not being placed properly and thus producing error in thickness calculations in that area. The fact that the outlines (shown in red) matched so closely is a rare occurrence that caused an unforeseen problem.

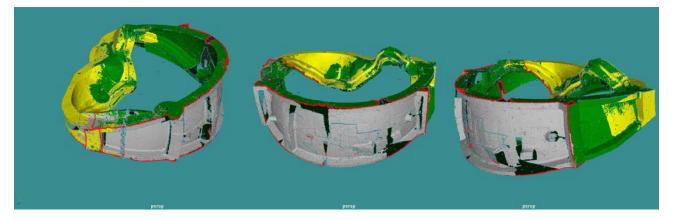


Figure 3: The edges of the green and grey sessions are shown in red.

### The Solution:

To rectify the problem, reference marks were recovered from the original data. The points circled in Figure 4 were captured in the background on the opposite side of the part. These reference marks were then able to be used to register the grey session to the green session. Not only did it provide a solution for aligning the two but it also provides an achieved accuracy result. The cluster of reference marks matched from grey to green sessions to within +/- 0.00175 inches! Unfortunately because there were no reference marks in common in the foreground of the grey scan and the fact that these reference marks are on the opposite side of the part, a lever arm effect must be accounted for to compensate for how a small error on the opposite side is magnified before it resolves on the foreground side.

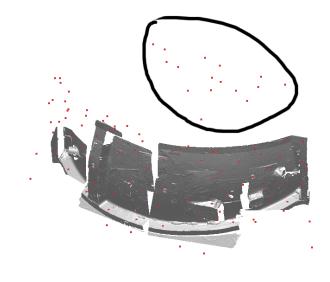
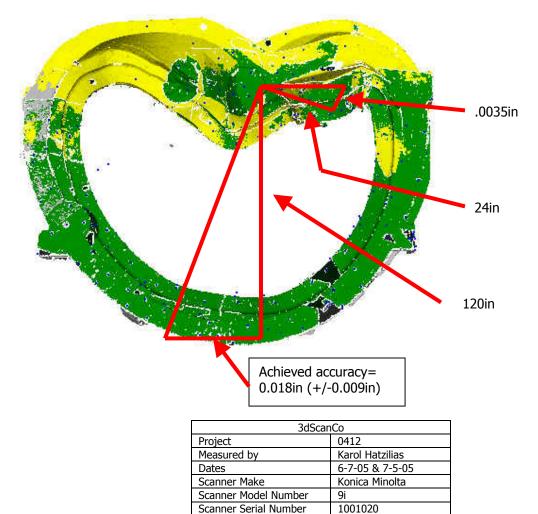


Figure 4: A cluster of reference markers was fortunately recovered in the background of this scan.

#### Achieved Accuracy:

All three sessions independently remained within working tolerances during the scanning operation and thus the quoted system accuracy of 0.05mm (0.002in) applies. When considering the entire inspection as a whole, the largest error source is from this lever arm effect due to having to use reference marks from across the part. A conservative distance of 120in was used for the lever arm as the part can easily fit inside that distance. Similarly a conservative "platform width" of 24in was used to approximate the width of the "base" of the lever arm since the cluster of reference marks used is at least 24in in the narrowest area. Therefore the achieved accuracy when considering the fact that there is a lever arm effect comes to 120tan(sin^ - 1(0.0035/24))=0.018in or +/-0.009in. Therefore the thickness measurements and all other measurements on the inspection should have tolerance of +/- 0.009in taken into consideration at all times. If that achieved accuracy is not sufficient, then it may be necessary to rescan in order to attempt to achieve a higher tolerance.



Scanner Last Calibrated

Scanner Cal Artifact

Photogrammetry Make

Photogrammetry Model

Photogrammetry Serial

Photog Cal Artifact

Photogrammetry Last Cal

#### Disclaimer:

The results of this analysis are believed to be reliable but are not to be construed as providing a warranty, including any warranty of merchantability or fitness for purpose, or representation for which 3dScanCo assumes legal responsibility. Client should undertake sufficient verification and testing to determine the suitability of any information presented. It is the sole responsibility of the Client to review the results and make any determinations. Nothing herein is to be taken as permission, inducement or recommendation by 3dScanCo to practice any patented invention without a license or to in any way infringe upon the intellectual property rights of any other party.

6-6-05

PSC-1

1001020

7281026

7141013

Konica Minolta

6-6-05 & 6-16-05

#### 3dscanco\_0412\_acasting\_20050713

Date: 7/7/2005 / Time: 7:30:05PM

Source Filename:

inspecting\_01.mdl

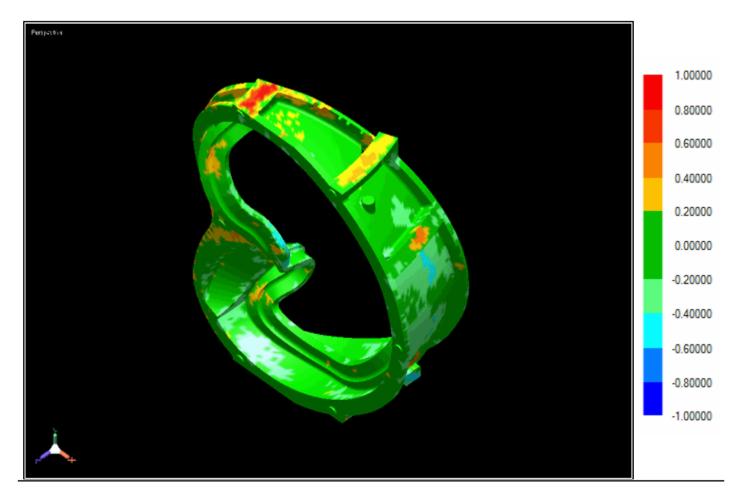
Length Unit: in

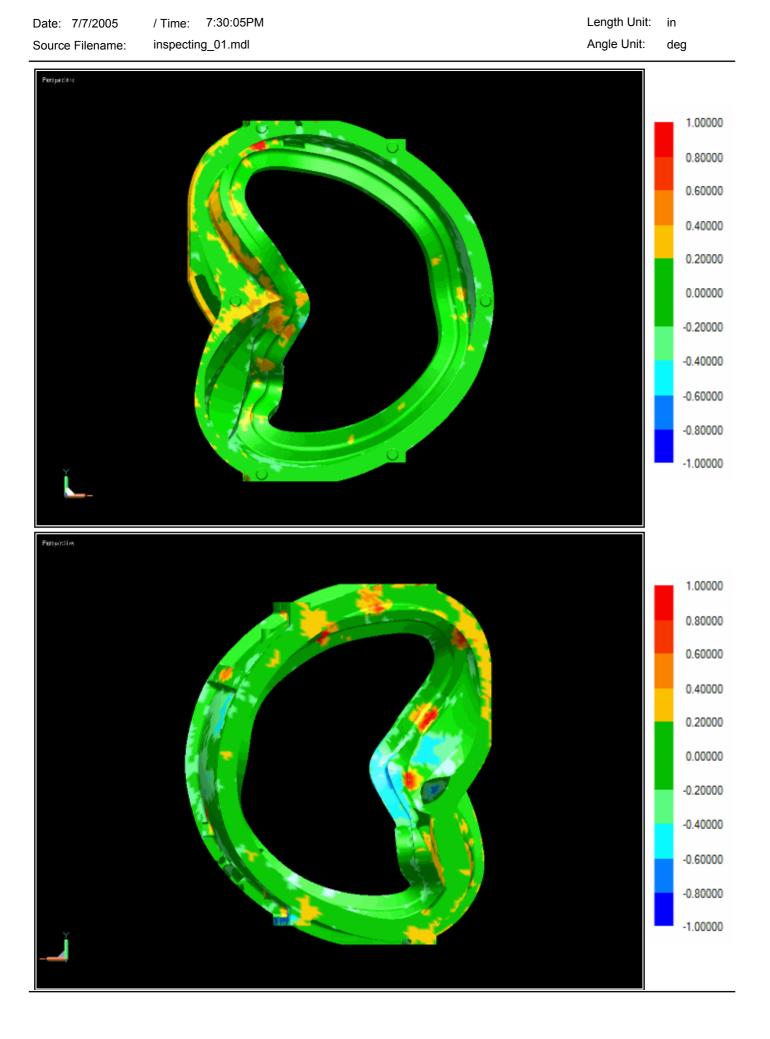
Angle Unit: deg

# Whole Deviation Session

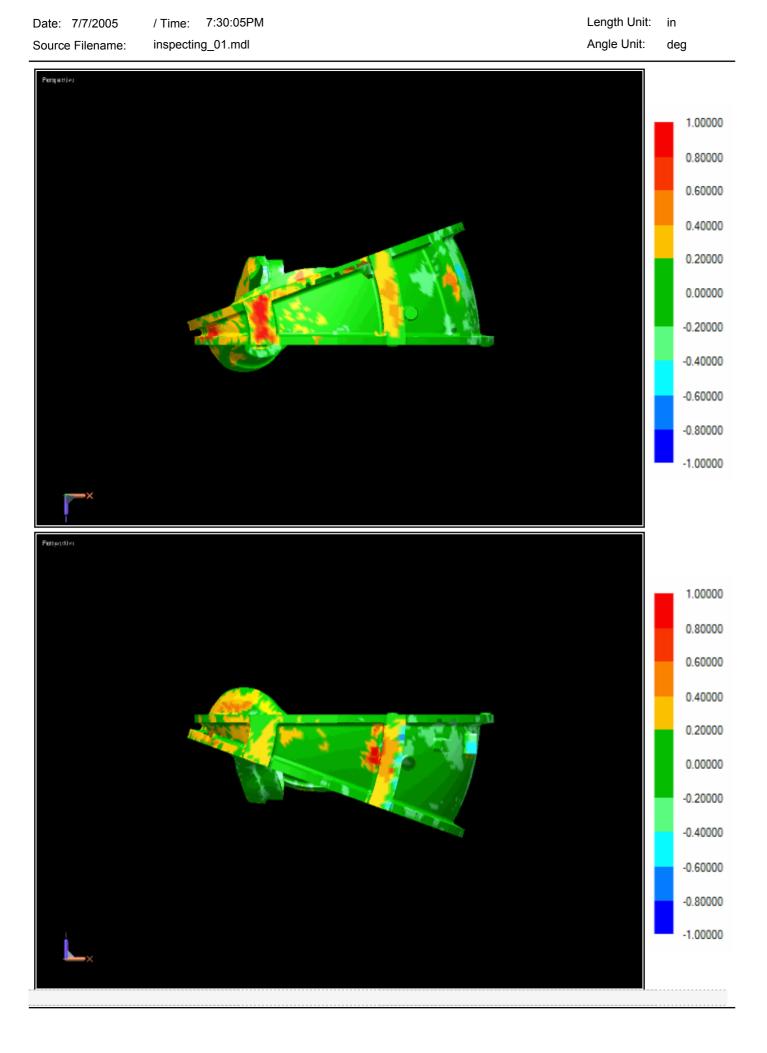
### Type: Surface Type

Type: Canado Type						
Name: Whole Deviation	Name:Whole Deviation 2Calculate Tolerance:2.81862					
1st Reference Entity:	scan_2_merge3_PGNOPG and scan_merge_02	Acceptable Tolerance:	0.00000			
		Maximum Range:	1.00000			
2nd Reference Entity:	521 Surfaces	Minimum Range:	-1.00000			
		Average:	-0.01692			
		Standard Deviation:	0.26034			





Length Unit: / Time: 7:30:05PM in Date: 7/7/2005 Angle Unit: Source Filename: inspecting\_01.mdl deg Perspective 1.00000 0.80000 0.60000 0.40000 0.20000 0.00000 -0.20000 -0.40000 -0.60000 -0.80000 -1.00000 Peripet(in) 1.00000 0.80000 0.60000 0.40000 0.20000 0.00000 -0.20000 -0.40000 -0.60000 -0.80000 -1.00000



in

deg

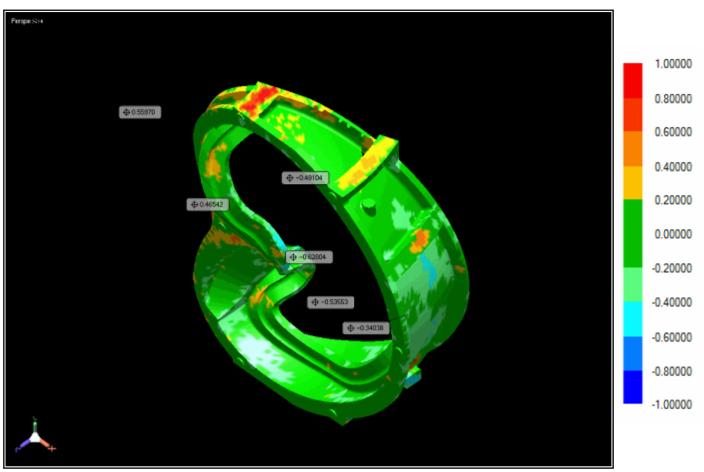
Source Filename:

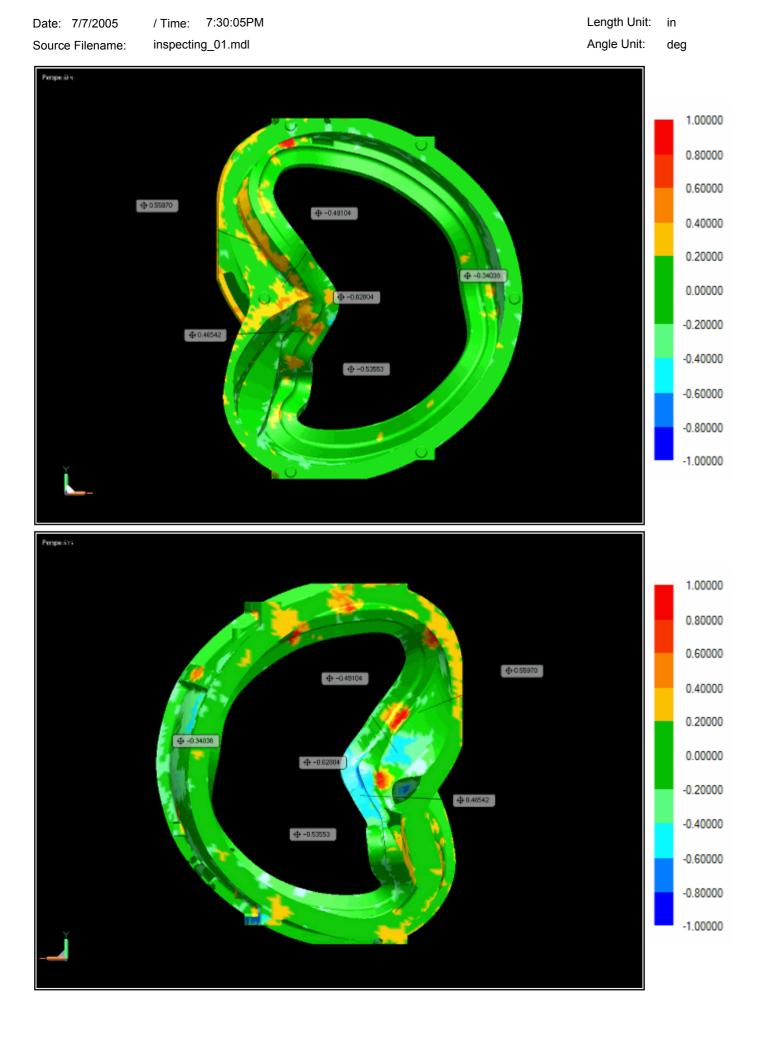
inspecting\_01.mdl

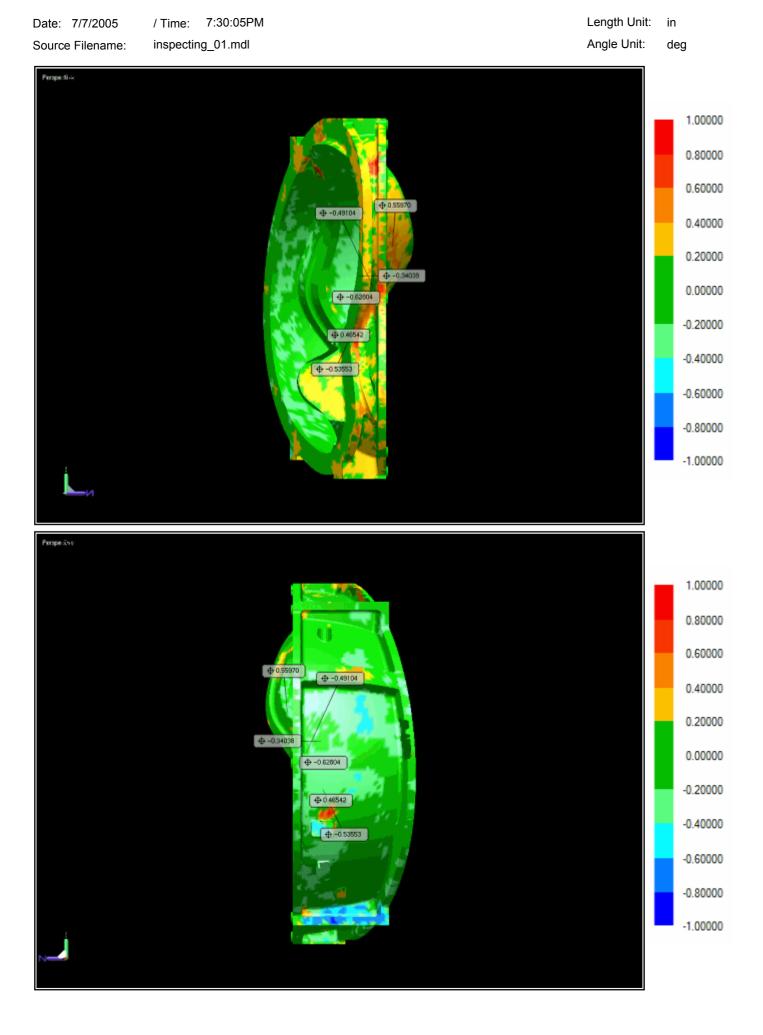
Annotation Session

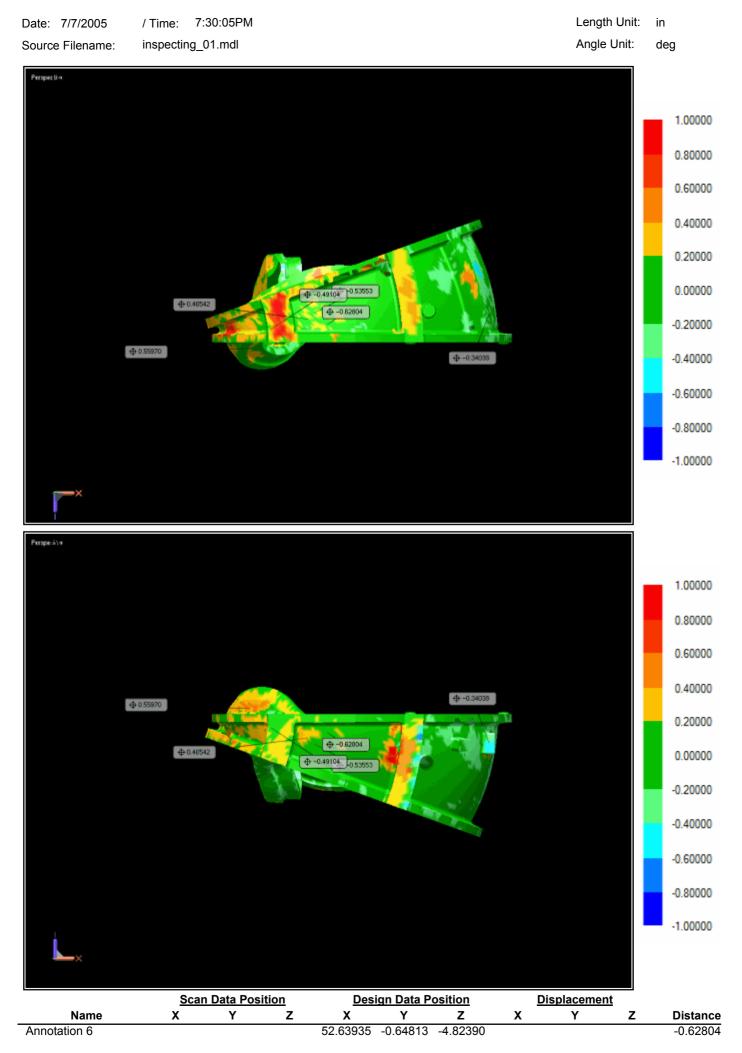


Whole Deviation 2











December 28, 2005

## Project # 0412 Fusion Chamber Castings A Patterns

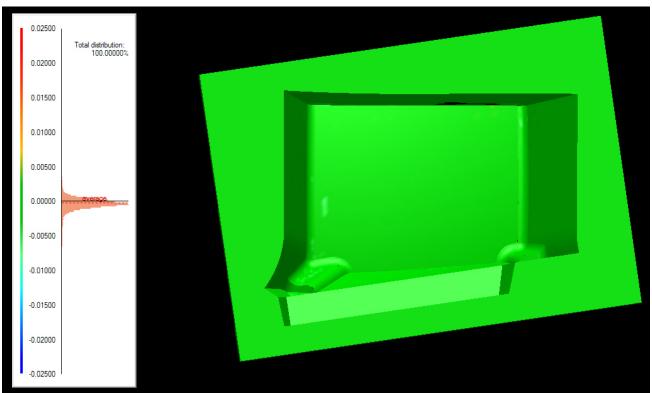
Tim Wenninger Project Manager Lawton Pattern Division 1950 De Pere, WI 54115 <u>timw@calawton.com</u> 920-983-4053

After reviewing the scan data from the A patterns it is evident the original results provided with inspection results are sound. A double check of the data was done for all core boxes including the cope and drag. The alignment of the scan data to CAD was also verified.

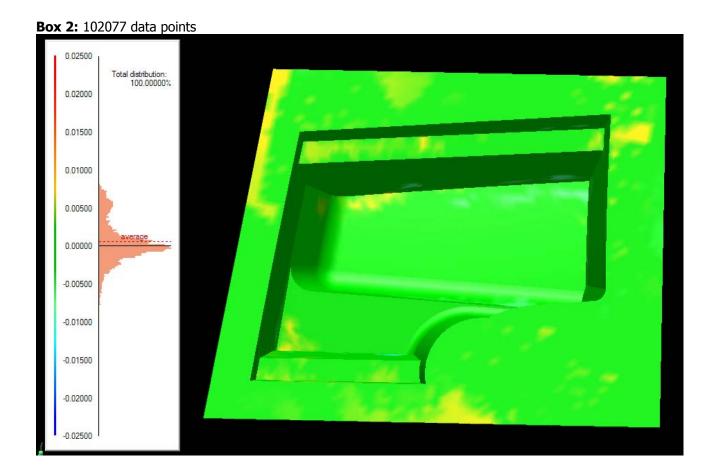
The patterns are machined using precision CNC mills. The accuracy achieved on these patterns is at least an order of magnitude better then that observed on the casting. The patterns all came in with an RMS residual error under 0.0050" except core box 6, which was the largest RMS value at 0.0052". Each pattern was scanned using a photogrammetry session, each session has an overall RMS residual error. This means we are confident in the data of each session to this value. Here are the results of each photogrammetry session.

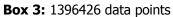
Core Box	Overall RMS residual error(mm)
1	0.0299
2	0.0425
3	0.117
4	0.0593
5	0.0744
6	0.132
7	0.0642
8	0.0647
9	0.0743
10	0.0793
cope	0.113
drag	0.106
polodial	0.0303

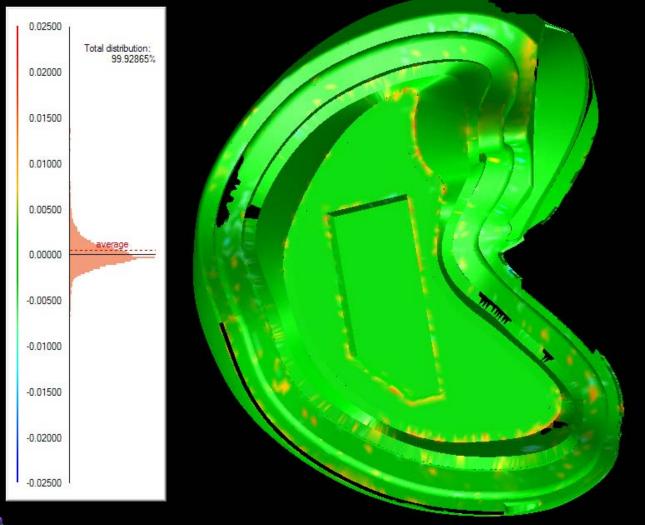
The color maps below show the deviations of scan data when compared to CAD. These are the same color maps as were in the original inspection reports. Shown here is also the histogram report, which shows how much of the data resides within each deviation band. For example 100% of the 428,125 points scanned for box 1 are within 0.025" and the majority are within 0.005".



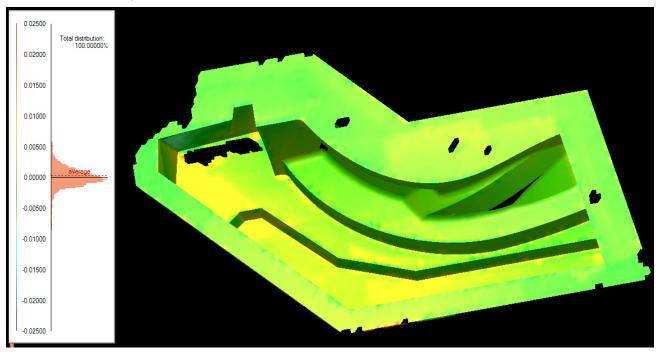
**Box 1:** 458125 data points



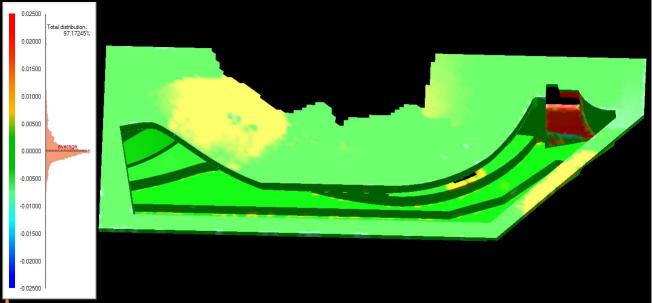




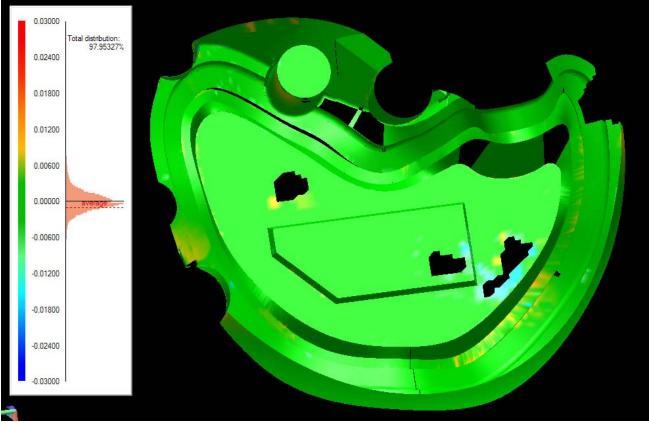
Box 4: 382140 data points



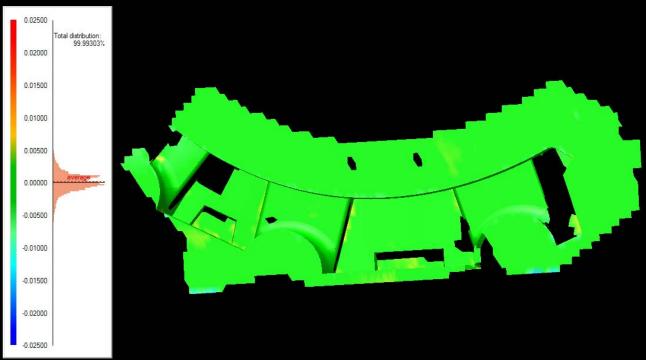
### Box 5: 685973 data points



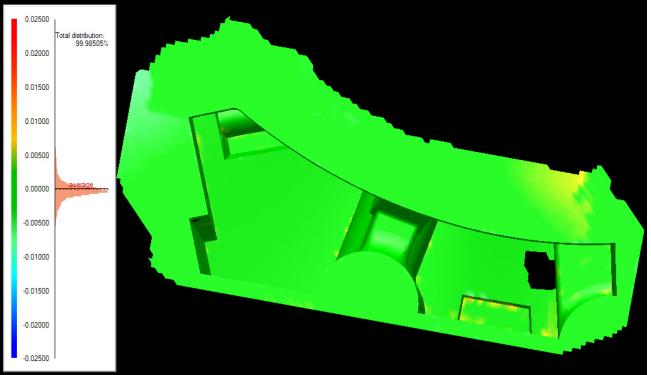


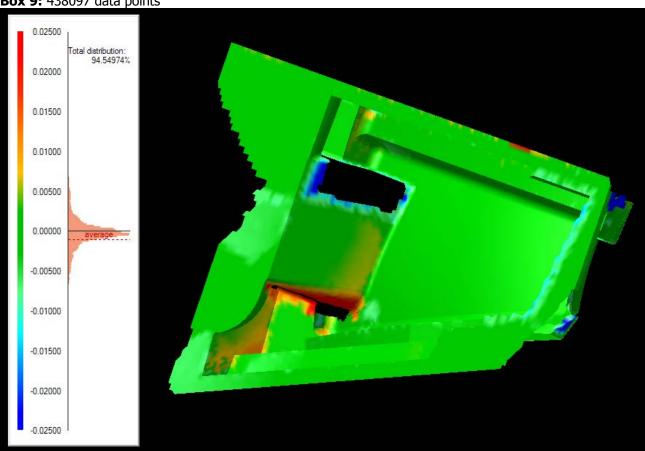


### **Box 7:** 573572 data points

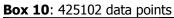


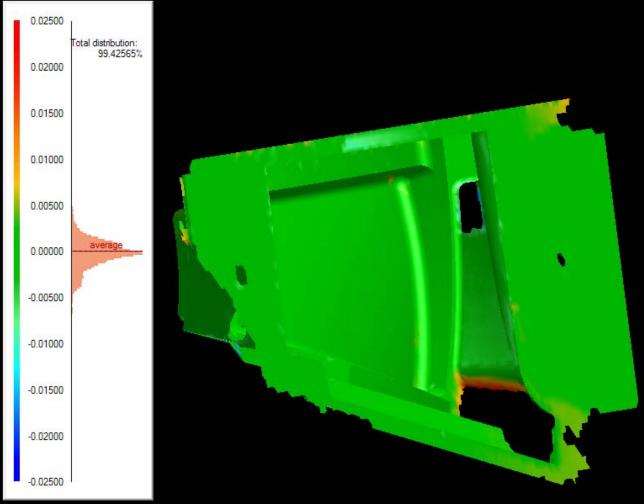
### Box 8: 668847 data points

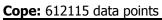


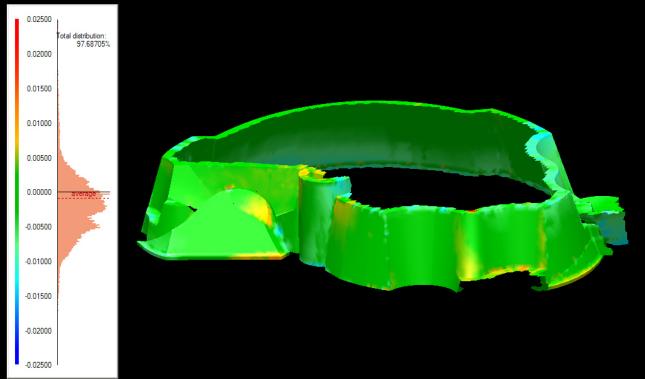


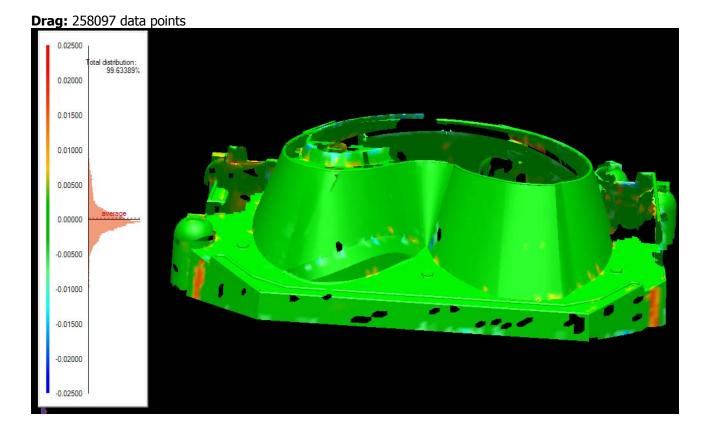
### Box 9: 438097 data points



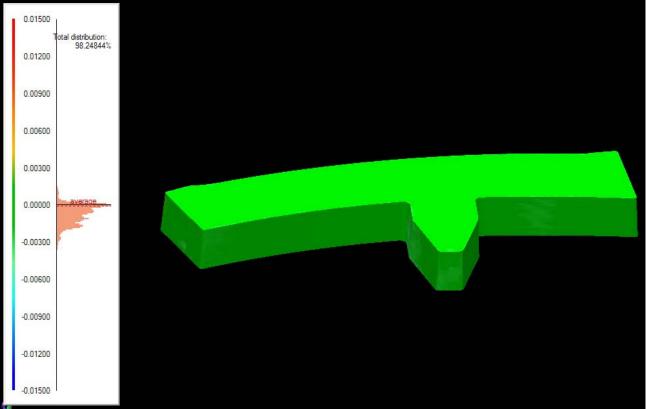


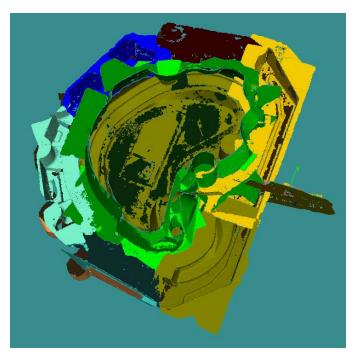


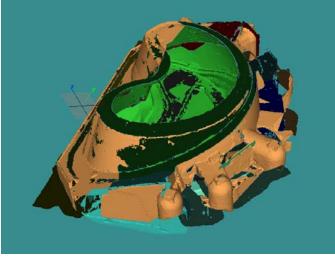


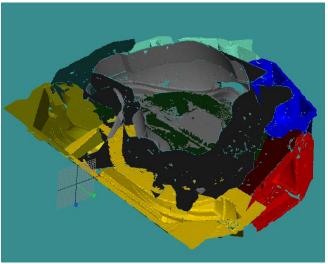


#### Polodial: 998922 data points









#### **Disclaimer:**

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#### Stocked A model 1.503 1.501

#### Evaluation of stocked A model for adequate stock

#### Notes:

- 1. Measurements shown are through-wall thickness measurements of the stocked A model (no shrink) created by Lawton Patterns.
- 2. Measurements taken along wall where the A-1 casting is exhibiting thin wall conditions ranging down to 1.18"
- 3. Software used to verify wall thickness of model Solid View/Pro 2003.1
- 4. Measurements taken on 8/2/05 by Roy Sheppard of EIO

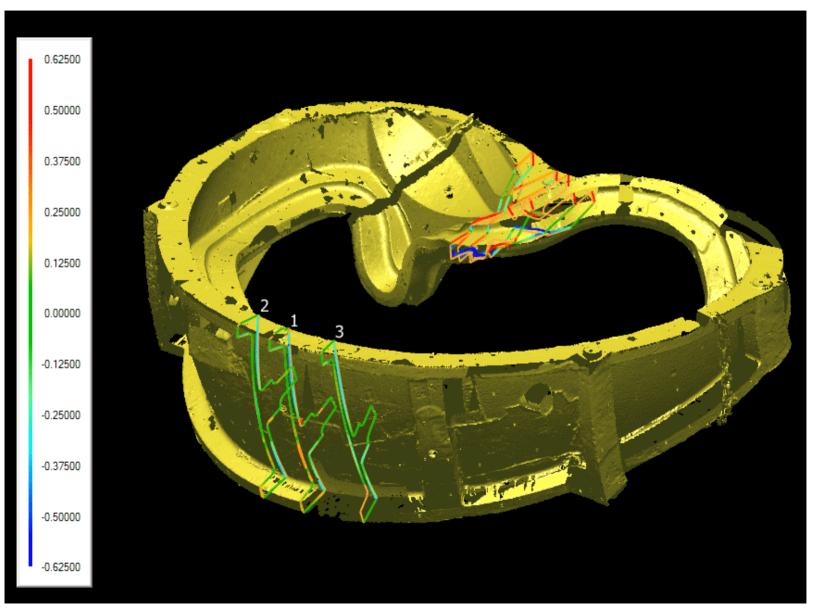
## **Energy Industries of Ohio**

A-Coil Winding Form Metrology Discussion – Pattern Verification

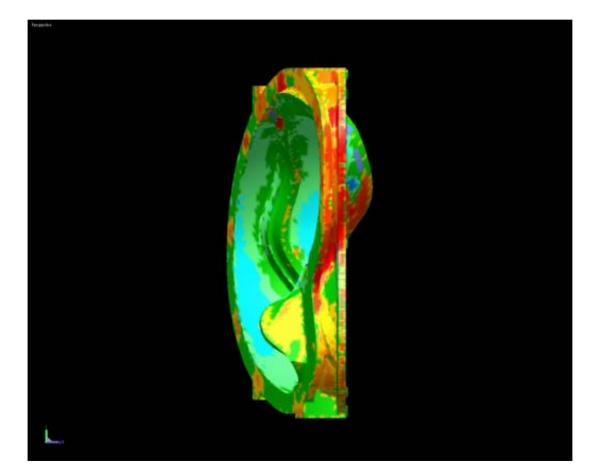
## Issues

- Dimensional data supports a under tolerance condition exists on an area of the shell
  - Limited options on increasing thickness on A1
- 3D Scanco data correlates to physical measurements taken by MetalTek on the A1
  - MetalTek dimension taken from shell at cut-thru
- Dimensional data supports that the A-B alignment will be achieved at the flanges, but may not align shells (no interference issues)
  - Root cause not confirmed
- Dimensional changes to A1 part are all long time period changes and involve extensive work to part and matching work on pattern equipment
  - Quickest path forward may be FEA and Waiver

#### Location of 3 cross sections



## Left View



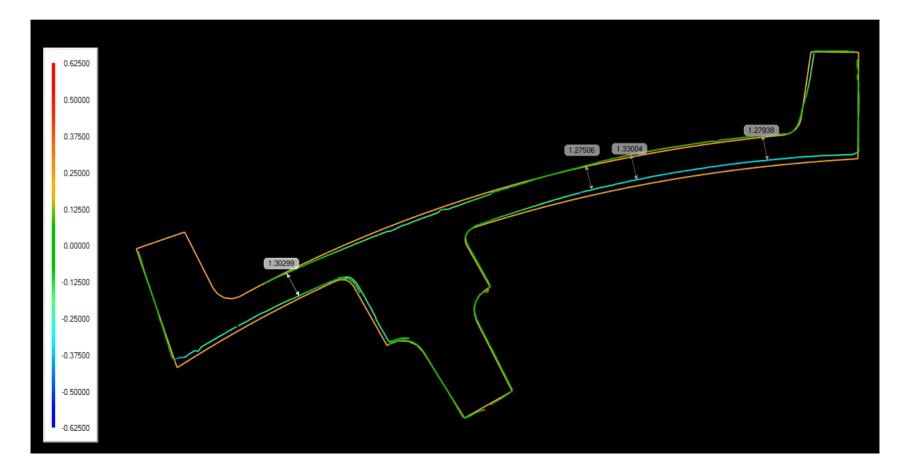
## **Right View**



#### **Cross Section 1**



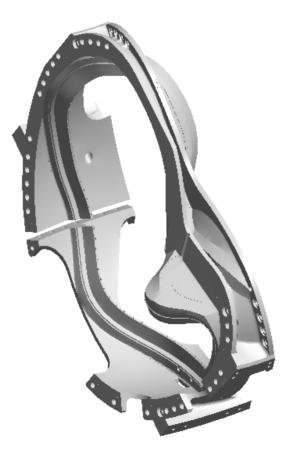
## Cross section 2



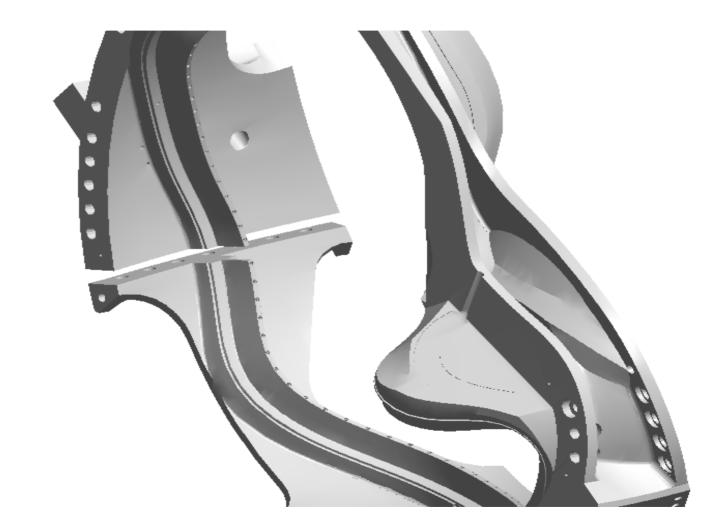
## **Cross Section 3**



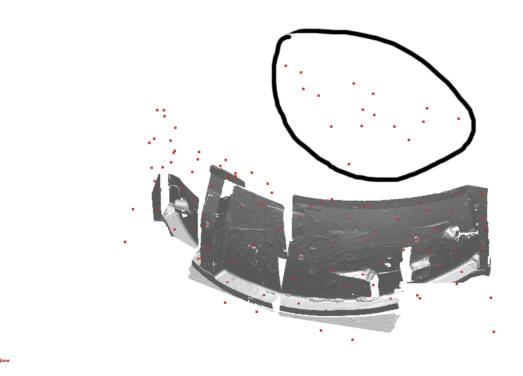
#### Machined Coil A



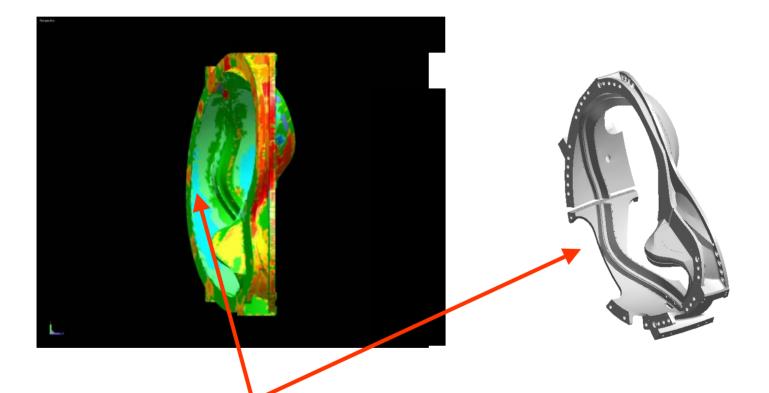
## Back wall after machining



#### Additional points snagged for orientation

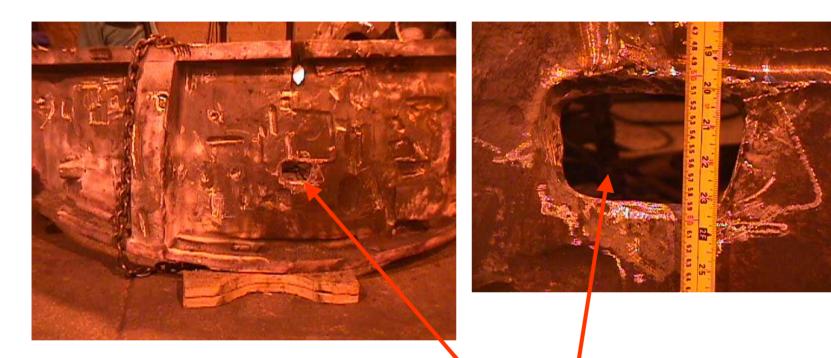


## Comparison of Machined Part to 3DScanco Layout



Views are slightly rotated. Use racetrack reference

## **MetalTek Verification**



Excised hole for dimensional verification (1.24-1.27")

# Summary of Layout

- A substantial amount of the wall appears to be under the design thickness
- 3DScanco data is at 95% Confidence Level (Approx. 0.018" error per 3DS)
- MetalTek verified one area with direct measurements
- Remediation options are limited and have risk

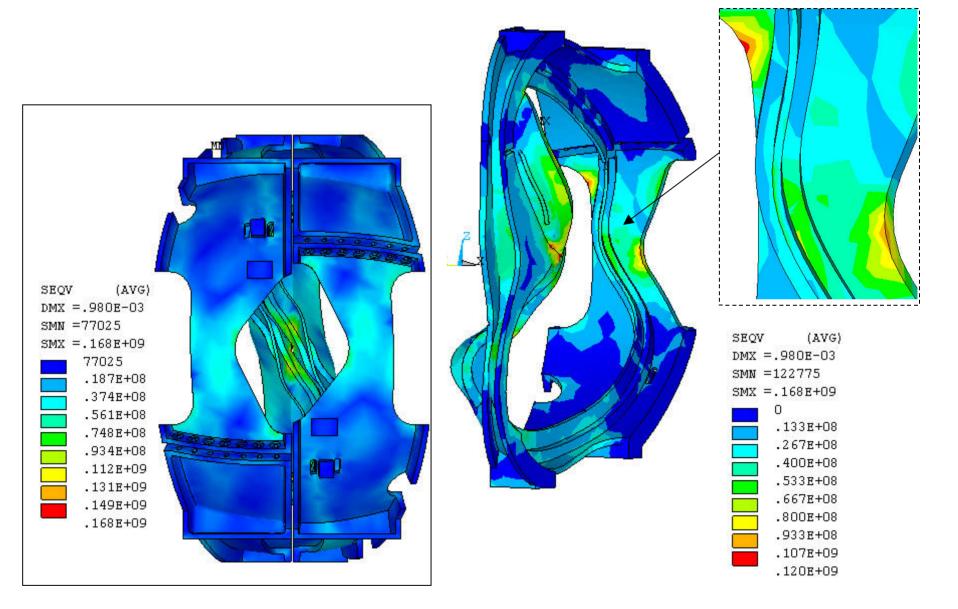
# **Remediation Options**

- Option 1 Permanent Waiver
  - PPPL would need to assess part dimensions and FEA and assure that thin wall will not impact performance
  - Affects all A-coils
- Option 2 Use-As-Is NCR
  - Would move A1 forward, but at risk of continued dimensional learning and schedule
  - Affects A1
- Option 3 Weld Build Up
  - Would have to optimize part and identify areas for build up. Substantial shape risk on component. Large schedule impact.
- Option 4 Remake
  - Would have schedule slip on both pattern and component in schedule.
     Would likely complete C coils and have production gap in program while B pattern completes and A is adapted.

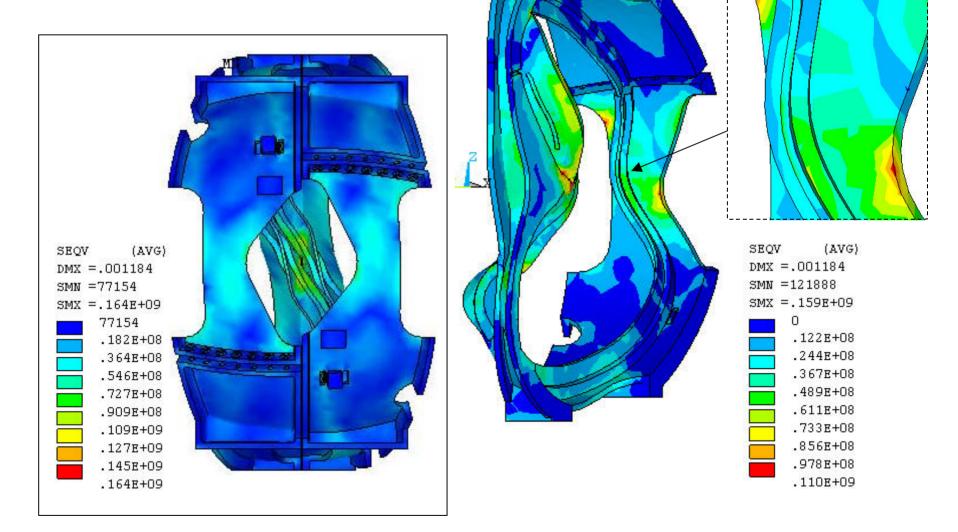
# Request

- Energy Industries of Ohio Team requests that PPPL analyze this and respond with preferred direction to move forward
  - MetalTek can offer additional laser scanning for verification of shape/dimension
  - Lawton has offered transfer measurement as a means for direct measurement of thickness, MetalTek has experience using similar technique
  - Component is on process hold pending resolution.
     Time is of the essence.

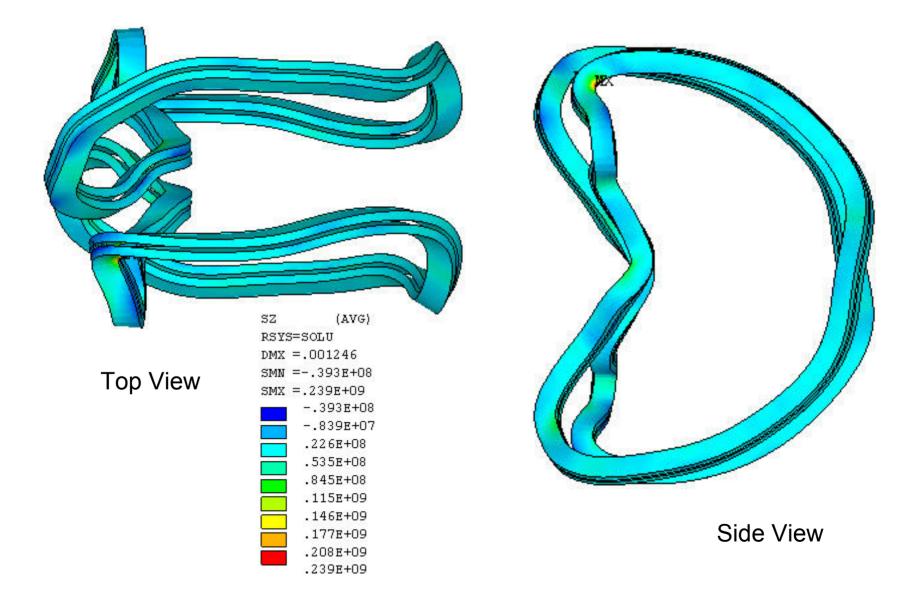
## Stresses in Shell A1 for E=193 GPa



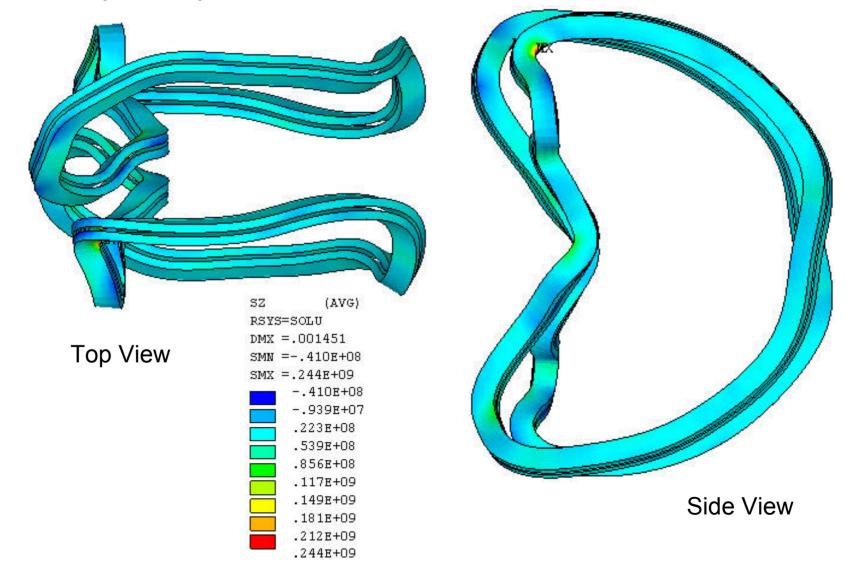
# Stresses in Shell A1 for E(A)=152 GPa and E(B&C)=193 GPa



### Stresses in Shell A1 for E=193 GPa



# Stresses in Shell A1 for E(A)=152 GPa and E(B&C)=193 GPa

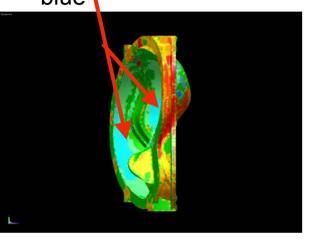


## FEA Analyses Results of the A1 Casting with Thin Wall Regions

August 8, 2005

## Thin Wall Areas in the A1 Casting

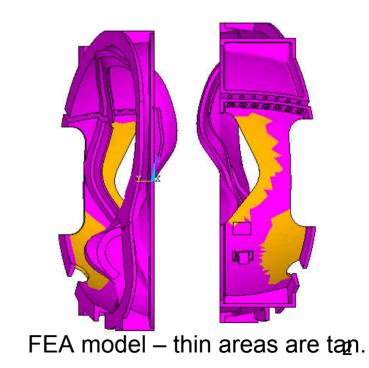
thin areas In light blue





Machined Casting

Note That Much Of the Thin Area is Machined Away, Lessening its Effect



## SCANCO data well quantifies the actual wall thicknesses

Specified thickness is 1.375" +0.25 / -0.00

Thinnest actual section is 1.18".

"Guesstimate" is the thin area is 15% of the wall area.



### FEA Studies for the Shell A Thin Wall Region:

- Run #1: Baseline Engineering Analysis used E for 316 SS. The E=193 GPa was based on data for 316 stainless steel as an interim value until E for cast "Stellalloy" was determined.
- Run #5: Analysis Corrected for the E of "Stellalloy". All shells having E=145 GPa, the value given by the specification for "Stellalloy".
- Run #6: This model reflects the updated E and also thin shell regions in A1 with wall thicknesses t=1.18". The E of shell A is modified by a thickness ratio of 1.18/1.375. The E of shell A become 124 GPa. (Note: In the FEA model, the affect of the thin wall is achieved by modifying the effective modulus, E, rather than actually changing the wall thickness in the model )
- Run #4: This model uses a corrected E and models All Type A Castings as Having A Thin Region Like A1 but 1.05" thick. E of shell is 145 GPa except in the shell A thin wall regions, where E=111 GPa

The Analyses Show That The Thin Region With Either Thickness Has a Very Minimal affect!

The slides which follow show that this is by far the most significant affect!

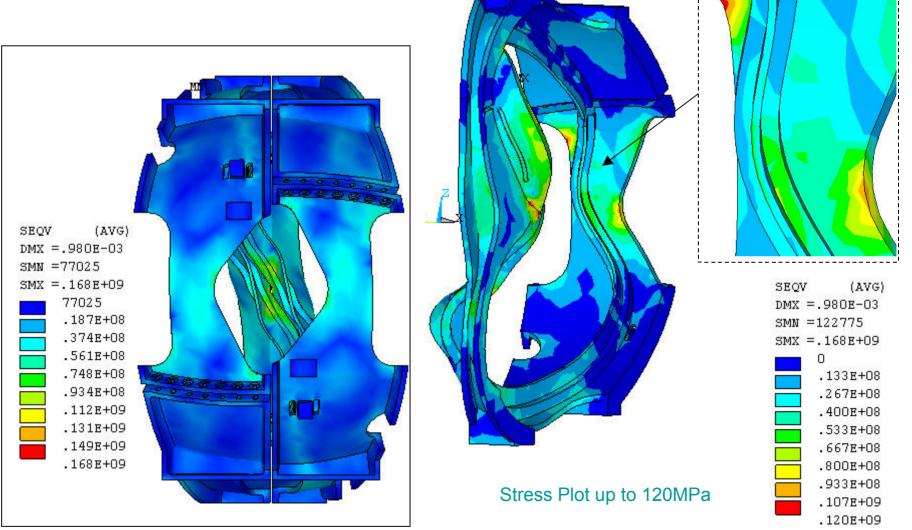
### The Stress Allowable Based on the Spec. Minimum

Property at 77 K									
Property	Required	C-1 Casting Heat 27728 (averages)	LNM 4455 Electrode						
Elastic	21 Msi	23.3	27.1						
Modulus E	(144.8 Gpa)								
0.2% Yield	72 ksi	98.4	126.3						
Strength	(496.4 Mpa)	124							
Tensile	95 ksi	170.2	187.7						
Strength	(655 Mpa)	170.2							
Elongation	32%	55%	33%						
		58.7%							
Charpy V –	35 ft. lbs.	78	51						
notch Energy	(47.4 J)								

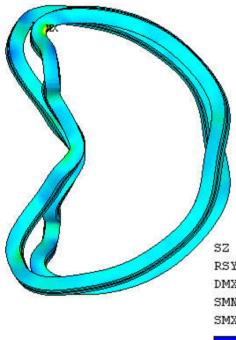
•The allowable is the lesser of  $\frac{1}{2}$  tensile strength or 2/3 yield.

•Using the spec minimum, this would be 322.5 MPa. (the lesser of 322.5 or 327.6)

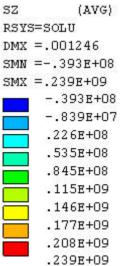
## **The Baseline Analysis:** Stresses in Shell Type A (Run 1) - E=193 GPa

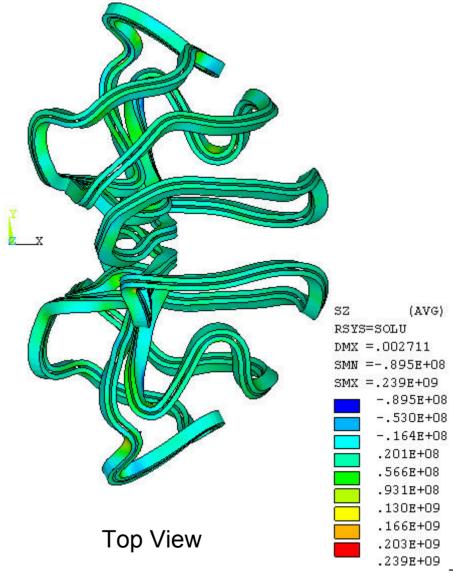


#### Baseline: Axial Stresses in Modular Coils for Run No. 1 - E=193 GPa



#### Coil Type A





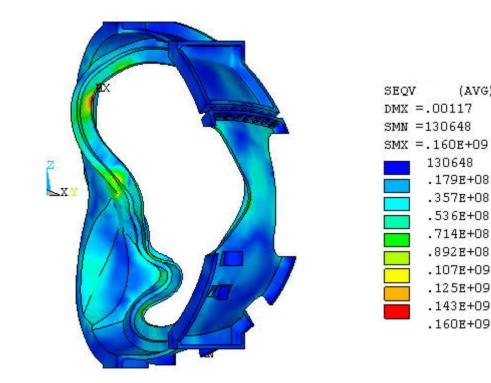
## Analysis Results with the E Updated for "Stellalloy"

(AVG)

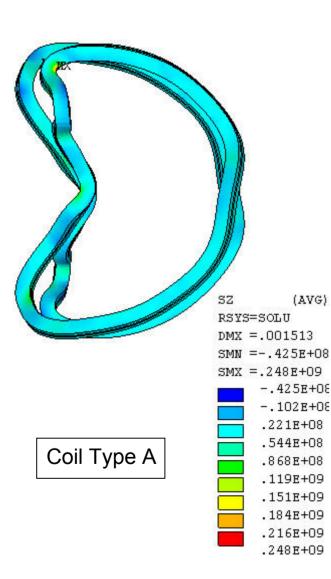
.179E+08 .357E+08 .536E+08 .714E+08 .892E+08 .107E+09 .125E+09 .143E+09 .160E+09

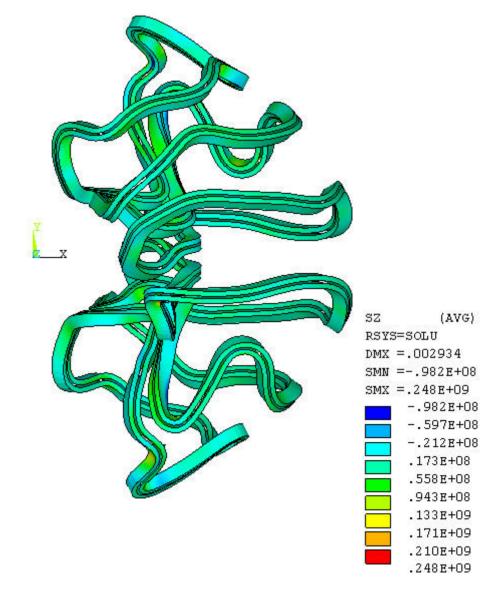
Stresses in Shell Type A for Run No. 5

- E=145 GPa



# E Updated for "Stellalloy" Axial Stresses in Modular Coils for Run No. 5 - E=145 GPa

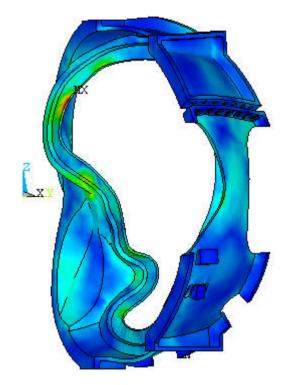




### This model reflects the updated E and also thin shell regions in A1 with wall thicknesses t=1.18". Stresses in Shell

Type A for Run No. 6

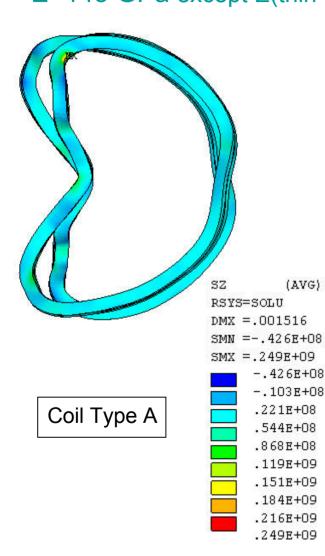
- E=145 GPa except E(thin wall region)=124 GPa

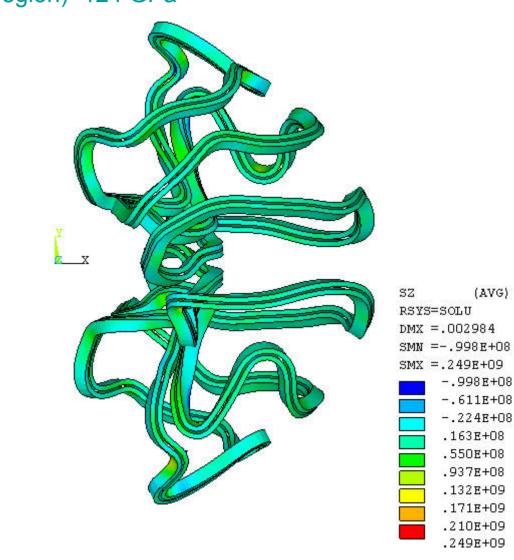


SEQ	/ (AVG)
DMX	=.001169
SMN	=131056
SMX	=.161E+09
	131056
	.180E+08
	.358E+08
	.536E+08
	.715E+08
	.893E+08
-	.107E+09
	.125E+09
	.143E+09
	.161E+O9

# This model reflects the updated E and also thin shell regions in A1 with wall thicknesses t=1.18". Axial Stresses in Modular Coils for Run No. 6

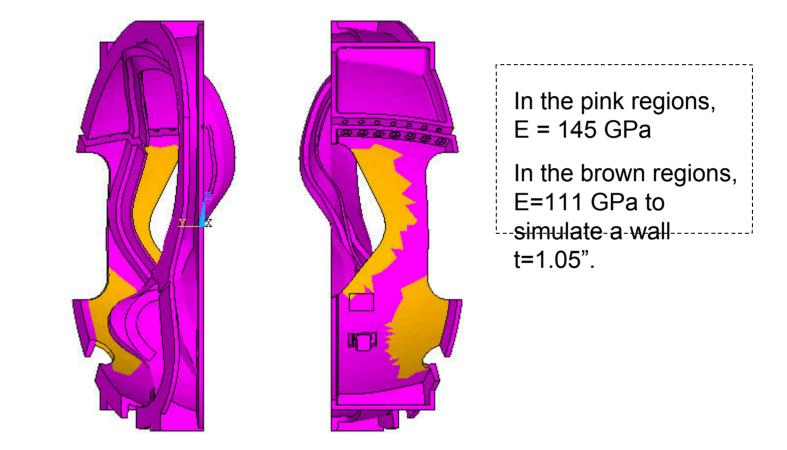
- E=145 GPa except E(thin wall region)=124 GPa





#### This model uses a corrected E and models All Type A Castings as Having A Thin Region Like A1 but t=1.05"

Modulus of Elasticity in Shell Type A for Run No. 4,

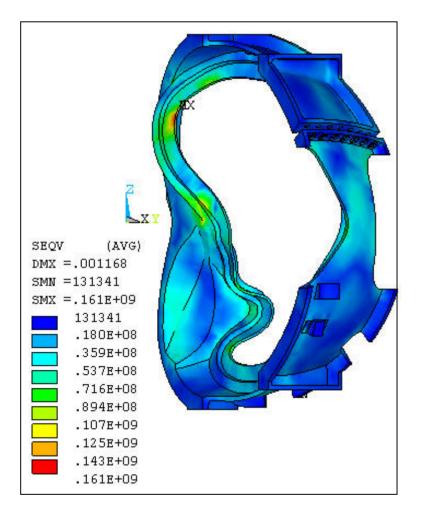


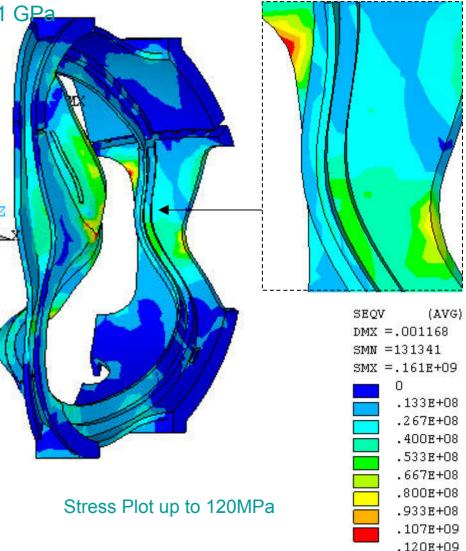
**Right View** 

#### This model uses a corrected E and models All Type A Castings as Having A Thin Region Like A1 but t=1.05"

Stresses in Shell Type A for Run No. 4

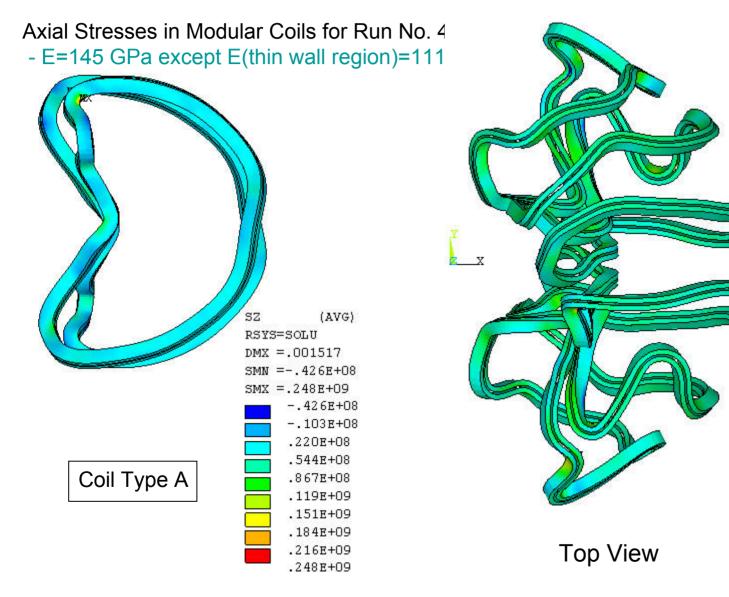
- E=145 GPa except E(thin wall region)=111 GPa





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#### This model uses a corrected E and models All Type A Castings as Having A Thin Region Like A1 but t=1.05"



SZ (AVG) RSYS=SOLU DMX =.002971 SMN =-.982E+08 SMX =.248E+09 -.982E+08 -.596E+08 -.211E+08 .174E+08 .559E+08 .944E+08 .133E+09 .171E+09 .210E+09 .248E+09 14

### Summary:

• As the table below shows the most significant effect is the updating of the modulus E to that of the "Stellalloy".

• Thin shell areas like that of A1 has an extremely minor affect on the stresses and displacements in ANY of the coils or shells with the thickness being either 1.18" as for A1 or even with the thickness being 1.05" which MTK projects is the minimum if the shell is not changed. Reasons:

a) The shape of the tee is not changed by this, and the tee provides most of of the bending stiffness

b) Some EM forces are transferred to the shell B from the wing.

c) The thin wall region is not the location for the peak stress and much of the area will be machined away.

		Shell Type A		<u>Coil Type A</u>		All Coils	
		Max.	Max.	Max.	Max.	Max.	Max.
		Displacement -	Stress -	<b>Displacement -</b>	Stress -	Displacement -	Stress -
<u>Run #</u>	<b>Configuration</b>	mm	Мра	mm	Мра	mm	Мра
1	Baseline	0.98	168	1.246	239	2.711	239
5	Updated E	1.17	160	1.513	248	2.934	248
6	Updated E; thin sect. =1.18"	1.169	161	1.516	249	2.984	249
4	Updated E; thin sect. =1.05"	1.168	161	1.517	248	2.971	248

# Consequently...

- Since the thin section of A1 has virtually no affect on stresses or deflections of either the coil or shell, the NCR for A1 with the thin region having a minimum thickness of 1.18" will be dispositioned to "Accept As Is".
- Pending the root cause analysis and EIO's recommendation, if necessary, based on these analyses, we have the flexibility to allow the wall thickness IN AN AREA SIMILAR TO A1 for all future Type A Castings to be a minimum of 1.050" and a maximum of 1.375 +0.250 =1.625" (which is the same as the upper limit currently specified).