

Status of ARIES Compact Stellarator Reactor Parameters

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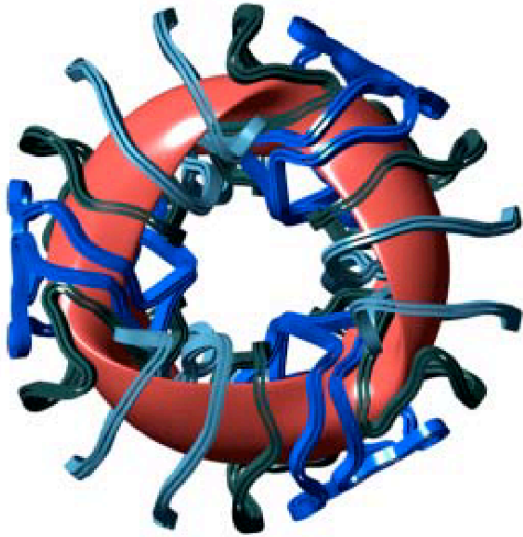
Stellarator Theory Teleconference

Feb. 5, 2004

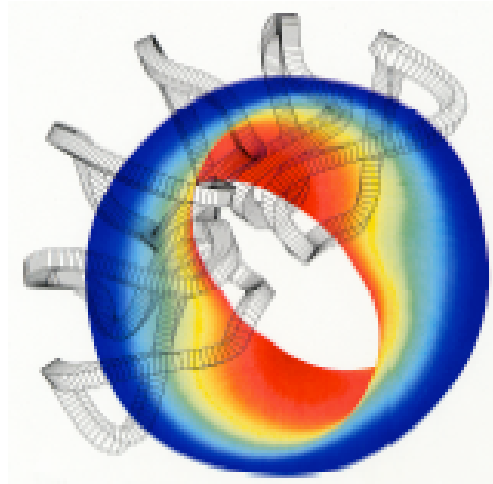
Topics

- **Plasma and coil characterization**
- **Optimization assumptions, calculations**
- **NCSX-R, MHH2-R and QPS-r cases**
- **Choices**

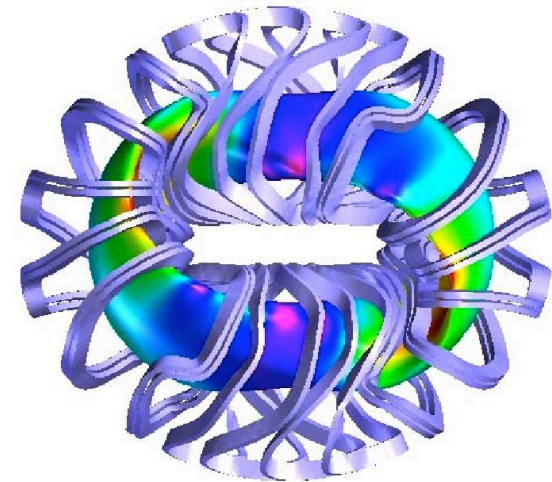
Possible Reactor Configurations



- **NCSX-R**
quasi-axisymmetric
18 modular coils
 $\langle \kappa \rangle_{ave} = 0.5$, $\langle \eta \rangle = 0.6$



- **MHH2-R**
quasi-axisymmetric
16 modular coils
 $\langle \kappa \rangle_{ave} = 0.45$, $\langle \eta \rangle = -0.22$



- **QPS-r**
quasi-poloidal
20 modular coils
 $\langle \kappa \rangle_{ave} = 0.3$, $\langle \eta \rangle = 0.28$

- **Except for MHH2-R, these configurations have been optimized for an experiment and *not* for a reactor!**

Configuration Characterization

	NCSX-R	MHH2-R	QPS-r
Plasma-coil aspect ratio $A_{\square} = \langle R \rangle / \square_{\min}$	5.90	5.52	6.08
Min. coil-coil aspect ratio $A_{c-c} = \langle R \rangle / (c-c)_{\min}$	10.1	13.3	10.1
B_0/B_{\max} for $R = 6.5$ m, $d = 0.3$ m, $k = 1$	0.49	0.43	0.45
Plasma aspect ratio $A_p = \langle R \rangle / \langle a \rangle$	4.50	3.75	2.74
\square -particle loss (%)	30	30	25
$\langle \square_{\text{limit}} \rangle$ (%): infinite- n to finite- n modes	4.1 to 6	4 to 5?	2.5 to >5

Reactor Parameter Selection

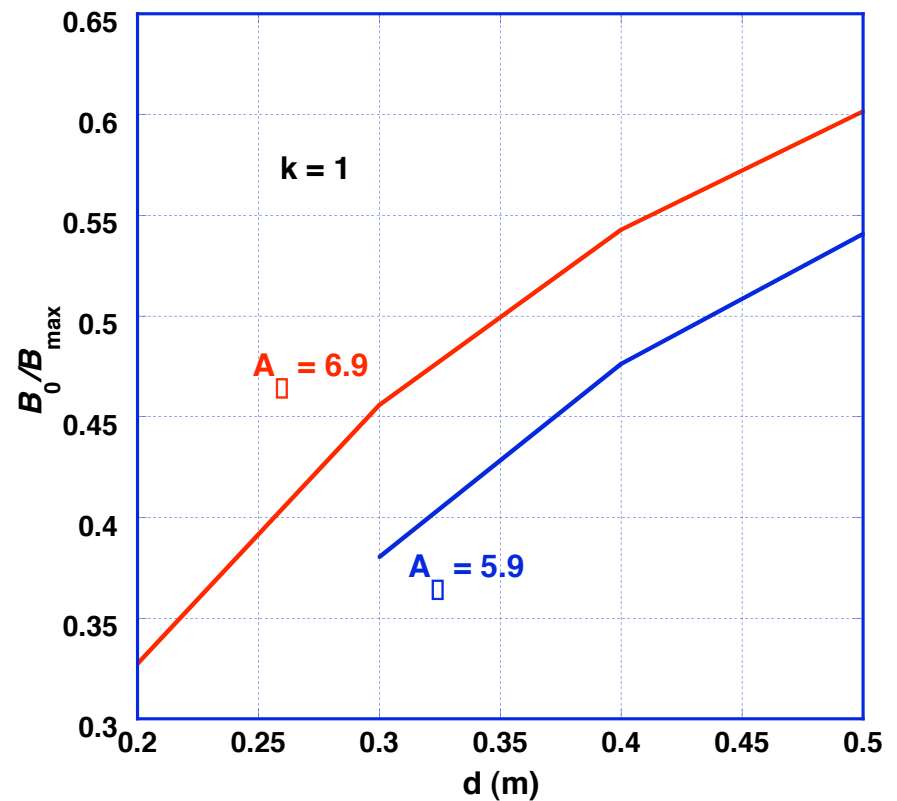
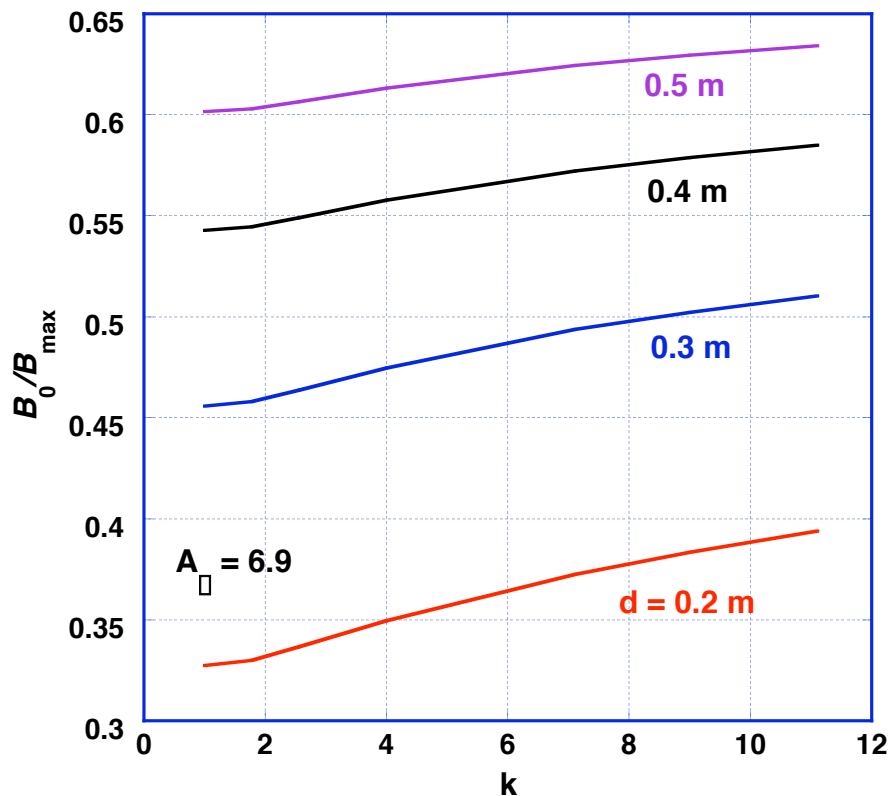
- **Minimize reactor core cost**
 - Cost ~ blanket/shield + coils + vacuum vessel
 - Cost ~ surface areas, approx. $\sim R^2$
- **Minimize R for a reactor -- small d , large k**
 - $\langle R \rangle \geq A_{\square} (t_{so+fw+sh+cc} + d/2k^{1/2})$
 - Min. coil-coil dist. $R/A_{c-c} - k^{1/2}d - 2(csth) \geq 0$
 - * $A_{\square} = \langle R \rangle / \square_{min}$, $d = (cw \times cd)^{1/2}$, $k = cw/cd$
 - * $t_{so+fw+sh+cc} = 0.95 + 0.0624 \ln(p_{n,wall}/2)$, **$csth = 1 \text{ cm}$**
- **Maximize B_0 (minimizes \square)**
 - $B_0(T) = 16 B_0/B_{coil,max}(d,k) / (R/8.25)$ (for NCSX-R)

Check if Need to Increase R

- If $\eta > \eta_{\text{limit}}$: ($P_E \sim \eta^2 B_0^4 R^3$)
- If $j_{\text{coil}}(\text{MA/m}^2) = 13(B_0/5.3)(R/8.25)/d^2 > 330$
(or $>110-135$ for Nb_3Sn)
- Increase R by increasing d (increases B_0 & reduces k) but need to keep $B_{\text{coil,max}} < 16 \text{ T}$
 - $B_{\text{max}} = (R/8.25)B_0 / \{B_0/B_{\text{coil,max}}(d,k)\}$

Maximum B_0 Determination

- $B_0(\text{T}) = 16 B_0/B_{\max}(\text{d},\text{k}) / (R/8.25)$
- $B_0/B_{\max}(\text{d},\text{k})$ from Ku (2/25/03 NCSX coil set)
- Normalize to $B_0/B_{\max}(\text{d} = 0.3 \text{ m}, \text{k} = 1)$ for each coil case and interpolate between d,k values



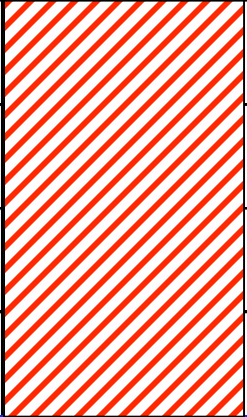
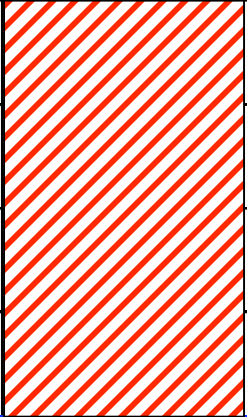
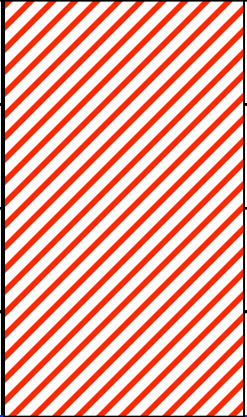
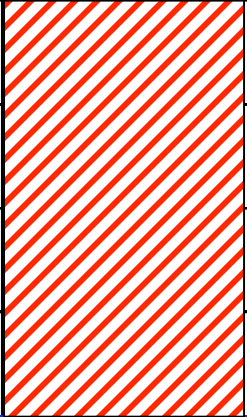
Physics Constraints

- **Beta limit**
 - Nominally set by linear infinite- n ballooning limit
 - However, limits for finite- n ballooning and external kink or vertical modes are more realistic
 - Use equilibrium beta limit instead?
- **Confinement multiplier H-ISS95**
 - H-ISS95 values up to 2.5 obtained in experiments
 - No deterioration seen at highest β values in experiments
 - Quasi-symmetry aiding rotation should help, so reasonable to assume H-ISS95 up to ~ 4 ?
- **Alpha particle losses: 10% loss vs 30% loss**
 - Small effect on parameters: $\beta = 5\% \rightarrow 4.4\%$, 16 T \rightarrow 15 T
 - *But*, factor of 3 reduction in high-energy flux to divertor
 - * reduces blistering (a problem?)

NCSX-R Parameter Selection

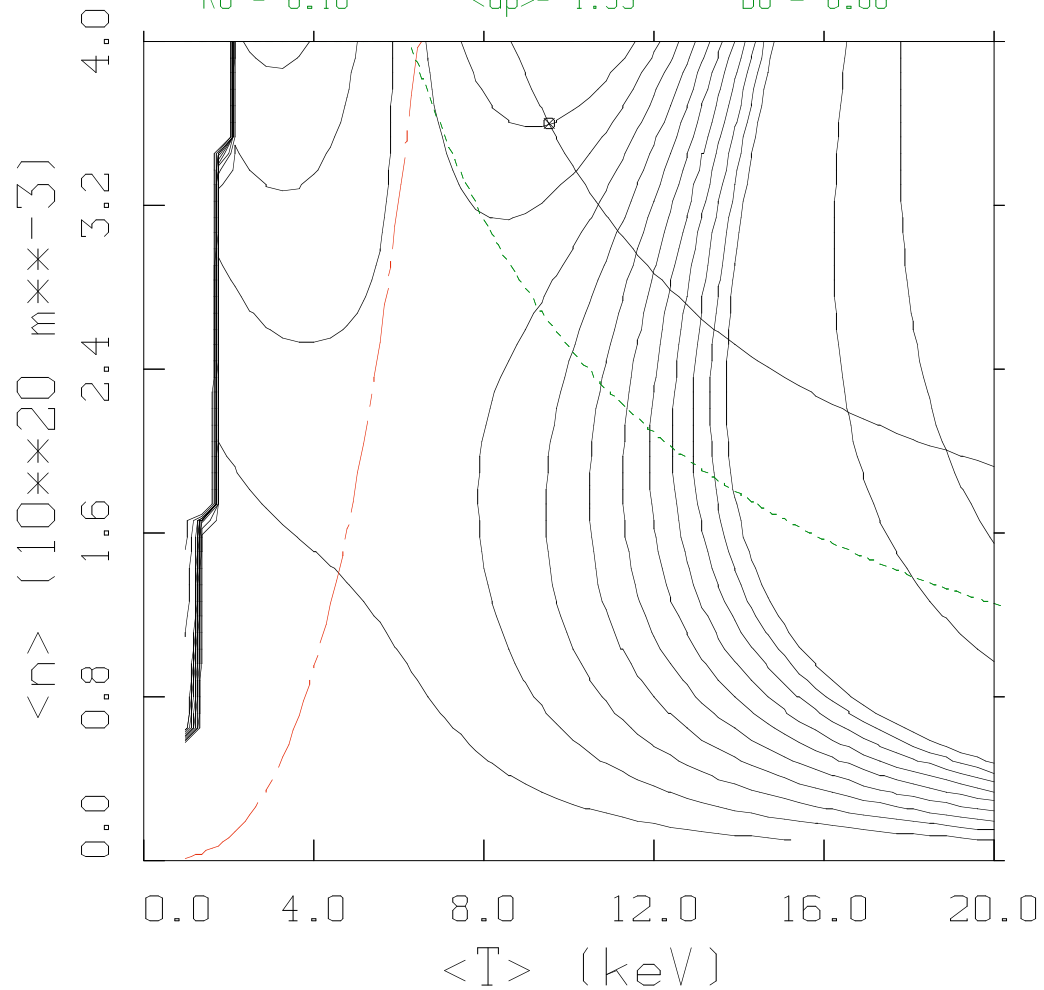
Coil d	Coil k	R axis (m)	Max B axis j (MA/m ²)	c-c min	Wall load	Beta (%)	
0.2 m	1.00	6.39	5.18	252.87	0.41	4.27	9.04
	1.78	6.26	5.32	254.83	0.33	4.44	8.81
	2.56	6.19	5.49	260.05	0.27	4.54	8.42
	4.00	6.12	5.54	259.43	0.19	4.64	8.41
	7.11	6.06	6.21	287.83	0.05	4.74	6.80
	8.41	6.04	6.35	293.59	0.00	4.76	6.52
	9.00	6.04	6.42	296.23	-0.02	4.77	6.41
0.227 m	6.84	6.09	6.89	249.07	-0.01	4.69	5.48
0.25 m	1.00	6.53	6.44	205.55	0.38	4.09	5.67
	1.78	6.36	6.65	206.96	0.28	4.31	5.52
	2.56	6.28	6.85	210.36	0.20	4.42	5.31
	4.00	6.19	7.16	216.95	0.09	4.54	4.95
	5.53	6.14	7.40	222.55	0.00	4.61	4.69
	7.11	6.11	7.64	228.57	-0.08	4.66	4.43
0.275 m	4.77	6.19	7.87	197.23	-0.01	4.54	4.09
0.3 m	1.00	6.66	7.59	171.64	0.34	3.93	3.96
	1.78	6.46	7.86	172.45	0.22	4.18	3.86
	2.56	6.36	8.08	174.60	0.13	4.31	3.74
	4.00	6.26	8.40	178.75	0.00	4.44	3.54
	7.11	6.16	8.88	186.01	-0.21	4.59	3.24
0.4 m	1.00	6.92	9.14	120.88	0.27	3.64	2.57
	1.78	6.66	9.53	121.23	0.11	3.93	2.51
	2.47	6.53	9.79	122.22	0.00	4.08	2.45
	2.56	6.53	9.81	122.31	-0.01	4.09	2.44

Configuration Comparisons

	NCSX-R	MHH2-R	QPS-r
Average major radius (m)	6.09		6.38
Average magnetic field on axis (T)	6.89		5.65
Volume-average beta (%)	5.50		4.67
ISS-95 confinement multiplier	3.50		3.65

An NCSX-R Reference Case

Case= 329 ISS-95= 3.50 Paper= 2000.0
<n>op= 3.60 <T>op= 9.55 betaop= 5.50
Pfmin= 1493.1 betamin= 4.79 Psp= 0.12
<n>sp= 2.28 <T>sp= 6.32 Pfsp= 356.8
He%= 6.69 %DT = 80.36 Zeff= 1.50
R0 = 6.10 <op>= 1.35 B0 = 6.88



Choices

- **Beta limit = 4%, 5%, 6%? Use equilibrium limit instead of linear infinite- n ballooning**
- **Maximum H-ISS95 = 4 typically ~3.5**
- **B_{\max} on coils = 16 T**
lower B_{\max} is an option at larger R
- **1 cm coil side case thickness**
- **High-T superconductor, Nb₃Sn, NbTi**
- **Impurity radiation to reduce power to divertor**
- **Divertor geometry -- affects everything!**

Summary

- **Improved reactor parameters for 2 cases**
 - **Ku's NCSX coil configuration**
 - Garabedian's MHH2 configuration
- **Facts in hand to choose a case for *exploring engineering issues* but *not* a final candidate**