

I-8

# Local Island Divertor Experiments on LHD

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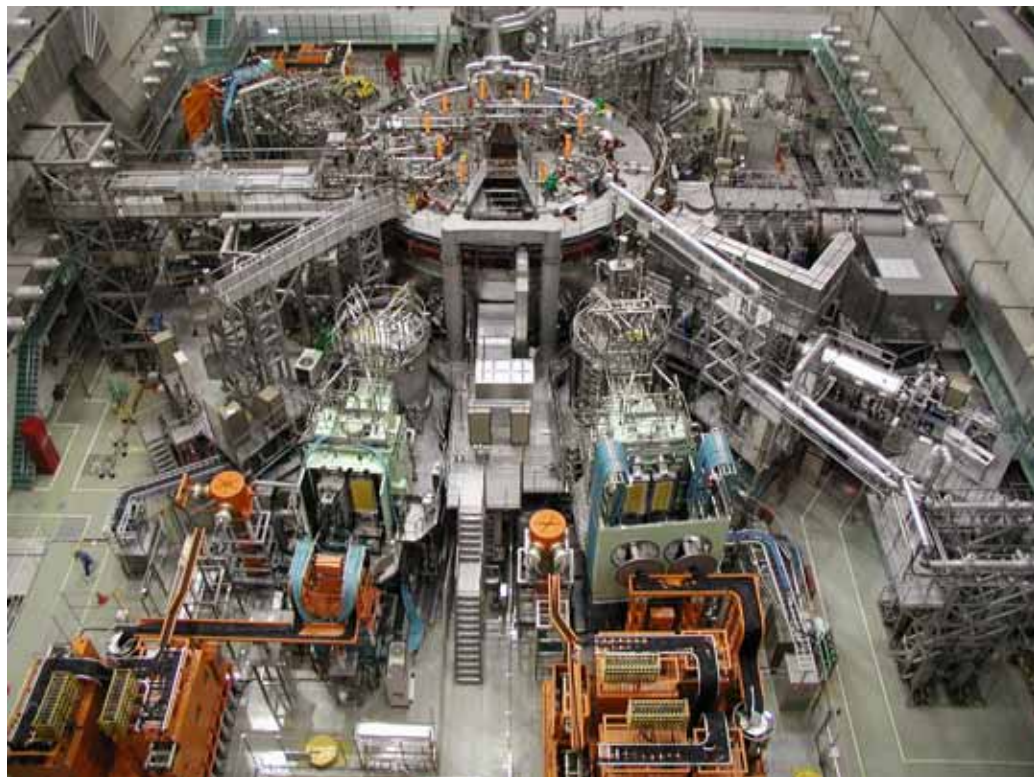
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- (1) Introductions to LHD.
- (2) LHD Divertor Strategy.
- (3) LID Experiments.
  - 3-1) proof of the LID principle.
  - 3-2) modeling.
  - 3-2) impurity control.
  - 3-2) confinement properties.
- (4) Summary.

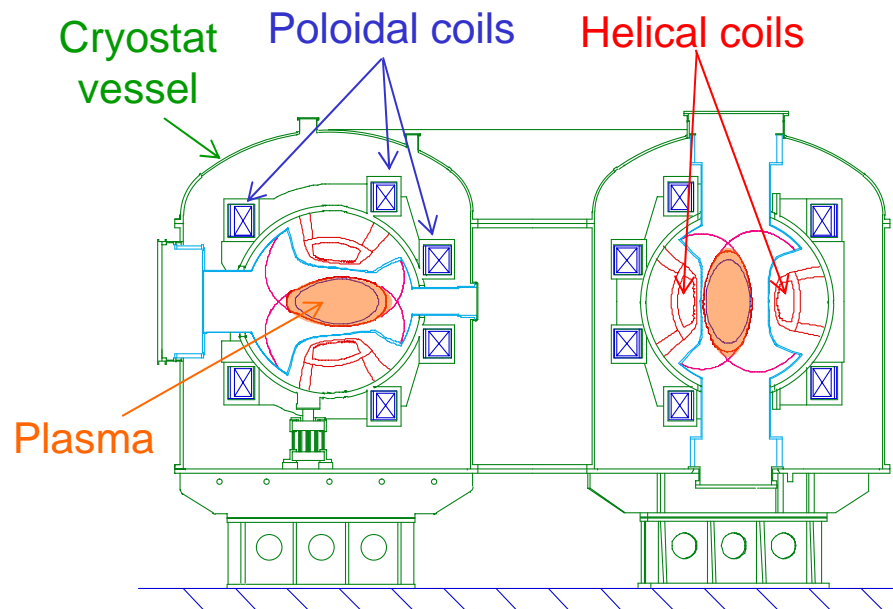


Large Helical Device

# LHD (Large Helical System)

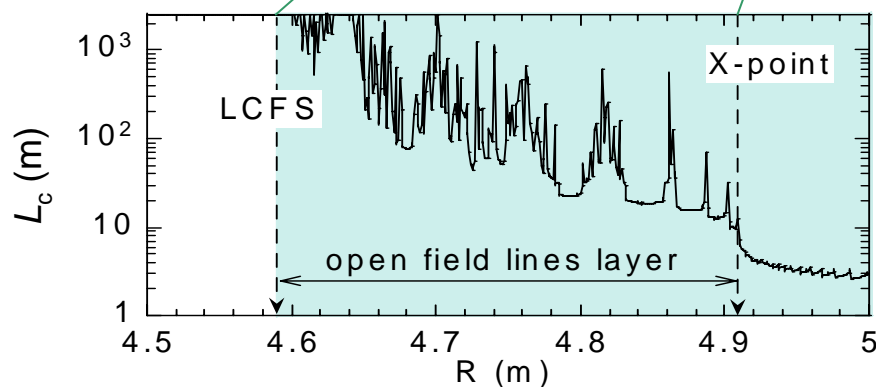
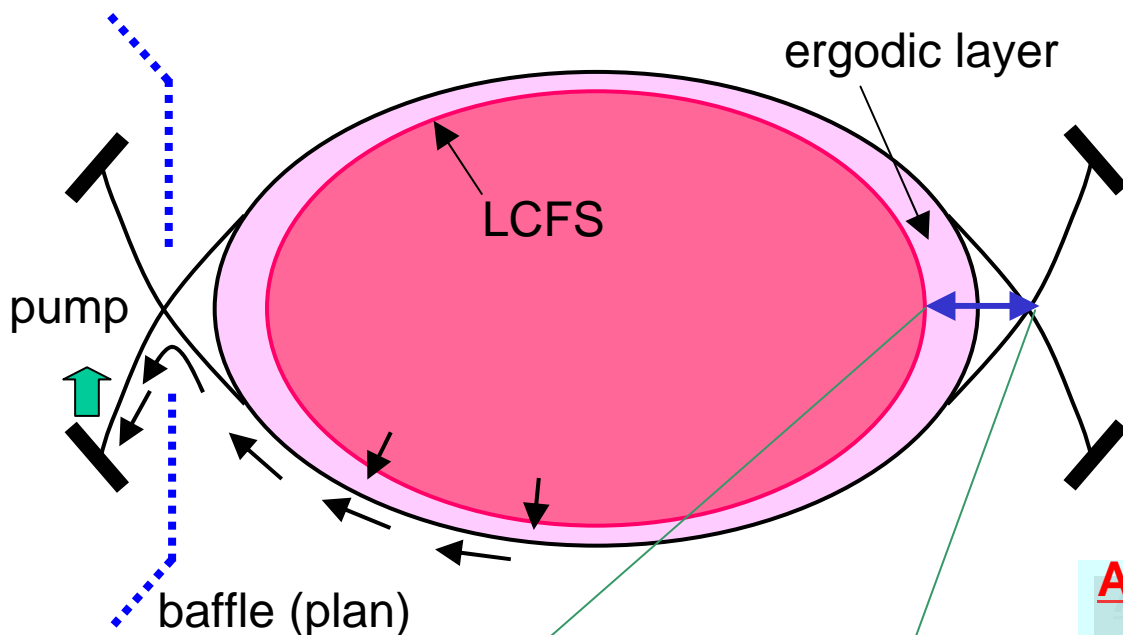


May 14, 2004



Plasma Major radius	3.5 - 4.0 m
Plasma Minor radius	~ 0.6 m (average)
Plasma Volume	~ 30 m <sup>3</sup>
Coil minor radius	0.975 m
Magnetic field	2.893 T (at R <sub>ax</sub> =3.6m)
Heating power	
ECH	1.2 MW
N-NBI	10 MW
ICRF	3.0 MW

# Helical Divertor (HD)



## Feature

### Intrinsic double-null type divertor

- \* long legs.
- \* short field lines (2-3m in LHD).

### Nonaxisymmetric magnetic field

- \* 3-d structure.

### Ergodic layer surrounding core

- \* thick (~ 30cm in LHD).
- \* no clear separatrix.
- \* long  $L_c$  (several 100m in LHD).

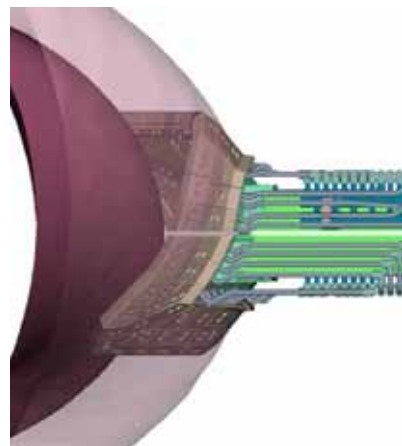
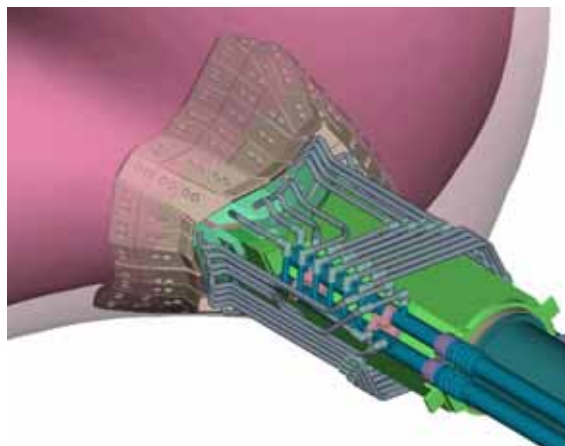
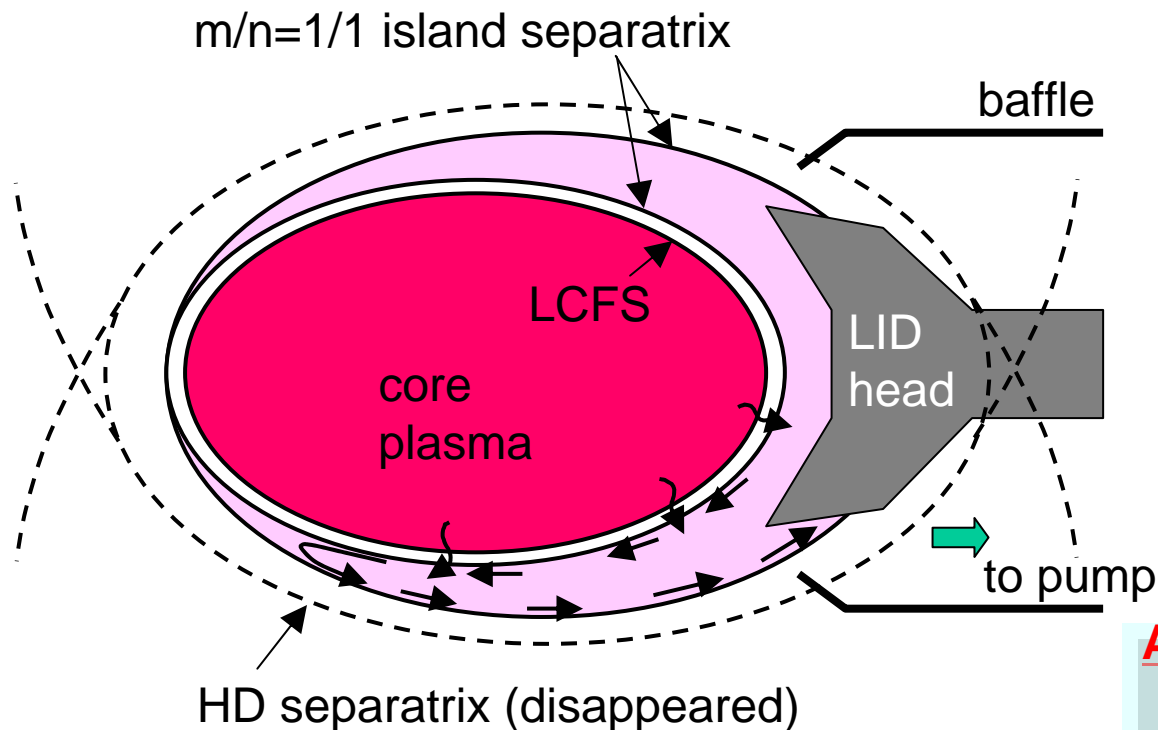
## Advantage

- \* relatively wide wetted area.  
--> favorable for heat removal.
- \* long distance from target to core.  
--> favorable for impurity screening.

## Disadvantage

- \* complicated.  
--> inadequate for diagnostics, blanket.
- \* difficult to construct (3D).  
--> high cost.

# Local Island Divertor (LID)



## Features

- \* Utilize  $m/n=1/1$  island.
- \* Insert a divertor head locally.
- \* LCFS defined by island separatrix.
- \* No leading edge problem.
- \* Closed system.
- \* High efficient pumping.
- \* No ergodic layer.
- \*  $L_c \sim 250m$ .

## Advantage

- \* high efficient pumping.
- \* easy to realize closed system.
  - > superior cost performance.
- \* compact and integrated
  - > favorable for blanket, diagnostics.

## Disadvantage

- \* small wetted area.
  - > high heat load.



# LHD Divertor strategy

Active edge control by LID.



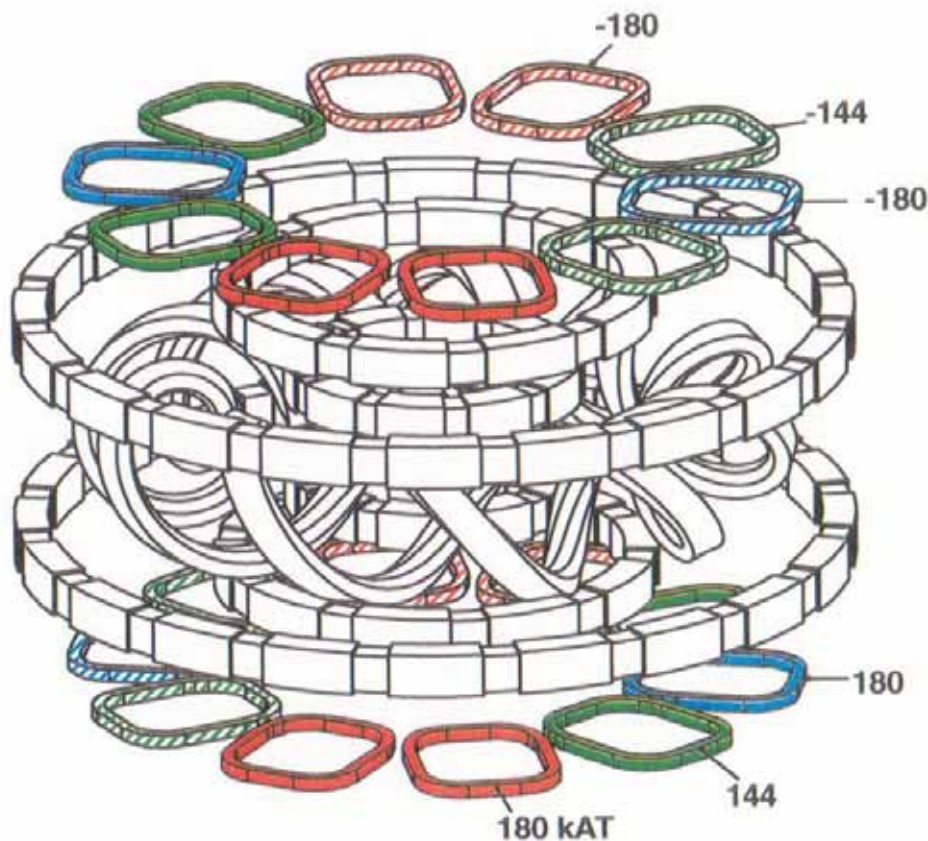
Steep  $T_e$  and  $n_e$  gradient.



**Confinement improvement.**

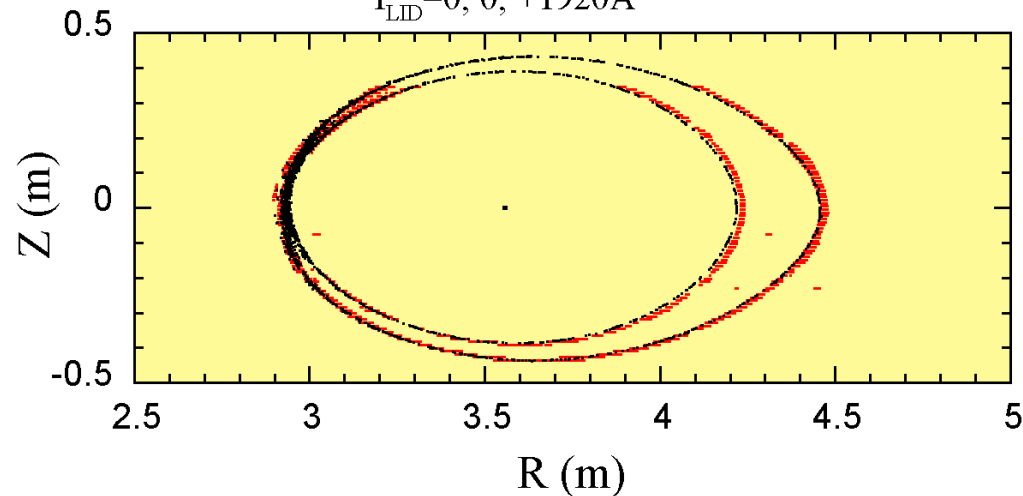


# Perturbation coils



$$R_{ax}=3.6\text{m}, B_q=100\%, \gamma=1.254, B_t=2.75\text{T}$$

$$I_{LID}=0, 0, +1920\text{A}$$

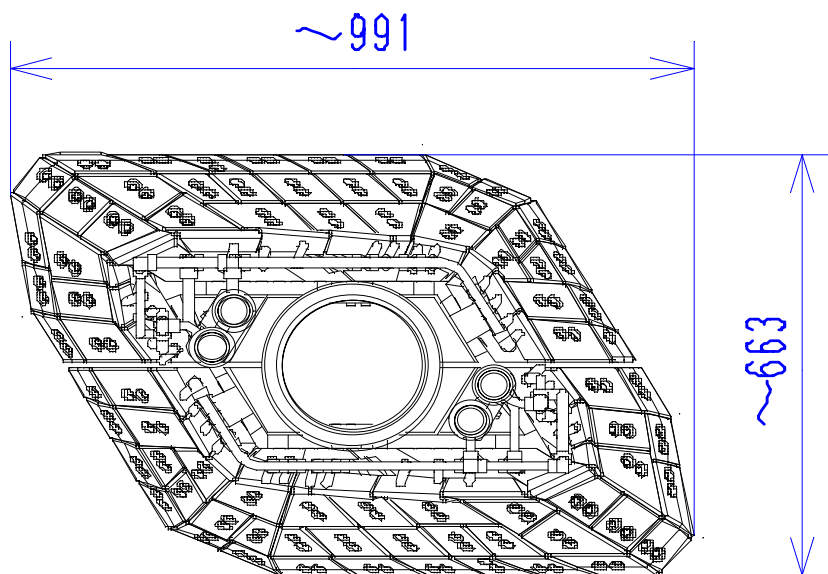


## m/n = 1/1 island

- \* surely exists as expected (calculation).
- \* confirmed by flux surface mapping with electron beam and probe.

**10 pairs of normal conductor coils**  
for m/n=1/1 island generation

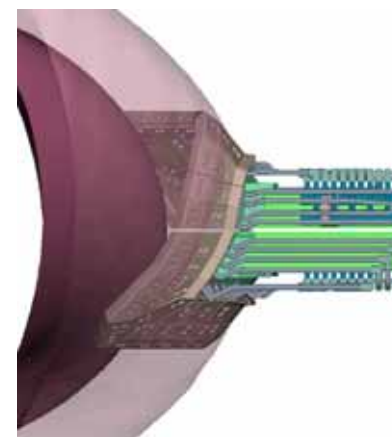
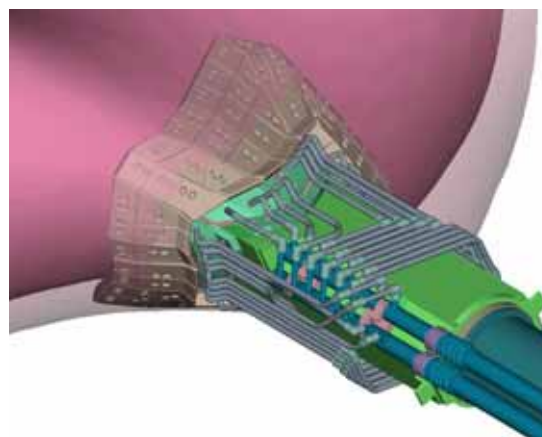
# Divertor head



## Divertor head

water cooled heat sink (stainless steel)  
covered with carbon tiles.

$P < 7.5 \text{ MW/m}^2$  (5s).

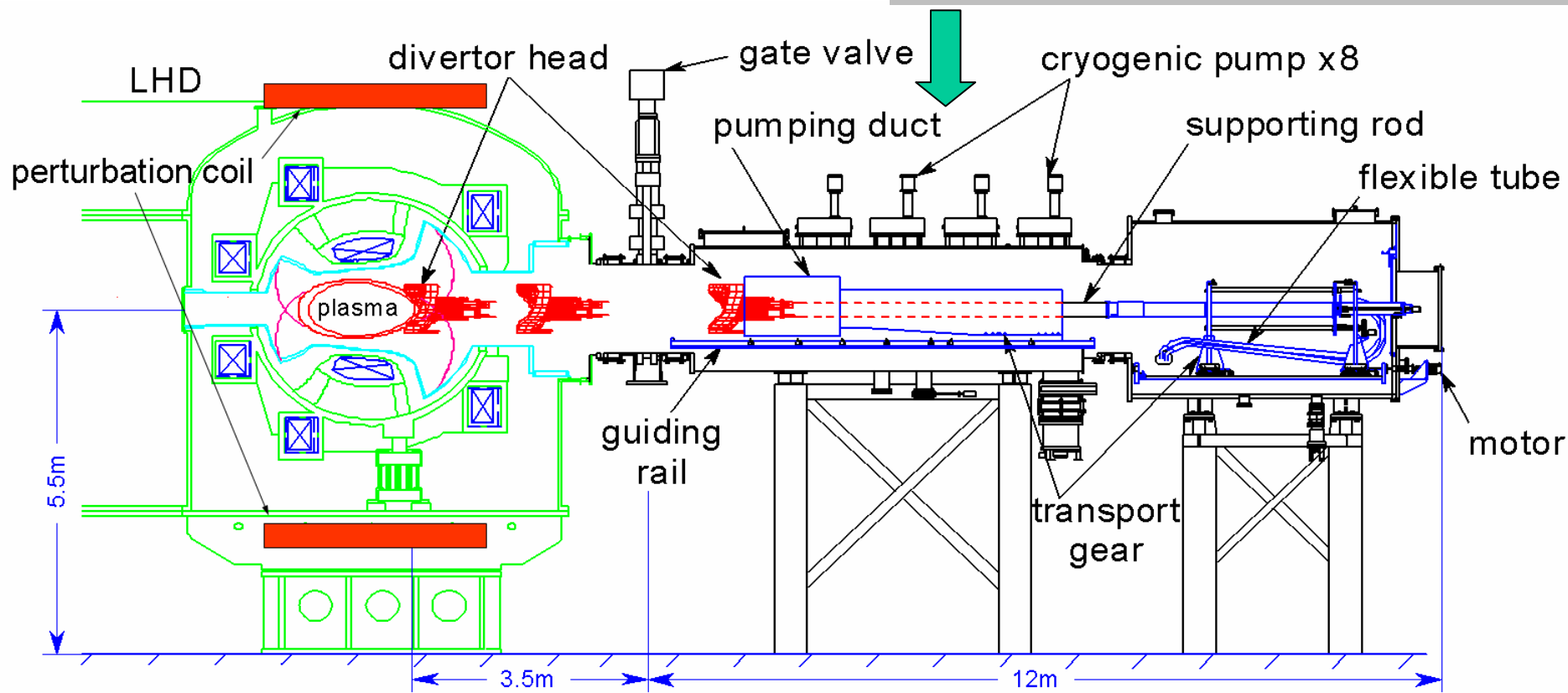


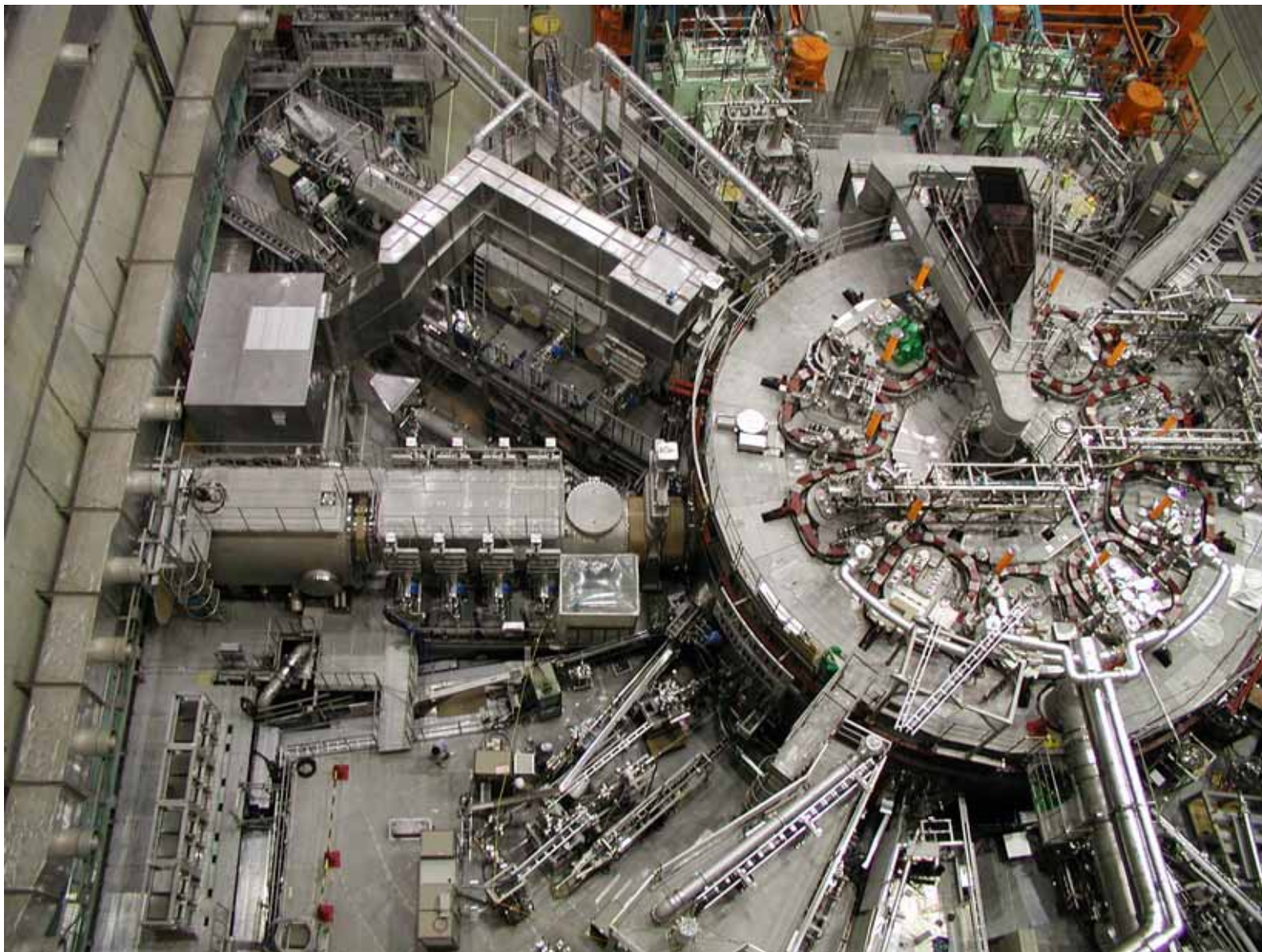


# Schematic of LID system

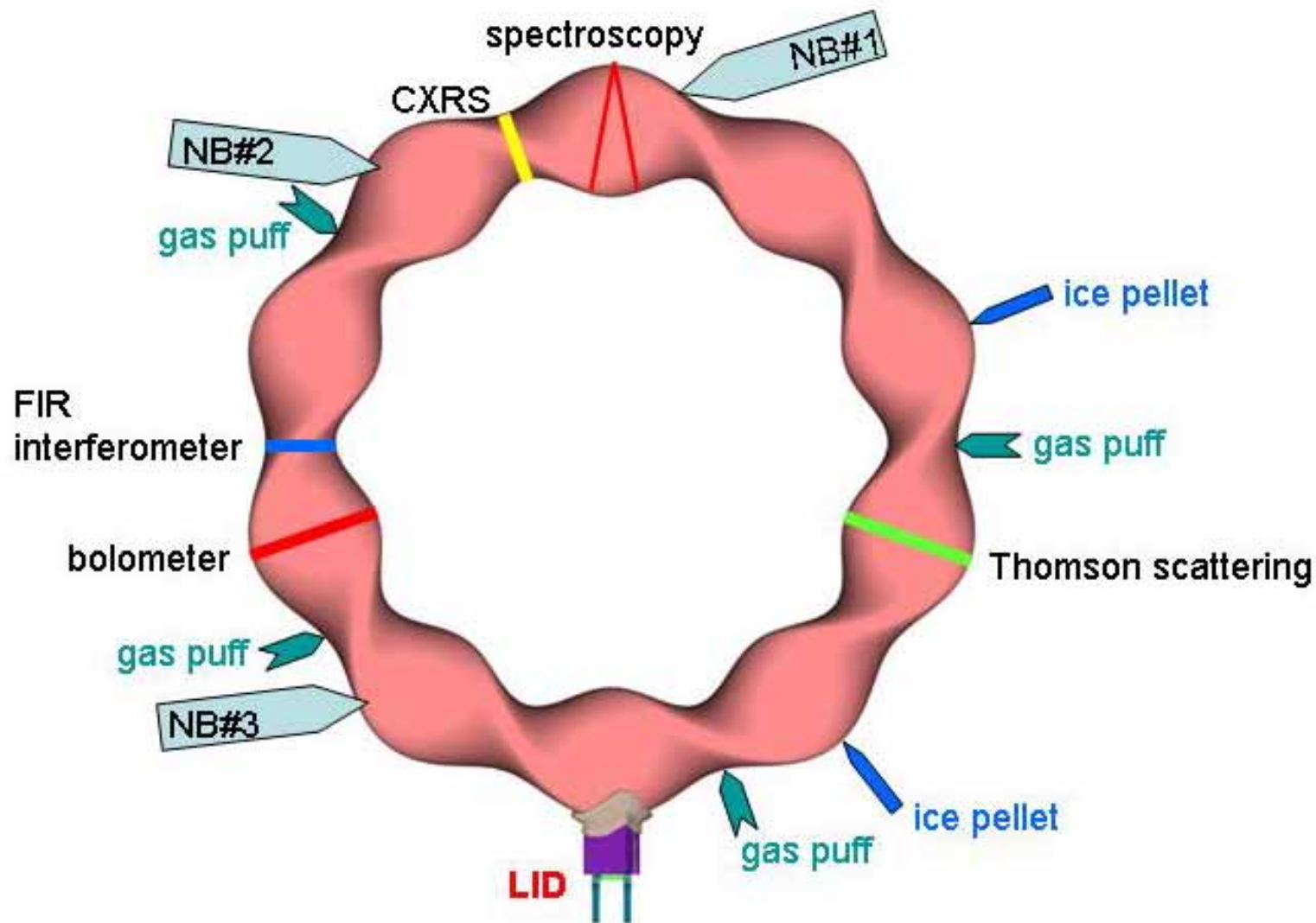
## Pumping system

- \* 8 cryogenic pumps (42m<sup>3</sup>/s each).
- \* effective pumping speed ~ 100m<sup>3</sup>/s.

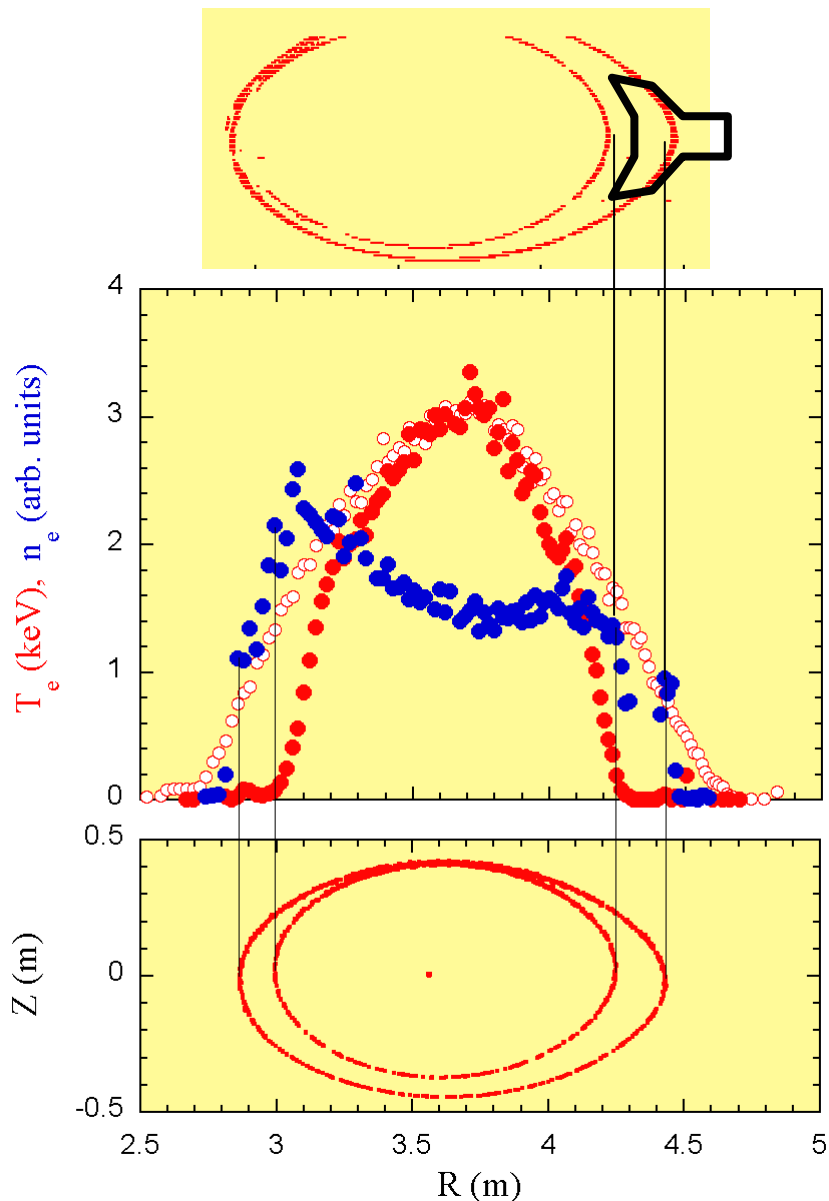




# Experimental setup



## $T_e$ profile and separatrix position



### In LID configuration,

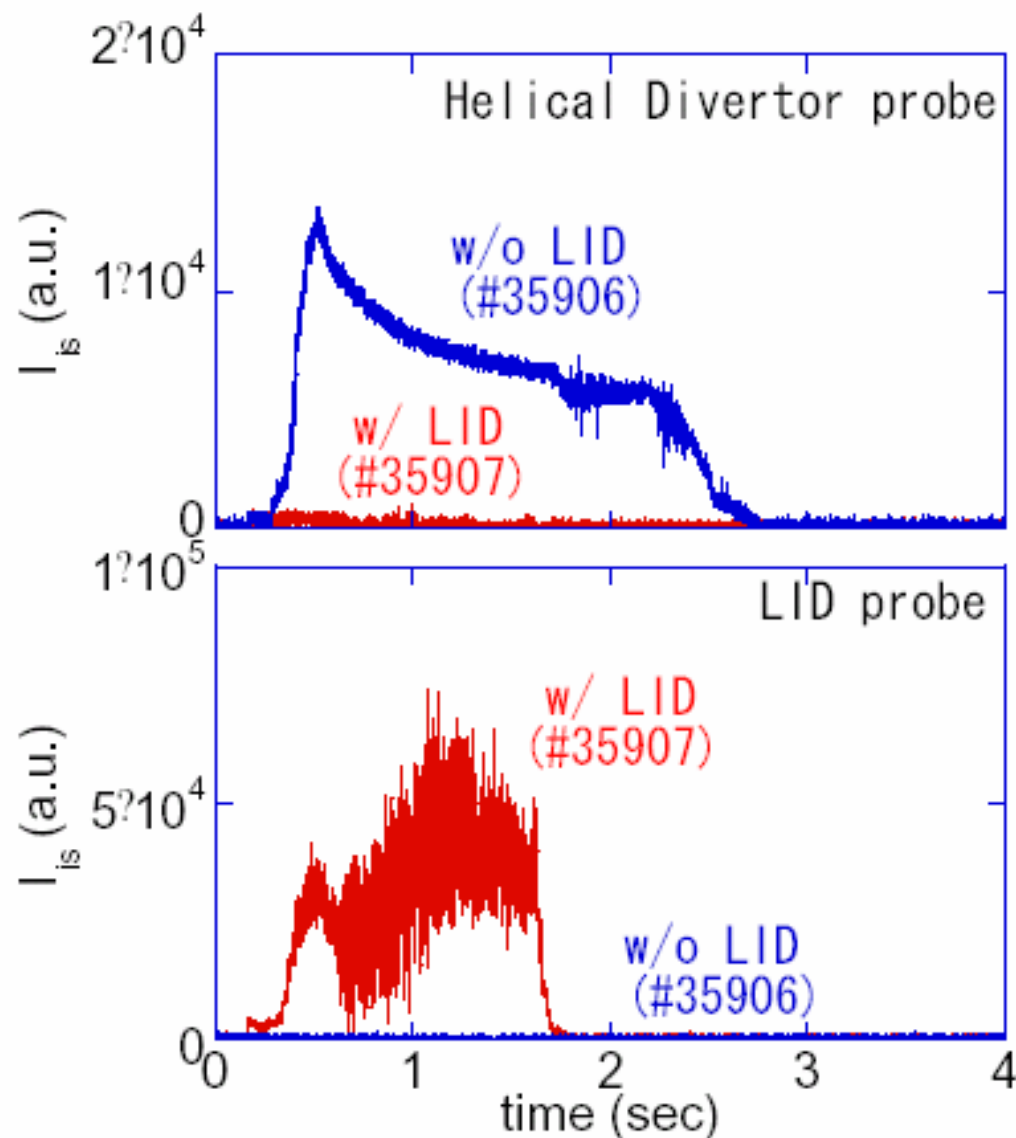
- no ergodic layer.
- volume is reduced at 60%.
- **steep  $T_e$  gradient.**
- while  $n_e$  boundary is unclear.  
---> because of long  $L_c$  ?

\* LID functions as a divertor.

--> because divertor head does not touch the core plasma.



## Particle flux to the LID head and helical divertor

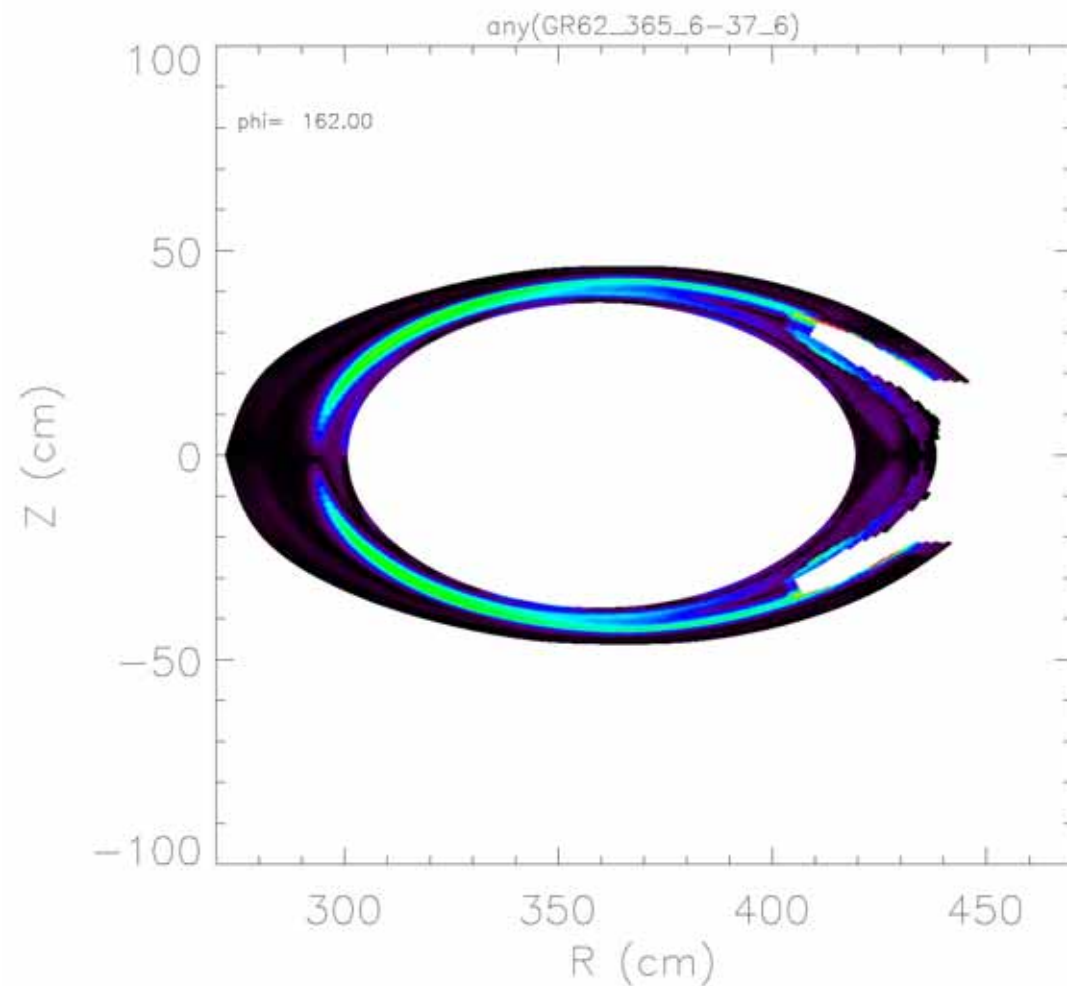


- \* **w/o** LID (open helical divertor)  
particle flux  $\rightarrow$  **helical divertor**
- \* **w/** LID (closed island divertor)  
particle flux  $\rightarrow$  **LID head**  
 $\rightarrow$  helical divertor  $\sim 0$



# Plasma flow predicted by EMC3-EIRENE

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Parallel flow established.

(as expected)

- along separatrix of island
- to LID head (back side)

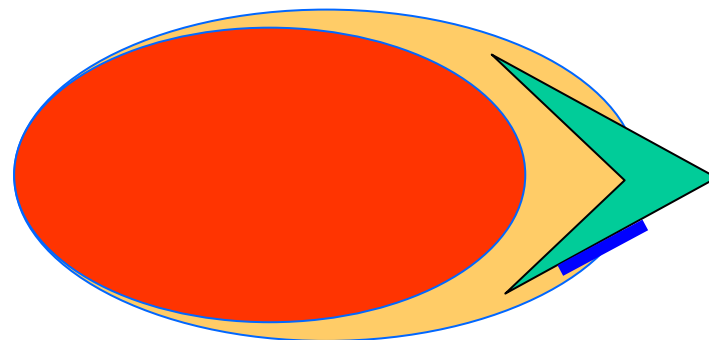
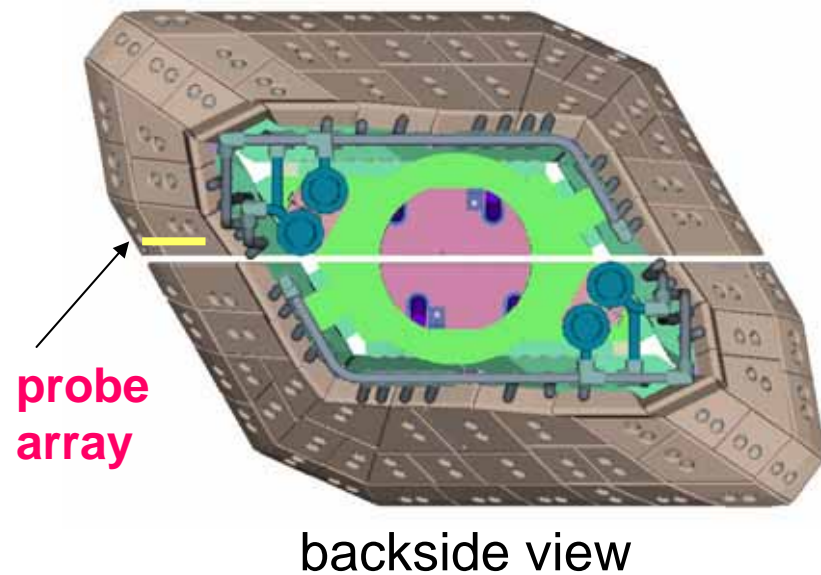
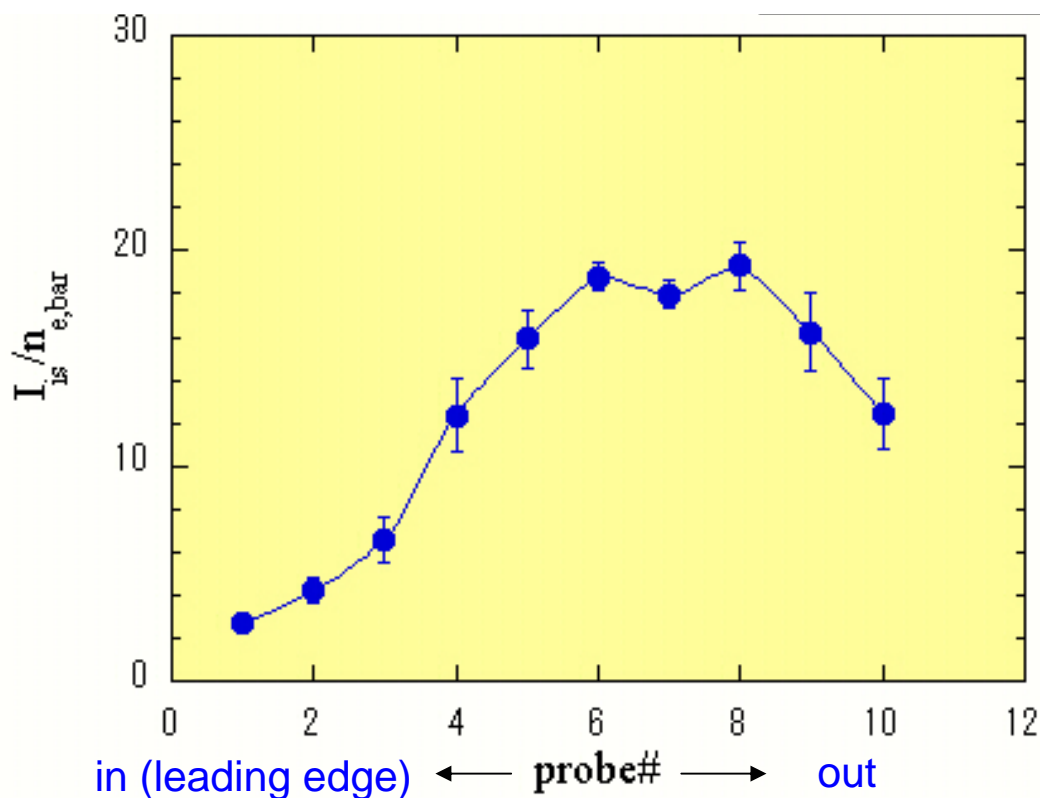
Unfavorable flow

- to leading edge
- to front side of LID head.

--> hot spot

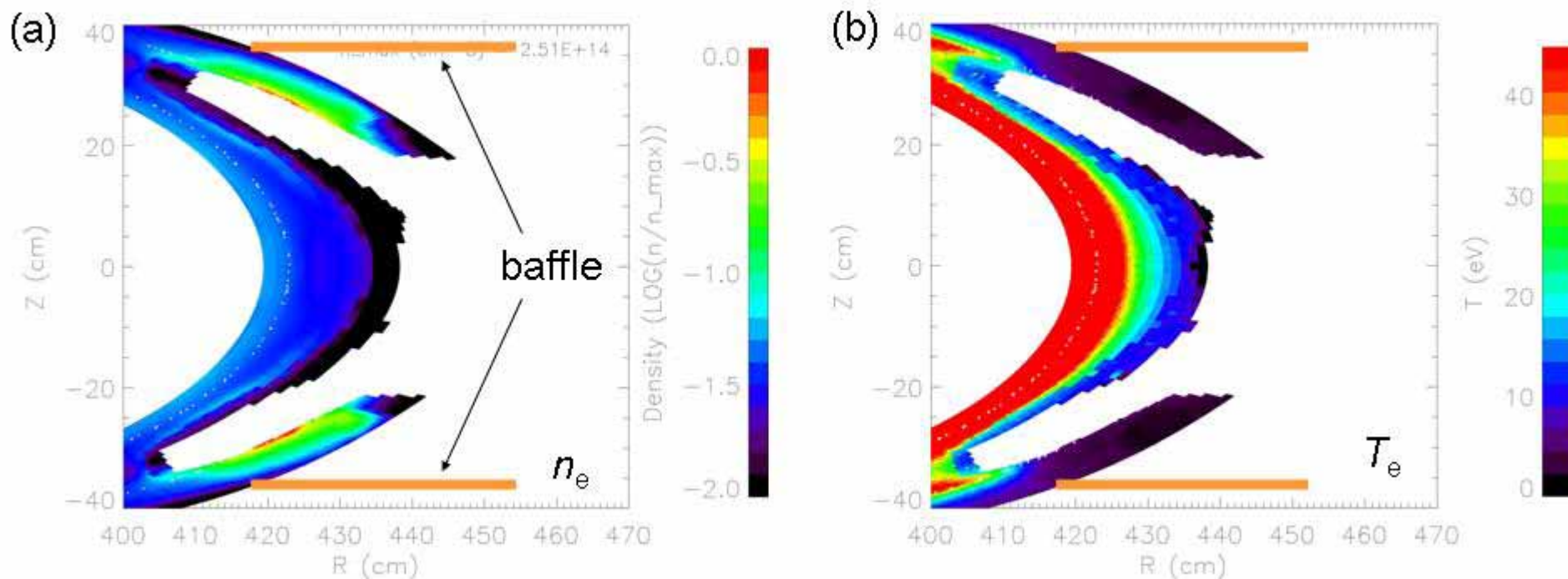
# Particle flux profile on the LID head

Head position scan (slit size=8cm=const.)



\* At the appropriate position,  
particle flux has its peak avoiding the leading edge.

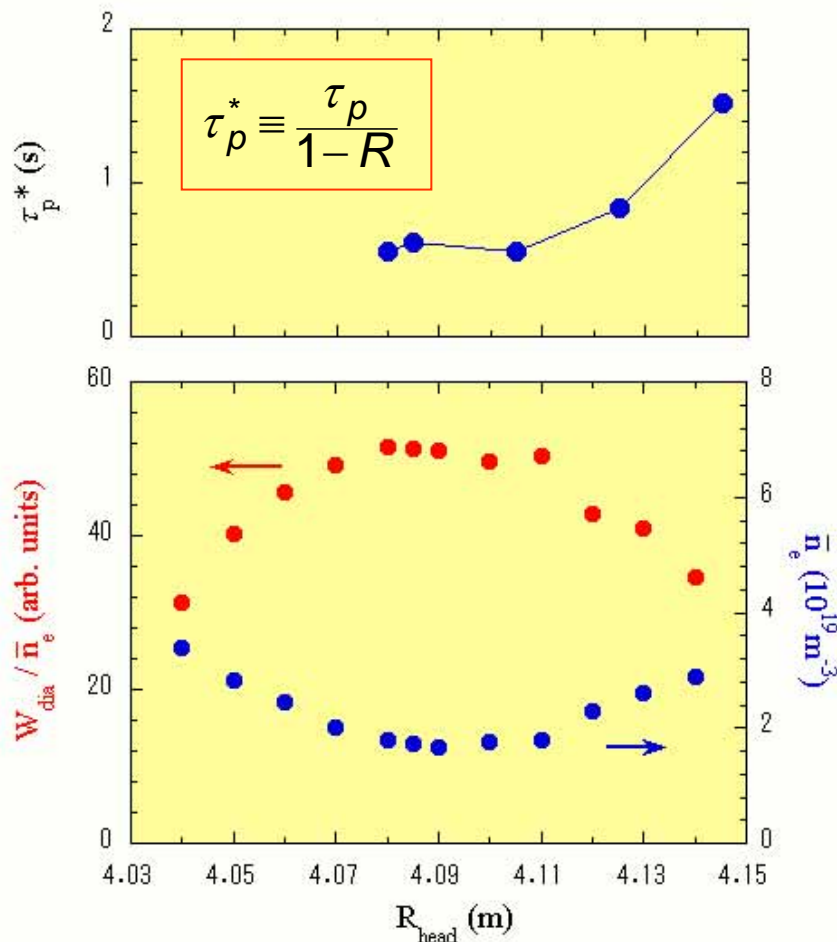
# $T_e$ and $n_e$ profile predicted by EMC3-EIRENE



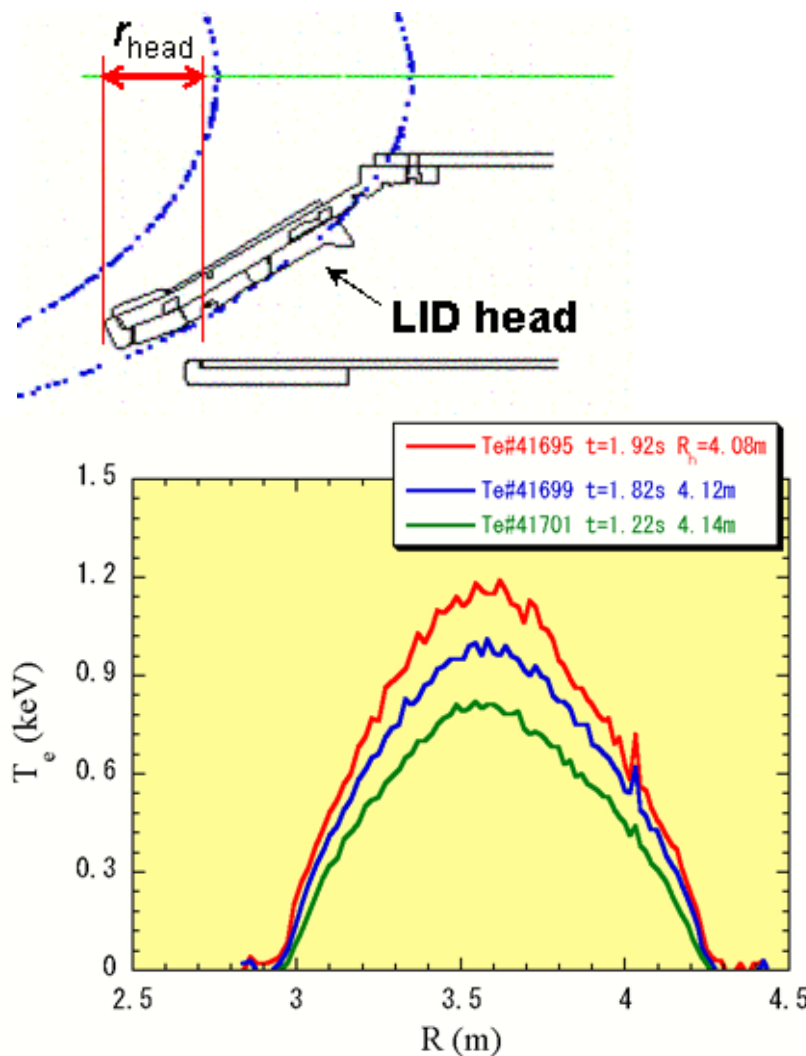
- \* Parallel flow along the island separatrix.
- \* Highest density at outer island separatrix.
- \* High  $n_e$  low  $T_e$  plasma around LID head.  
---> high recycling

# Pumping efficiency (head position dependence)

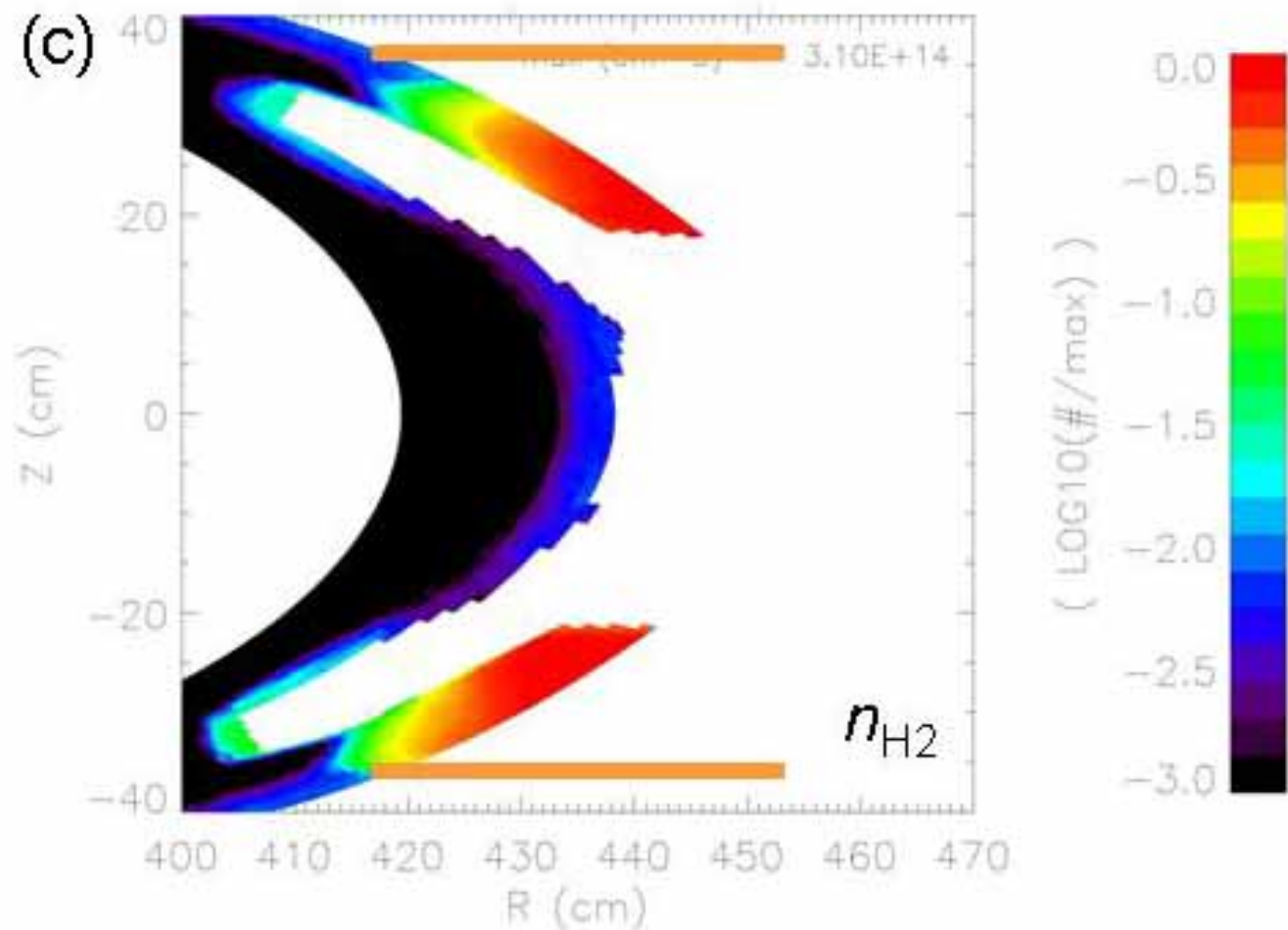
Large Helical Device



- \* gas puffing rate=const.,
- \* slit size=8cm (const.).
- \*  $\bar{n}_e$  is minimum at  $R_{\text{head}}=4.08 \sim 4.09$  m  
--> **Max. pumping efficiency**



# H<sub>2</sub> density predicted by EMC3-EIRENE



\* High particle flux.

\* Closed system.



High neutral confinement  
property ( $3 \times 10^{21} \text{ m}^{-3}$ )



\* High recycling.

\* High density.

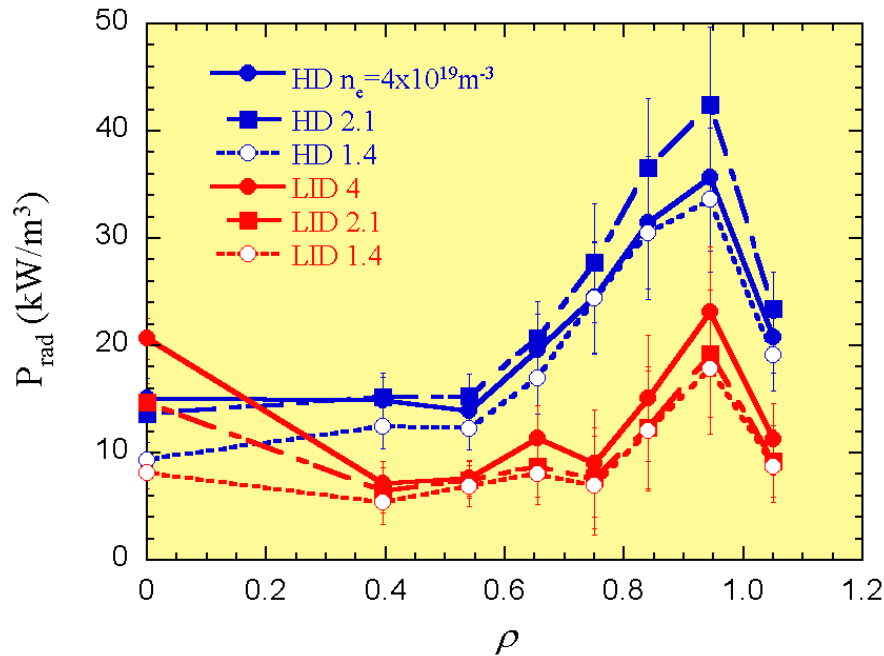


\* Detachment ?



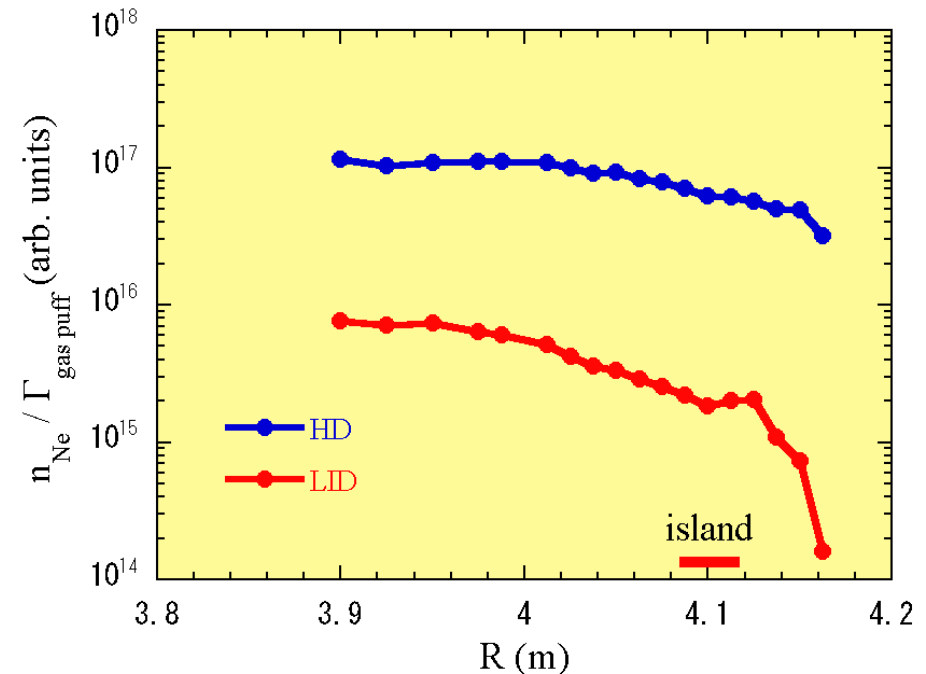
# Screening / pump out effect of LID on impurities

Large Helical Device



In **LID** configuration,

- \*  $P_{\text{rad}}$  is localized in island.  
--> accumulation at island ?
- \*  $P_{\text{rad}}$  is low in confinement region.  
--> lead to steep  $T_e$  ?
- \*  $P_{\text{rad}}$  at center increases as  $n_e$ .  
--> due to metallic impurity from LHD head.  
--> lead to degradation in  $T_e$  gradient.



\* Ne is injected by gas puffing.

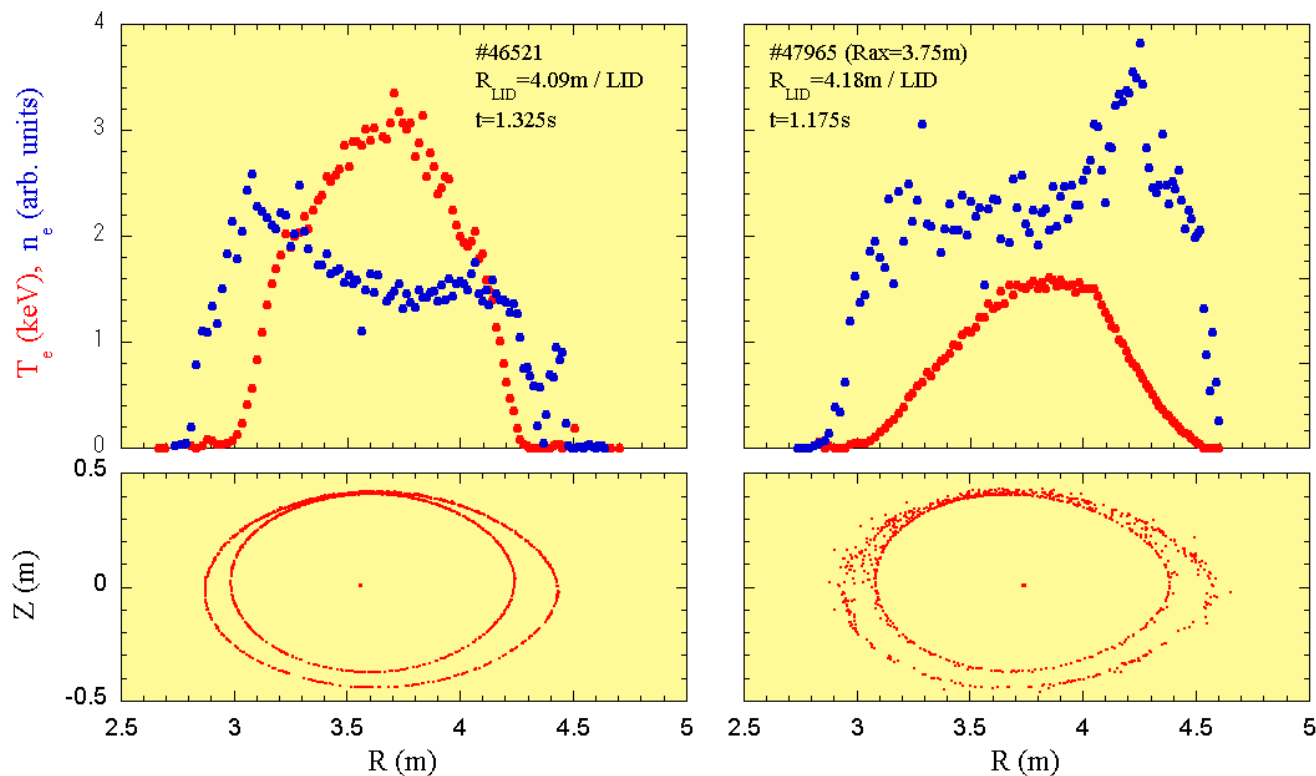
$$\begin{aligned} \Gamma_{\text{gas puff}} &= 3.26 \text{ Pa m}^3/\text{s (HD)} \\ &= \mathbf{34.7 \text{ Pa m}^3/\text{s (LID)}} \end{aligned}$$

\*  $n_{\text{Ne}}$  profiles are measured with CXRS.

**Low Impurity density in LID**

**--> impurity screenig**

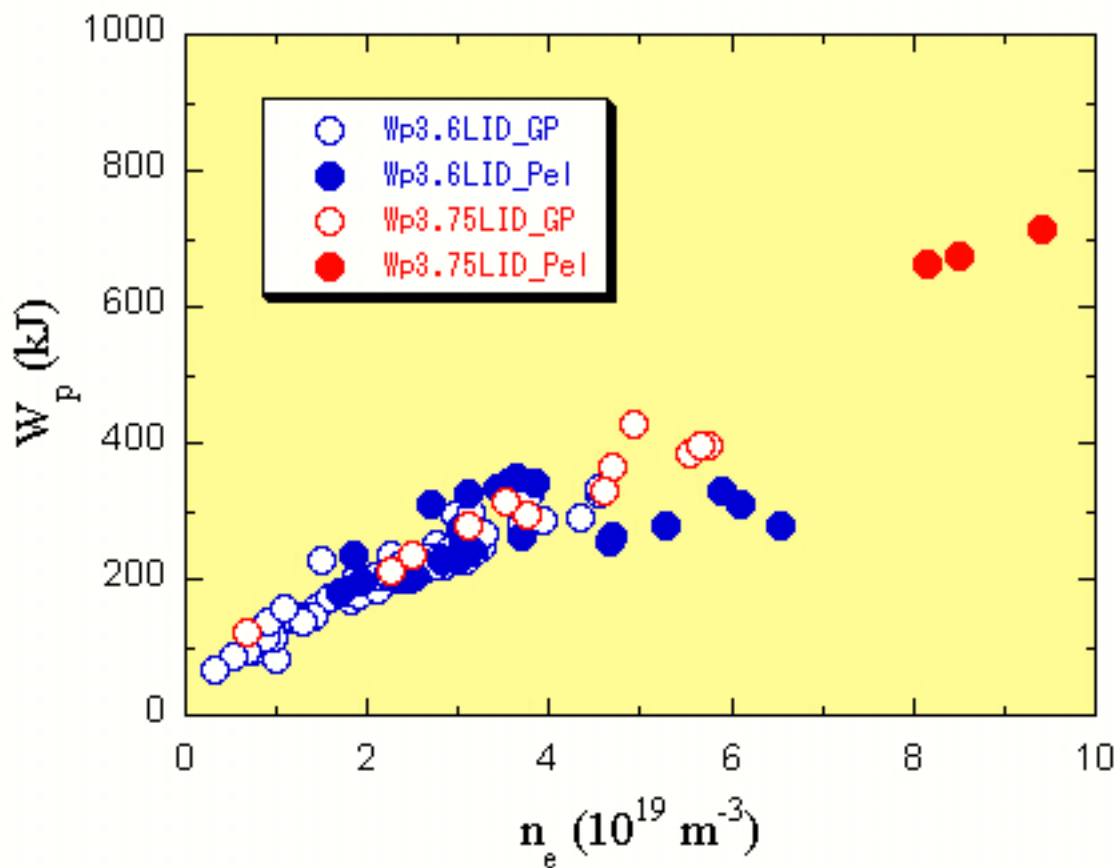
# New outward shifted magnetic configuration ( $R_{ax}=3.75m$ )



## In $R_{ax}=3.75m$ configuration,

- \* Confinement volume is almost the same as  $R_{ax}=3.60m$ .
- \* Foot positions of  $T_e$  and  $n_e$  are close ( $\rightarrow$  SOL is wide).
  - $\rightarrow$  due to the stronger ergodicity around the island ?
  - $\rightarrow$  due to the different  $L_c$  ?

## Parameter regime is extended

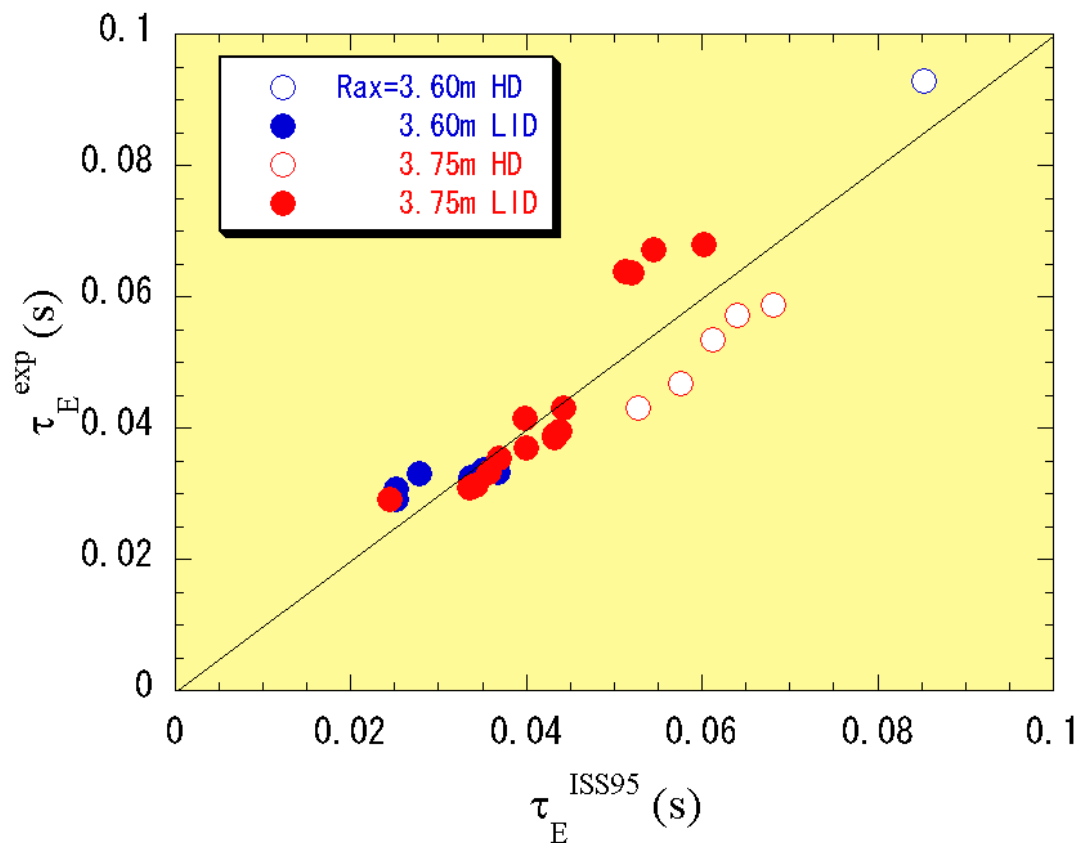


In  $R_{ax}=3.75\text{m}$  configuration,

\* higher  $n_e$  is achieved.

\*  $W_p \sim 757\text{kJ}$  (LID),  
-- comparable to HD ---

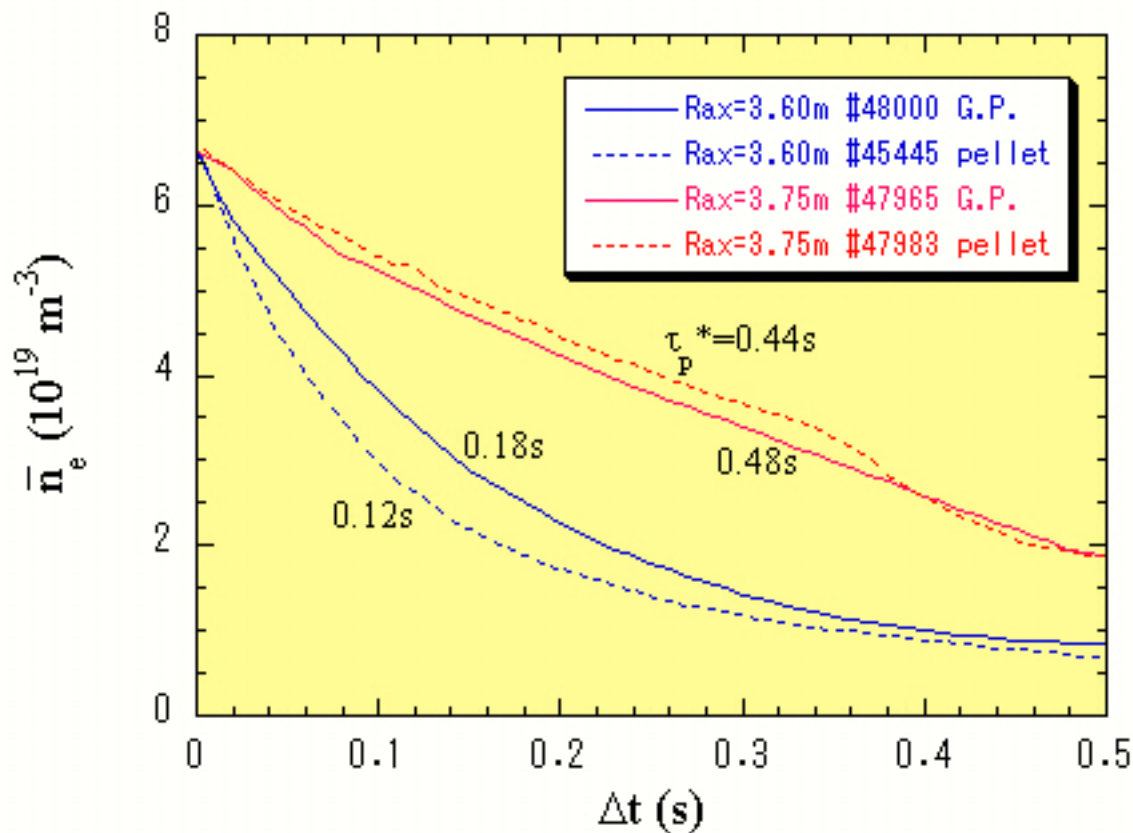
# Outward shifted configuration



## \* Energy confinement in LID

- confinement is improved in outward shifted configuration,
- which is superior to that in HD configuration.
- which is 1.2 times higher than that of ISS95 scaling.

## Density decay time in two configurations



In outward shifted configuration

- ergodic
- unfitted LID head shape



- \* Degradation of collecting efficiency
- \* Unfavorable recycling is enhanced.

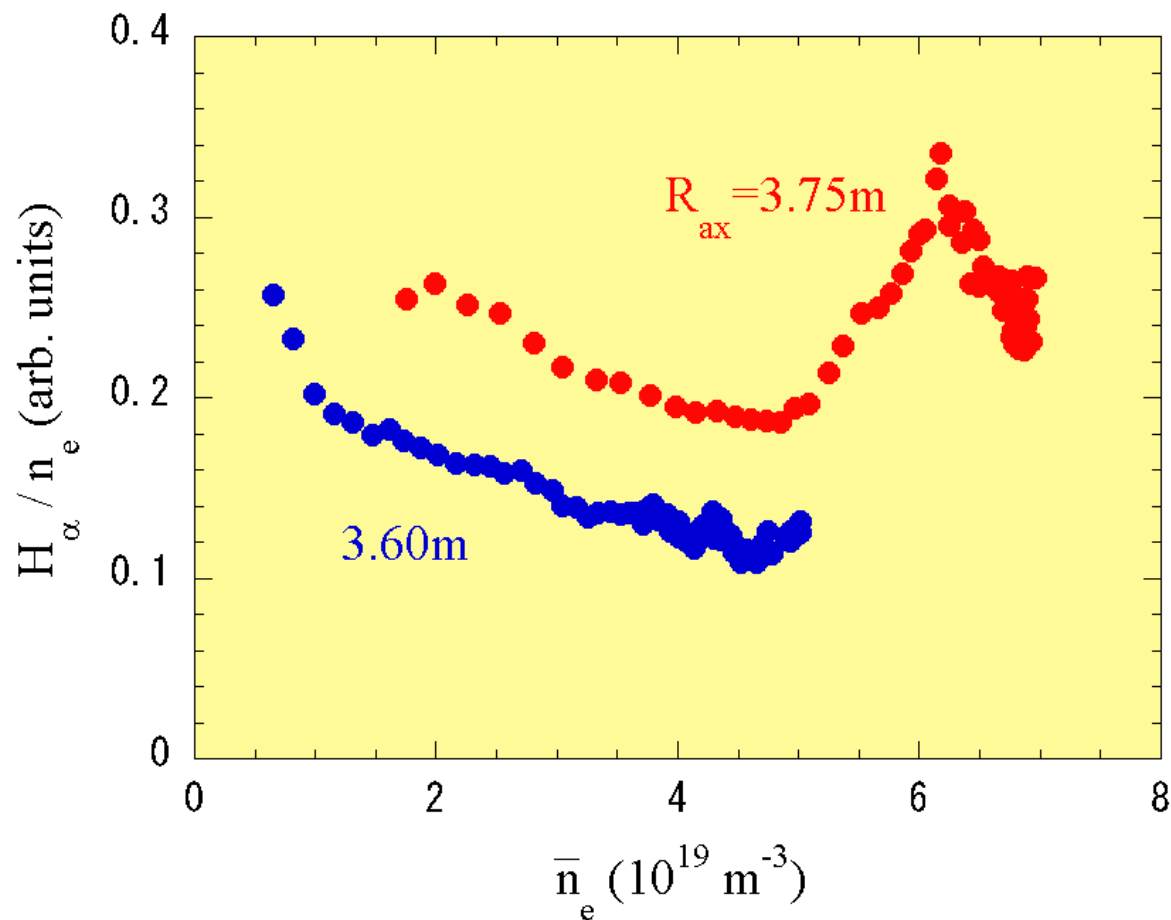


Long  $\tau_p^*$

No difference between gas puff and pellet



# Outward shifted configuration



In outward shifted configuration.



High recycling.



Fueling strongly increased.



Good plasma performance



# Summary

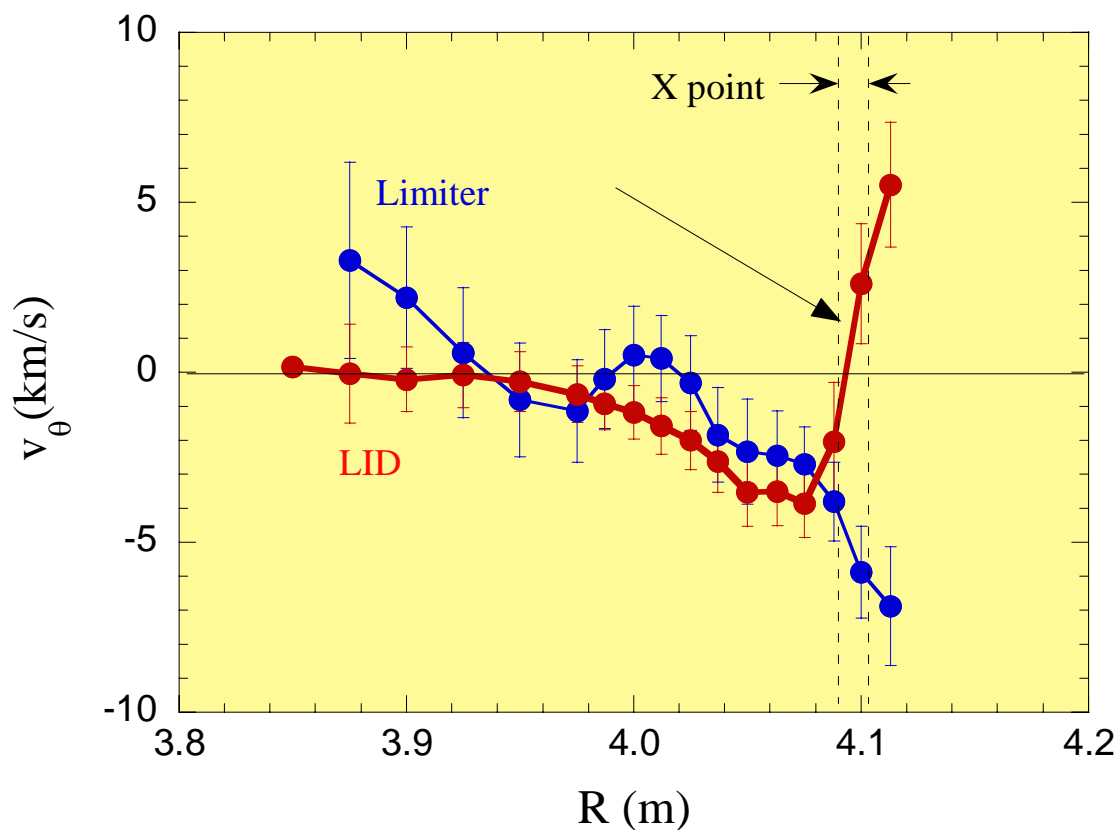
- 1) Fundamental functions of LID were confirmed, that is,
  - \* **strong pumping** effect,
  - \* formation of the **steep edge gradients**,
  - \* **avoiding the leading edge** problem.
  - \* **impurities (Ne) screening** effect.
    - > **pump out effect ?**
  
- 2) Confinement property in LID configuration
  - \* follows the ISS95 scaling law.
  - \* **improves in the outward shifted configuration**,
    - > 1.2 times higher than that of ISS95.
    - > **due to the enhanced recycling particles ?**
  - \* **efficient fueling leads to high confinement regime ?**
  
- 3) **First results from EMC3-EIRENE**

# Plans for next campaign

---

- 1) Control the  $L_c$  to LID head.
  - by shifting  $R_{ax}$ .
  - by controlling the perturbation field strength.
- 2) Divertor gas puffing.
- 3) Potential control
- 4) Estimation of pumping efficiency
- 5) Analyses of impurity transport.
- 6) Edge modeling (EMC3-EIRENE)

# Radial electric field

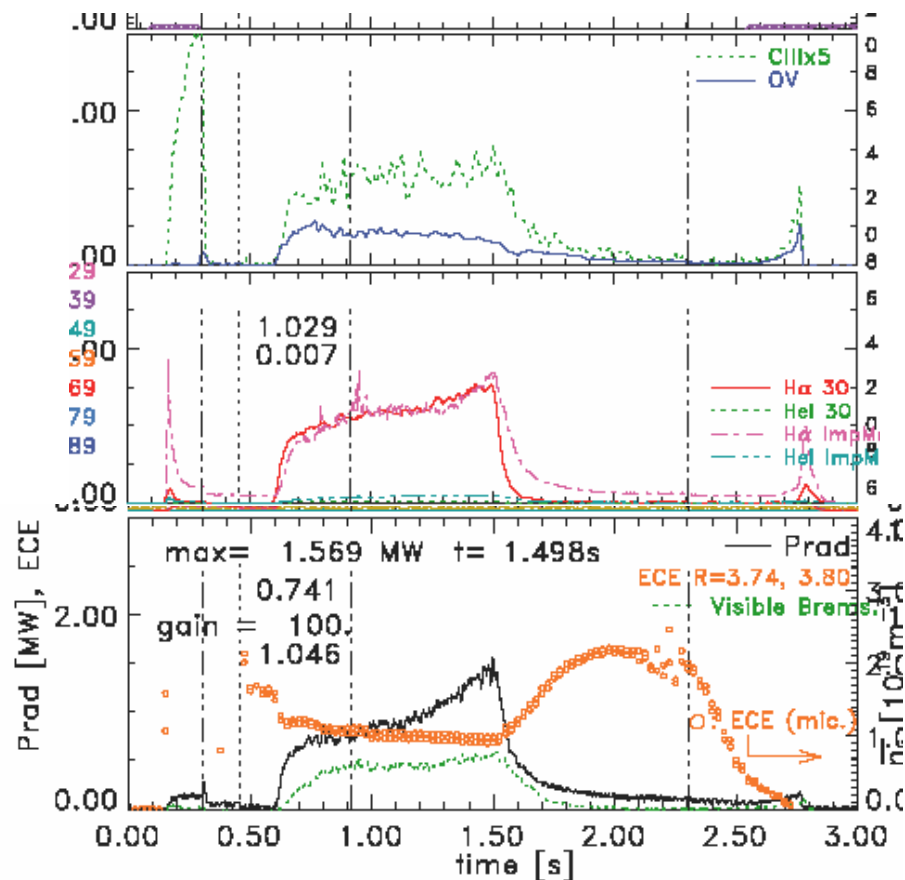


- \* Positive  $E_r$  in the island region (LID).
- \* Negative  $E_r$  (Limiter).
- \* Effect of  $E_r$  on impurity behavior is unclear.

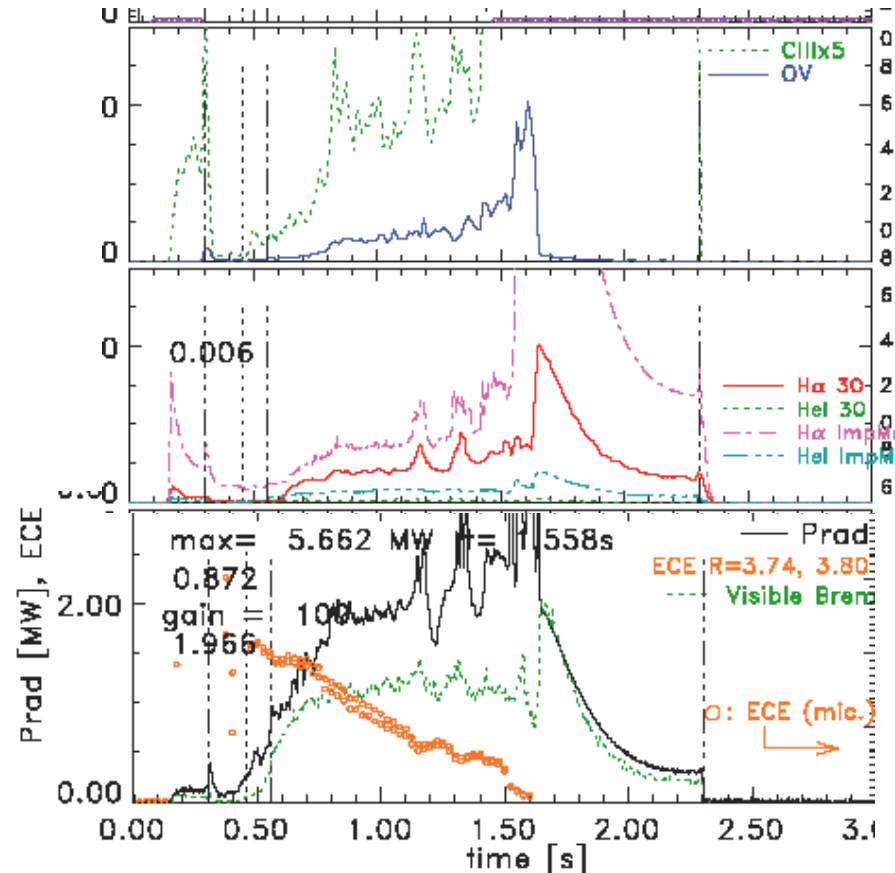
# Time behavior of impurity quantity, $P_{\text{rad}}$ and $T_{\text{e0}}$

Large Helical Device

## LID



## Limiter

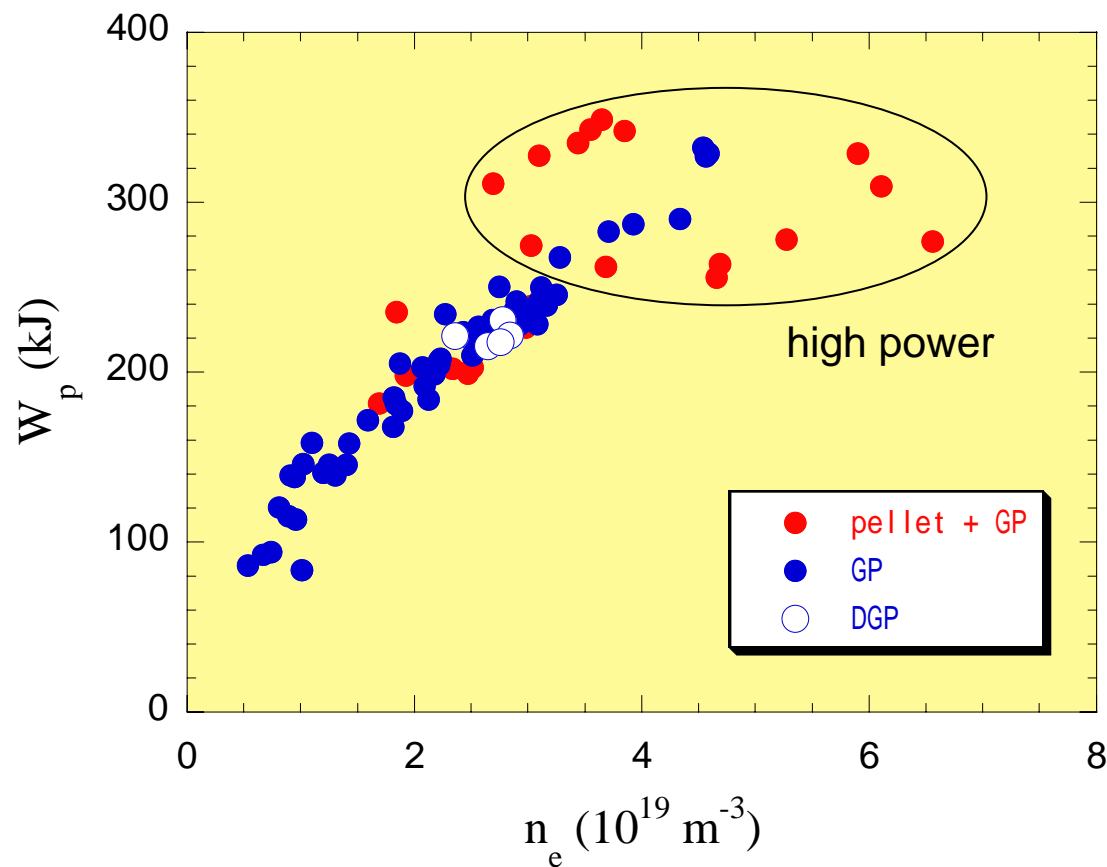


\* In limiter configuration during high power discharge, impurities (carbon) are released from the leading edge.

-->  $P_{\text{rad}}$  increase -->  $T_{\text{e}}$  decreases



# Confinement property with different fueling methods



\* **Low power region ( $P < 4 \text{ MW}$ ).**

- Little difference is seen in different fueling method.

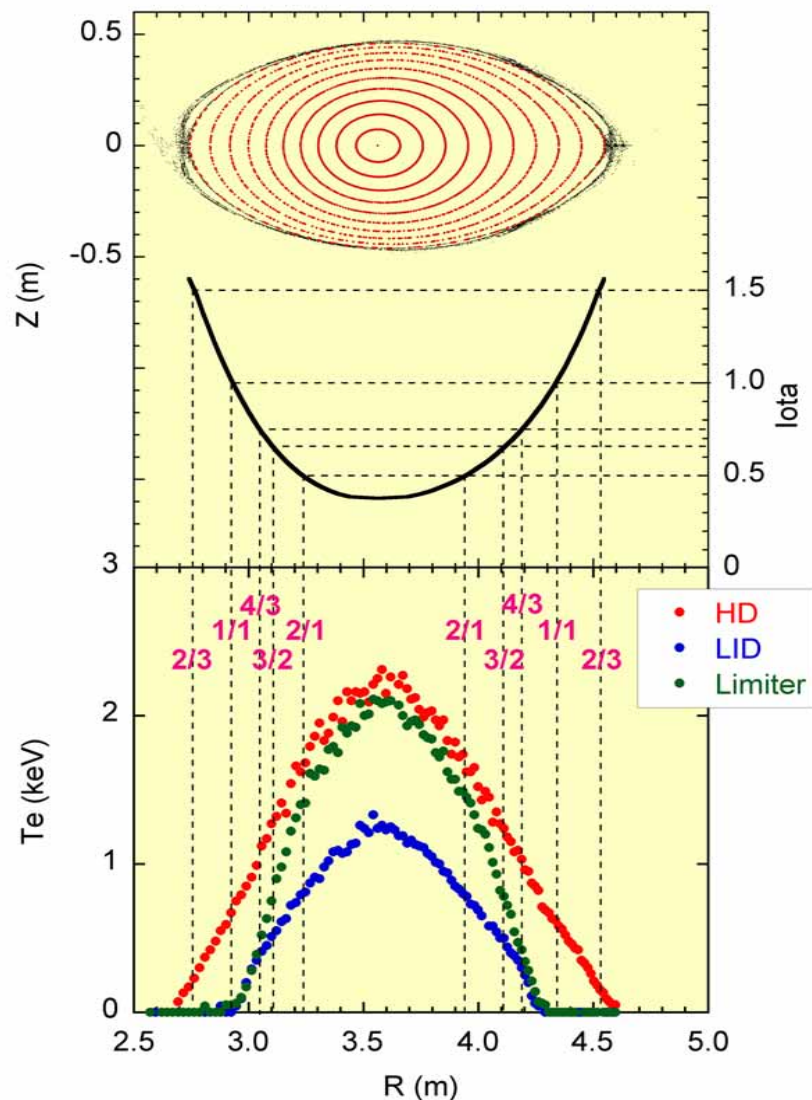
\* **High power regime ( $P \sim 9 \text{ MW}$ ).**

- Pellet injection is superior to gas puff.

\* **Higher power + pellet injection**

--> higher  $W_p$  is expected.

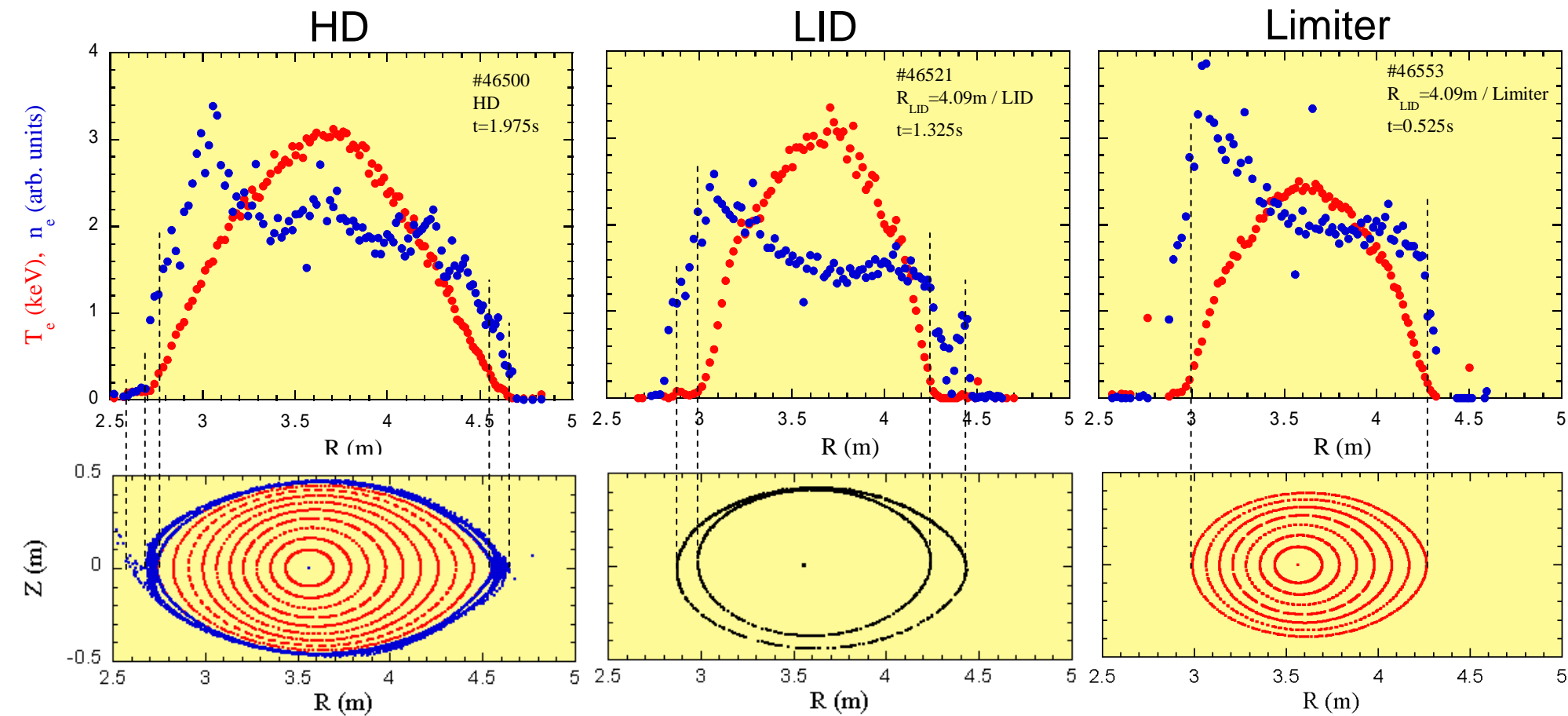
# MHD



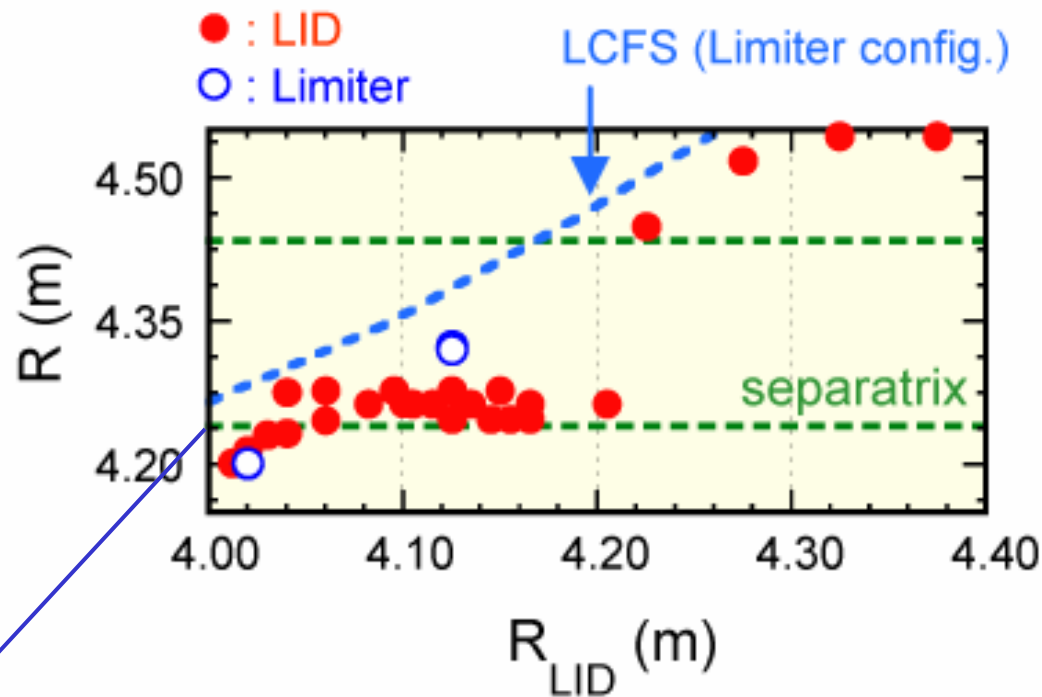
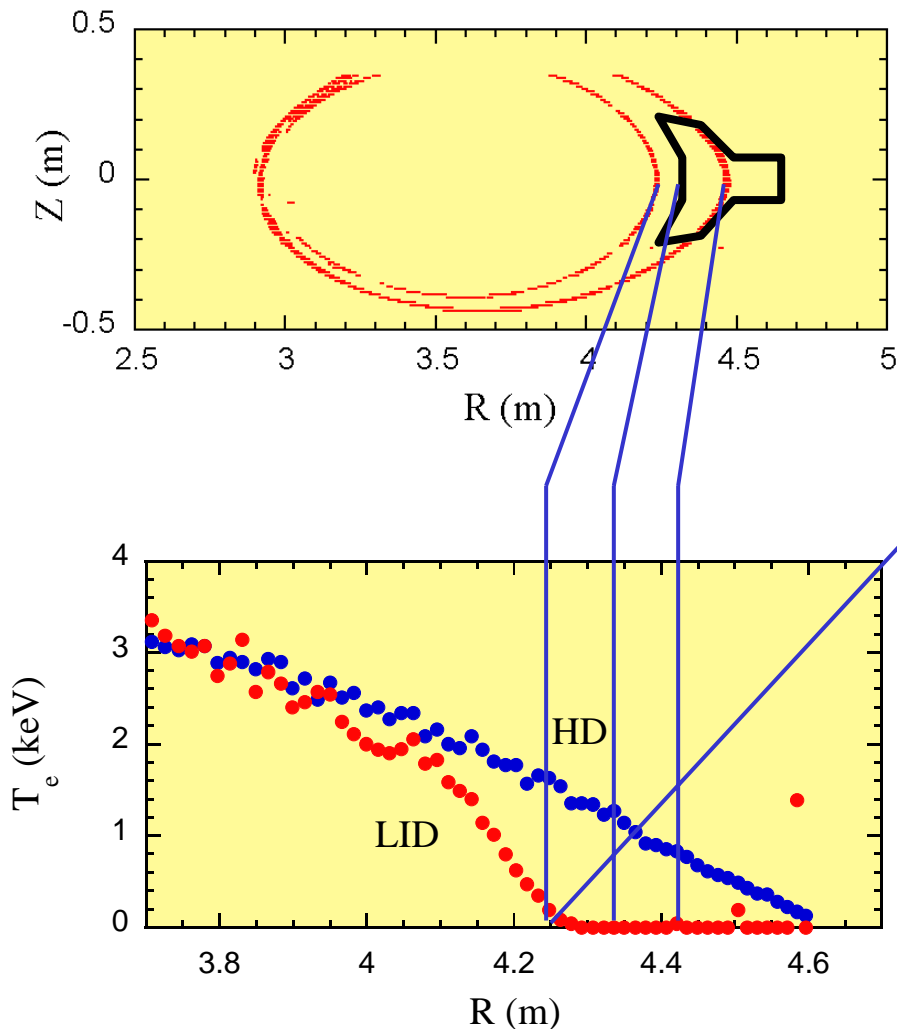
$R_{ax}=3.6\text{m}$ ,  $B_t=2.75\text{T}$ ,  $B_q=100\%$ ,  $\gamma=1.25$   
 gas=H,  
 $n_{e\_bar}\sim 2.8 \times 10^{19} \text{ m}^{-3}$  (const.)

	in				out		
iota_bar	0.5	0.67	0.75	1	1.25	1.33	1.5
m/n	2/1	3/2	4/3	1/1	4/5	3/4	2/3
HD				**	***	***	***
Limiter	*	***	***				
LID		***	***				

# $T_e$ and $n_e$ profiles at $R_{ax}=3.60m$



# $T_e$ profile and separatrix position



\* LID functions as a divertor.

--> because divertor head does not touch the core plasma.